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RECONNAISSANCE GEOCHEMICAL ASSESSMENT OF MINERAL RESOURCES IN THE SILVER PEAK SURVEY AREA (NV-050-0338), WEST CENTRAL NEVADA

Prepared by Jack Quade, Senior Geologist
J. V. Tingley, Principal Investigator

Prepared for:

UNITED STATES DEPARTMENT OF THE INTERIOR
BUREAU OF LAND MANAGEMENT
LAS VEGAS DISTRICT OFFICE
LAS VEGAS, NEVADA 89108
Under Contract YA-553-CT1-1058

This information should be considered preliminary. It has not been edited or checked for completeness or accuracy.

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Correlation Analysis, Panned Concentrate Samples
Correlation Analysis, Rock Samples

INTRODUCTION

The Silver Peak Wilderness Study Area (WSA, NV-050-0338) contains approximately 60 square miles and is within the Stateline/Esmeralda Resource Area, Esmeralda County, Nevada (Figure 1). The best access to the area is via State Route 3A near Dyer from the west or State Route 47 via Silver Peak from the east. Fair to good roads provide access to a limited area along the margins of the WSA.

The WSA is in the central portion of the north-south trending Silver Peak Mountains and includes 9450 foot Piper Peak, the highest peak in the range. From this point perennial stream courses radiate into Clayton Valley and Fish Lake Valley.

Mining activity first occurred along the present boundaries of the WSA in the period 1863-1864 when silver was mined in the Dyer district and in the Red Mountain district to the east. To the northeast, gold mining in the Mineral Ridge area also began in the early 1860's but the main activity was 1933 to 1942 (Albers and Stewart, 1972). Both patented and unpatented claims remain active within the area especially along the northern and eastern boundaries of the WSA, the Sanger and Sixteen-to-one mines are currently in operation and prospecting continues in all parts of the area.

A geochemical survey of the WSA and the immediate surrounding area was made in the spring of 1984 as part of the Bureau of Land Managements' resource evaluation of areas under consideration for wilderness classification.

GENERAL GEOLOGY

Pre-Cambrian Paleozoic basement rocks are exposed along the northern and southern margins of the WSA and smaller exposures of the rocks are also found near the western edge of the WSA. Intruding the older sediments are Mesozoic plutons and smaller bodies of pegmatites as well as aplite and latite dikes. Mineralization associated with these intrusives has been identified to the northeast in the Mineral Ridge district and to the west in the Dyer district.

The central highland of the Silver Peak range lies between the areas of basement rock and consists of late Pliocene tuffs and flows that originated from the Silver Peak Caldera. The caldera has its center about 3 to 4 miles northeast of Piper Peak and is about 4 by 8 miles across. The long axis of the caldera trends northwesterly parallel to the folding of the basement rocks and to an inferred Pliocene trough (Robinson, et al., 1968, p. 607). According to Robinson (1968), the trough may have extended from Clayton Valley northwesterly to Fish Lake Valley and received sediments from early to middle Pliocene time.

Early caldera erruptions produced rhyolitic to andesitic lava flows interbedded with airfall tuffs and waterlaid sediments. Later subsidence produced northeast striking, high-angle faults that became mineralized during the later stages of the caldera cycle, Keith (1977). The oldest volcanic rocks in the caldera cycle are dated at 6.1 m.y, and the youngest (basalts) are 4.8 m.y.. Robinson (1968) estimated that during that time interval, 25 cubic miles of lava were extruded from the Silver Peak caldera.

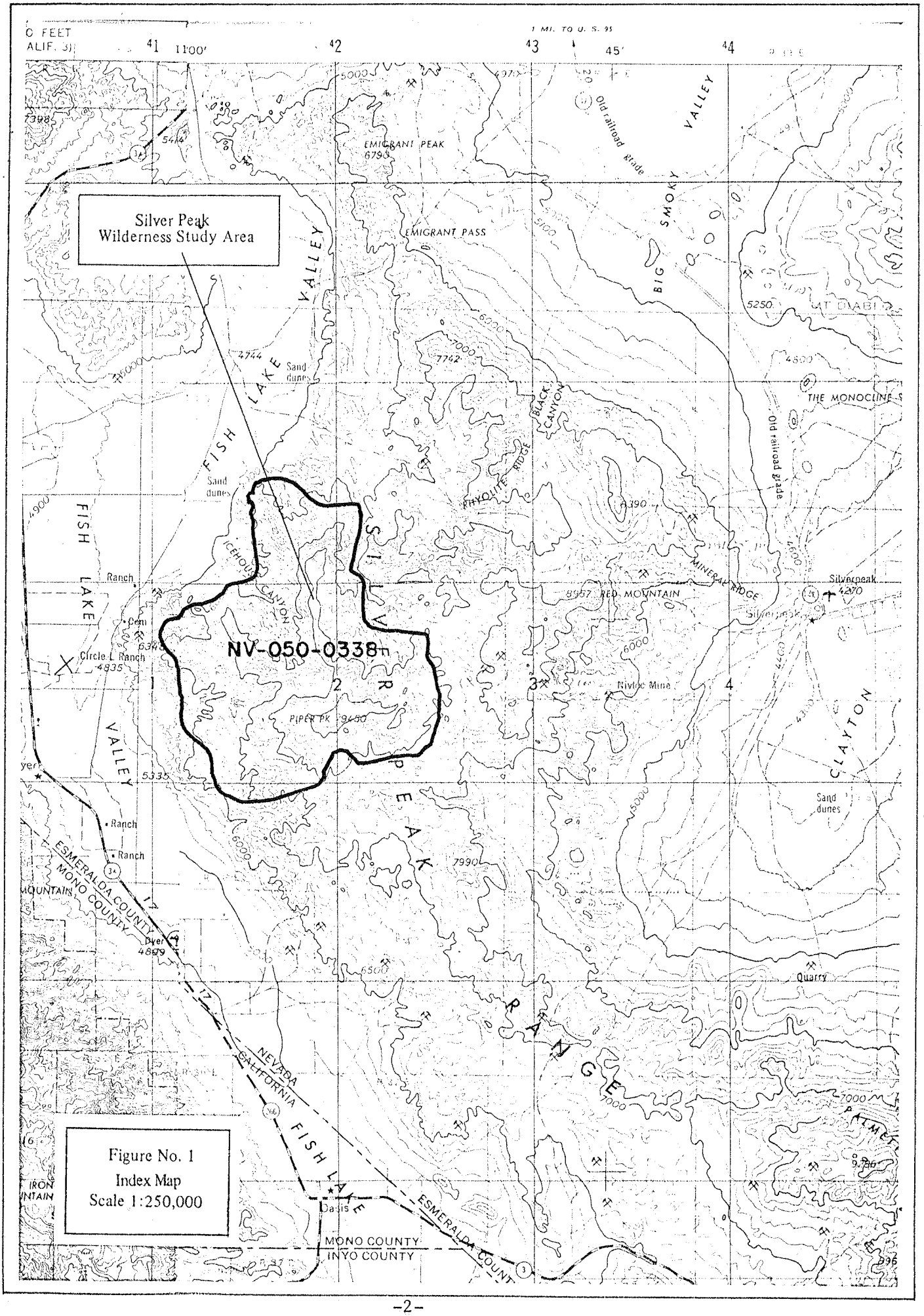


Figure No. 1
Index Map
Scale 1:250,000

Baker and Bruff, (1982) have a slightly different scenario for the later stages of activity of the Silver Peak caldera and for the time of mineralization in the district. According to their interpretation, during early caldron activity sediments, including lake beds, were deposited along with basaltic flows. During later resurgence of the caldera a central dome formed. By Baker and Bruff's interpretation, the final event was collapse of the resurgent dome and adjacent rocks outside the caldera by displacement along northeast bearing faults that extended from within the caldera some miles beyond the margin to the northeast. Development of these structures and formation of vein mineralization along them was late in the caldera cycle. Manganese mineralization cutting the youngest caldera sediments is felt to be evidence of this timing of mineralization (Baker and Bruff, 1982).

One effect of caldera collapse was to drop the northeast-striking veins in the western part of the caldera down to a position where they were protected from erosion, thereby preserving the mineralization further down in the system. In the eastern part of the district erosion has exposed mineralized veins,they have been leached and some display secondary enrichment at depth (Baker and Bruff, 1982).

Figure 2 is a generalized geologic and structural map of the study area by Albers (1967) and Albers and Stewart (1972). An excellent summary and discussion of geology, stratigraphy, structures, rock units, and mining activities is presented in G-E-M Resources Report for the Silver Peak Range (Great Basin Joint Venture, 1983). For more detailed description of the geology of Esmeralda County, see Albers and Stewart (1972). Baker and Bruff (1982) and Keith (1977) describe the Red Mountain Mining district and related geology in detail. Geologic coverage of the entire study area at a scale of 1:62,500 is provided by Krauskopf (1971), Robinson and Crowder (1973), Stewart and others (1974) and Robinson and others (1976). Much of the information for this report was taken from these sources.

SAMPLE COLLECTION AND ANALYTICAL TECHNIQUES

The geochemical survey included collecting stream-sediment and panned concentrates from the active drainage systems and rock samples from mines, prospects and outcrops within and along the margins of the WSA (see Figure 3). Field and sampling assistance was provided by Norman L. Stevens.

Stream-sediment samples were collected from 4 or 5 different places along the active portion of the stream course at each sample site and were seived to minus-80-mesh. Approximately 100 grams of sample were retrieved from each of 44 separate sites. A second sample was collected at each site from the same stream course consisting of a 10-15 lbs of minus-16-mesh stream sediment. The second sample was carried to a source of water where it was ultimately pan-concentrated to 100 grams. Rock samples were channeled from veins in mines, selected from dumps and prospects and chipped from outcrops. All of the samples were returned to Reno where they were analyzed in a portable laboratory by a team from the Branch of Exploration Geochemistry, U.S.G.S., led by Reinhard Leinz and David Grimes.

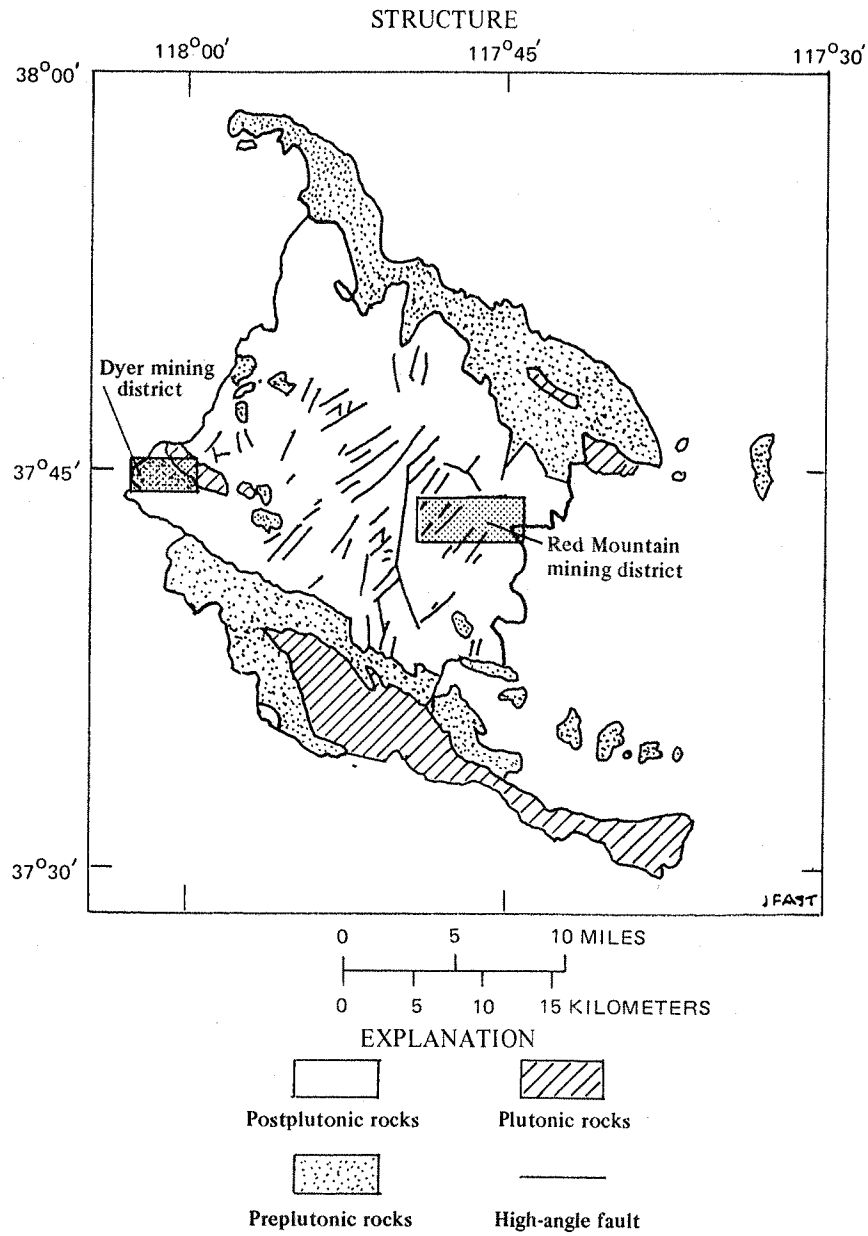
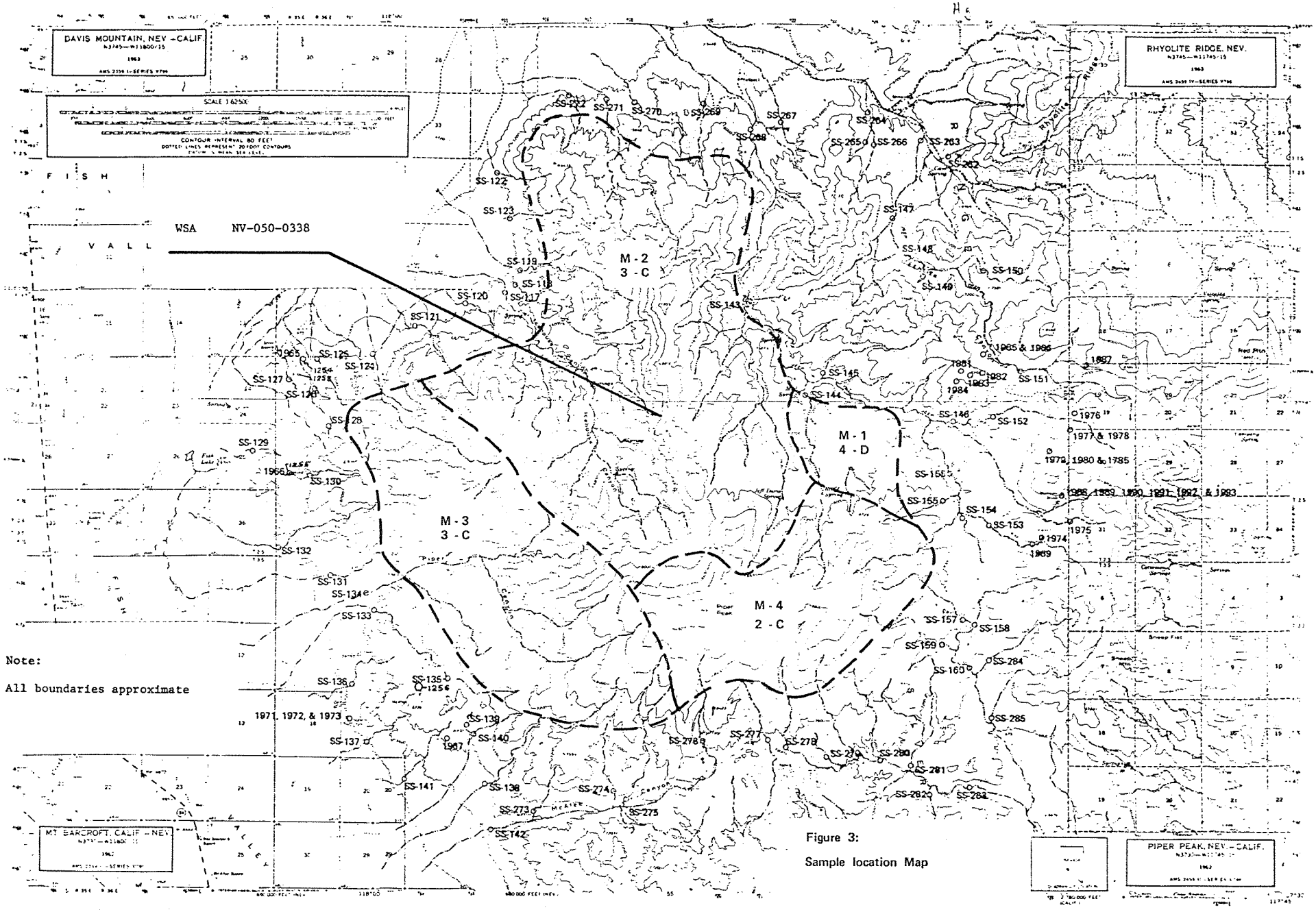


Figure 2. Generalized geologic and structure map of the Silver Peak structural block after Albers (1967) and Albers & Stewart (1972).



Note:

All boundaries approximate

Figure 3:

Sample location Map

At the lab the panned samples were further concentrated using bromoform and an electromagnet to remove the rock forming minerals and the magnetic fraction. The remaining nonmagnetic split was pulverized to minus 80-mesh as were the rock samples. The three sets of samples were dried at 90° C before being analyzed for 31 elements on an emission spectrograph. After reviewing the results selected samples were further analyzed by atomic absorption or other techniques to either improve detection limits or to add elements to the data base. Visual and microprobe techniques were used in several instances for mineral identification. Figure 4 shows the limits of determination for the spectrographic analysis.

Figure 3 is a single map of all of the sample sites, while Figures 7-10 are panned concentrate sample sites on a geochemical map showing the concentrations of individual elements. Rock sample locations are presented in Figures 11-20.

Geochemical anomalies were established using the following criteria: significant concentrations of a given element that exceeded the background, the detection limit of the analysis, geologic mapping, structures, lithologies, geomorphology, and a tertiary examination of cumulative frequency tables, and percent frequency tables. For visual inspection and to observe spatial and geochemical relationships there are separate figures to show each of the 11 elements; silver, gold, arsenic, copper, lead, zinc, mercury, tungsten, barium, and managanese.

Figure 5 is a visual and numerical comparison of which data set was best for detecting individual element concentrations using the E-Spec data from panned concentrates and sediment samples.

Figure 4 Limits of determination for the spectrographic analysis of rocks and stream sediments, based on a 10-mg sample.

Elements	Lower Determination Limit	Upper Determination Limit
	Percent	
Iron (Fe)	0.05	20
Magnesium (Mg)	.02	10
Calcium (Ca)	.05	20
Titanium (Ti)	.002	1
	Parts per million	
Manganese (Mn)	10	5,000
Silver (Ag)	0.5	5,000
Arsenic (As)	200	10,000
Gold (Au)	10	500
Boron (B)	10	2,000
Barium (Ba)	20	5,000
Beryllium (Be)	1	1,000
Bismuth (Bi)	10	1,000
Cadium (Cd)	20	500
Cobalt (Co)	5	2,000
Chromium (Cr)	10	5,000
Copper (Cu)	5	20,000
Lanthanum (La)	20	1,000
Molybdenum (Mo)	5	2,000
Niobium (Nb)	20	2,000
Nickel (Ni)	5	5,000
Lead (Pb)	10	20,000
Antimony (Sb)	100	10,000
Scandium (Sc)	5	100
Tin (Sn)	10	1,000
Strontium (Sr)	100	5,000
Vanadium (V)	10	10,000
Tungsten (W)	50	10,000
Yttrium (Y)	10	2,000
Zinc (Zn)	200	10,000
Zirconium (Zr)	10	1,000
Thorium (Th)	100	2,000

Figure 5

Detection of Elements using E-Spec
on Panned Concentrates and Stream Sediments

Comparable	Better		High Variability		Not Detected	
	PC	SS	PC	SS	PC	SS
Mg	Ca	Fe	B		Au	Au
Mn	Ti	B	Co		Sb	Sb
Cr	Ag	Be	Cu		Cd	Cd
V	As	Co	Zn			Bi
	Ba	Ni				W
	Bi					Nb
	Cu					Th
	La					Sn
	Mo					
	Nb					
	Pb					
	Sc					
	Sn					
	Sr					
	W					
	Y					
	Zn					
	Zr					
	Th					

DYER DISTRICT

The Dyer district covers a very small area on the western edge of the Silver Peak mountains, directly east of the Dyer Ranch.

Old mines and small prospects in the main part of the district are clustered within an area of about one quarter mile along a single northwest trending dry wash. Prospecting has been confined to a northwest-trending outcrop of Cambrian Harkless Formation which has been intruded by a body of quartz monzonite. Immediately to the northeast, the Harkless forms the lower plate of a thrust sheet that has been overridden by the Poleta Formation.

Spurr (1906) mentions that there was activity in the district in 1863-64, more in the period 1884-87, but the district was quiet during his visit in 1903. Lincoln (1923) mentions production from the district in 1912, and Couch and Carpenter (1943) show a small production in 1925. Total production for the district through 1972 is given at a little under $13,000 (Albers and Stewart, 1972), so the total of all the years of activity resulted in very little actual dollar value.

The best description of the old workings is given by Spurr (1906). Black copper-silver sulfides, in places oxidized to carbonates and oxides, occur in quartz veins in crushed, folded shales and silicified limestones. The structures along which the veins formed strike N60^{o}-80°W, and display manganese-iron oxide rich gossan zones along them. Areas of jasperoid laced with silica veinlets were seen in zones along a structure near sample site 1253. The site is within the Dyer Ranch Prospect and yielded a high value for Zn (10,000+ppm) and lower values for Cu, Pb, Ni, and V. Samples 1965 and 1254 were collected from the dumps of the Dyer Shaft and adjacent workings. Silver values from these samples were 50 and 3000ppm respectively. Anomalous values were recorded for Pb (500 and 20,000ppm), Zn (500 and 1500ppm), As (5,000 and 10,000ppm), Cu (150 and 1000ppm), Sb (78 and 1500ppm), with anomalous but lower values for Ba, Sr, V. Panned concentrate samples from 5 stream sediment sites within a mile of the Dyer shaft yielded anomalous Pb, Hg, Sr, and W with one sample having 5000ppm Zn. These elements and values clearly identify a base metal association with precious-metal mineralization. This geochemical fingerprint can be extended 2-3 miles to the southeast where similar element concentrations occur along parallel structures within the same band of Cambrian sediments.

The presence of tungsten in the stream sediments near the Dyer shaft may be accounted for by mineralization along the nearby contact between PreCambrian sediments and the Dyer Pluton. However, the increased tungsten values further to the southeast and away from any observable granitic source does not tie to the Dyer Pluton or to any other obvious explanation. The size of the mineralized area (see Figure 7) and the high values in the samples suggest there is or was a bigger contact zone than is presently exposed. The range of tungsten values in the panned concentrates from 7 drainages along the southwest side of the study area was 100-10,000ppm. The 50ppm tungsten in sample 1256 was the only tungsten value detected in a rock sample from this area.

Within the same locality mercury was detected as visable cinnabar in a panned concentrate (sample 130) collected from a drainage below a prospect later

identified as the Bluff Mercury Mine (Baker 1964). The Bluff workings consist of dozer cuts, pits and an old shallow shaft that expose thin beds of jasperoid and gossan along a N70W structure. The zone is exposed across about 50' of width along the side of an outcrop of silicified limestone. Sample 1965 of the jasperoid and gossan material ran 5.6ppm in mercury and was also anomalous in Mn and Ba. This site was the only mercury occurrence found in outcrop. However, anomalous mercury was detected in 36 other stream drainages originating from within the Silver Peak caldera. Nearly every drainage sampled on the western side of the range had anomalous mercury. Six of these drainages had values that were greater than 10ppm mercury. It is interesting to note that neither mercury nor tungsten were previously reported to be present in the district or in the study area.

The Pyramid Ranch claims in section 17 are about 4 miles south of the Bluff Mine and, are the site of an active mining operation which includes a small open-pit and extensive trenching. The open-pit was part of an earlier turquoise operation while current work is thought to be directed at precious metals. The workings are in thin bedded limestones and shales of the Palmetto Formation of Ordivician age that have been intruded by small diorite (?) stocks. The sediments are highly deformed and fractured. Small turquoise clots were observed in dark gray-black shale. Sample 1971 of this material ran high in Cu, Ba and V with lessor amounts of As, Cr, Ni and Y. Sample 1972 taken from highly altered and distorted sediments along a fault structure, yielded anomalous Cu, Ni, Zn and Ba. Sample 1973 taken from prospects in the same claim group had only low grade mineralization. Two of the three samples from these claims had low concentrations of silver but all of the samples were high in mercury.

The Aztec claims are about two miles northeast of the Pyramid claims and consist of a minor prospect along highly irregular quartz veins in argillite-slate. Sample 1256 was iron-stained vein material consisting of quartz and calcite that had low values for Cu, Pb, Ni and W, but fairly high values for Ba, Mn, Sr and V.

Another group of unnamed prospects is located about 1.4 miles northwest of McAfee Canyon. The workings are not identified on the Piper Peak 15' map nor are there any roads to the site. There is a shaft that may exceed 100', several adits as well as prospect-pits along N70-80W structures that have served as conduits for aplite (?) and felsic veins and or dikes. The host rocks are sandstone and limestone of the Cambrian Harkless Formation. Locally the outcrops are gossan-like with highly oxidized, iron-stained vein material. A wide variety of vein material was sampled including dump and outcrop material (Sample 1967) which was high in Zn (1000ppm) with lessor amounts of Ba and Mn and a trace of Ag. Local drainages included sample sites 134, 135, 136, 137 which were high in Pb, Hg and W.

The most recent staking noted on the western side of the range was in the area of the Dyer Shaft (notice dated 1980) where recent flagging gave evidence of a sampling project covering the old mine area. There also has been extensive staking on the western side of the range near the mouth of McAfee Canyon. No work was in progress at the time the area was visited in April 1984.

RED MOUNTAIN DISTRICT

The Red Mountain district, a rectangular strip of land about 1.5 miles wide and 4 miles long, extends from the crest down the eastern flank of the Silver Peak range. The Mohawk, Sanger and Silver Queen mines are on the west end of the district and the Nivloc is on the east end with the Sixteen-To-One in between. The district has production and reserves totaling about 14,500,000 ounces of silver and 45,000 ounces of gold from the Mohawk, Nivloc and Sixteen-To-One (Baker, 1982). Keith (1977, p. 38) includes 24,000 lbs of lead, 8,000 lbs of zinc and 700 lbs of copper with the earlier gold-silver production. The mines are aligned in a northwesterly direction which is thought to correspond to the early Pliocene trough from which the Silver Peak caldera erupted (Albers and Stewart, 1972).

The older volcanic rocks in the district are predominately andesites while the younger units are mostly rhyolite and latite with small plugs and dikes intruding the entire sequence. Rhyolites form the host rocks in the upper levels of the eastern mines but andesites dominate the lower levels at the Sixteen-To-One. On the eastern side of the district the Nivloc mine is reported to have encountered Paleozoic sediments at a depth of 300 feet and these rocks formed the host for much of the ores there (Baker, 1982). All the western mines are hosted in porphyritic latite that caps the ridges to the west. Lying uncomfortably on the latite, waterlaid and airfall tuffs fill local basins within and northwest of the caldera rim. In the northwest portion of the district these sediments have been cut by manganese rich quartz veins which contain precious metal values.

The dominate structural features in the Red Mountain district are the Silver Peak caldera to the west and a northeasterly-striking fault system which cuts both caldera and adjacent older rocks. The faults, which have acted as conduits for later vein emplacement, trend N20^{o}-70°E and dip at angles in excess of 55 degrees.

With the exception of the Nivloc, all of the mines are hosted in volcanics and are developed on epithermal veins formed along the northeasterly structures. The veins are vuggy, open-filling, fissure type veins with banded quartz and calcite and lessor amounts of barite and siderite. The veins, associated faults, and wallrocks show varying degrees of brecciation and alteration (argillization, silicification). The widths of the veins range from five feet at the surface to 50 feet at the deeper levels of the Sixteen-To-One and average close to 22 feet for the entire Sixteen-To-One orebody according to Young (1983) of the Sunshine Mining Co. These dimensions are very similar to the Mohawk vein where 40' widths existed below vein outcrops which were no more than several feet wide. At the Mohawk mine, leaching has removed most of the silver values and some of the gangue minerals at outcrop leaving behind only vuggy, manganese-rich quartz. Silver values in some of the stopes ranged from a few ounces at the surface to 40 ounces at 100 or more feet below surface.

Another characteristic of vein systems in the district is the lack of visible metallic mineralization especially in the upper levels of the mines. In the case of the Mohawk and Sanger mines, even the high-grade ores rarely have a visible silver mineral. Baker (1982) reported argentite and native silver as the dominate silver minerals. A more detailed account by Young (1938)

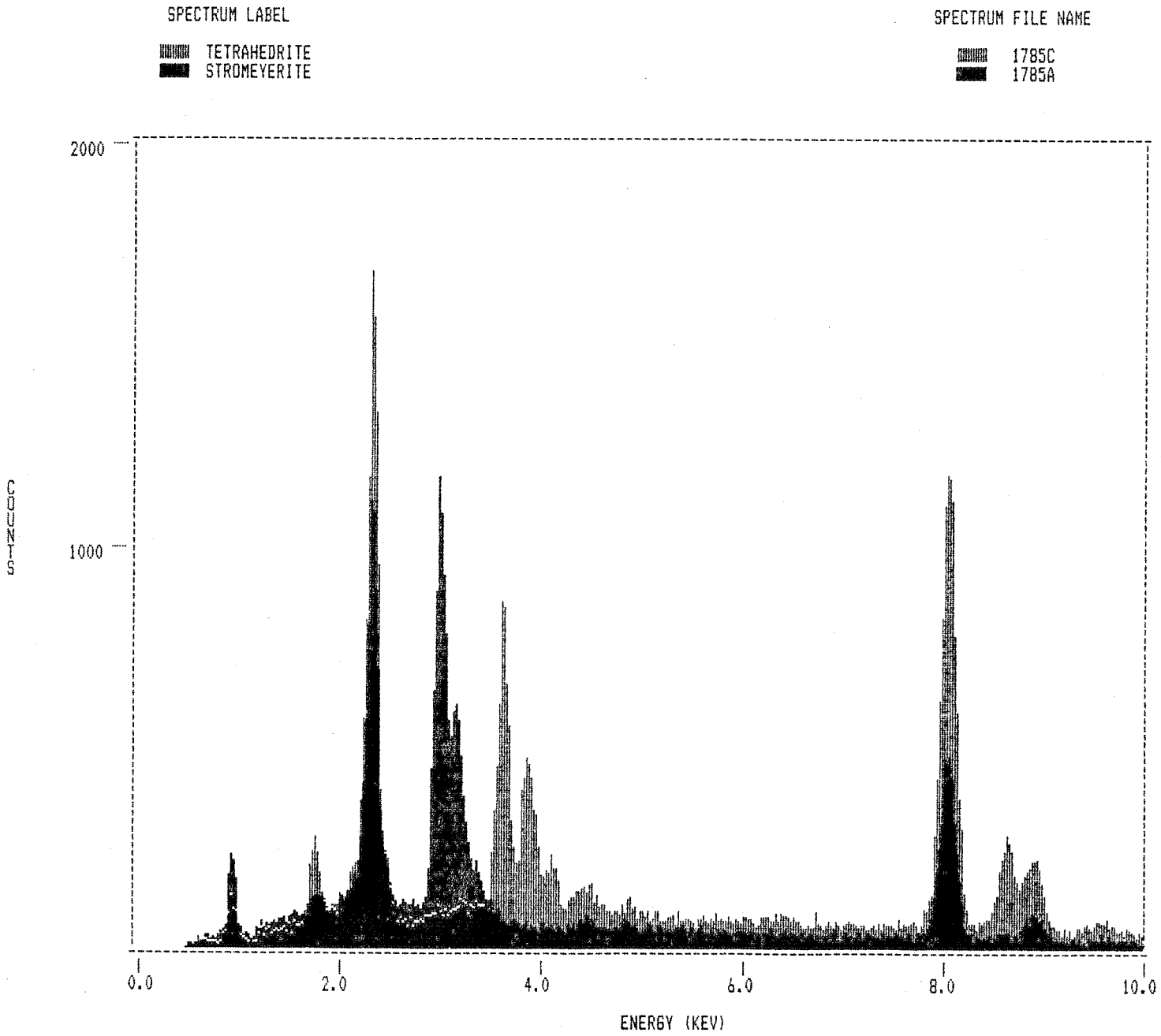
describes the precious metals of the Sixteen-To-One as predominately argentite (acanthite), with lessor amounts of the ruby silvers, proustite, and pyrargyrite. Additional silver minerals were tentatively identified microscopically as polybasite, stephanite, tetrahedrite and stromeyerite. Young also described native silver as wire and flakes in the upper workings and the gold as probably native gold but he had only seen it once in a thin section. He also reported base metals, especially in the lower mine levels, consisting of galena, spalerite and chalcopyrite. Mercury, antimony and arsenic have not been found in the ores of the Sixteen-To-One in significant amounts.

Early during this project, we took a sample (1785) of ore from the Sanger vein north and examined it on a microprobe (see Figure 6). From this single sample we were able to identify galena, argentite, chalcopyrite, tetrahedrite, and stromeyerite. Further, it is evident from the E-Spec data that individual elements existing in varying concentrations are present in all of the mines that would be necessary to evolve a similar complex mineralogical assemblage. Of much greater importance to this study, however, is the fact that many of these same elements were found to exist in anomalous concentrations in the drainage samples. We also found barite to be present in widths up to four feet thick in the Mohawk vein along with manganese up to 5 percent. Both of these elements are sparse in the eastern part of the district, but the eastern mines had the highest gold values. The Nivloc sample reported the highest average values at 0.05 ounces/ton.

All of the ground between the Sixteen-To-One and the mines to the west has been staked. The country northwest of the Mohawk-Sanger-Silver Queen mines is covered by claims for a distance of about 1.5 miles along the trend of the known district. Most of the claims are held by the Sunshine Mining Company. To the west of these claims and contigous on to them are the 93 claims of the Cabron group owned by Dr. Arthur Baker and Steven Bruff of Reno, Nevada. There are also many smaller claim blocks that fill in most of the rest of the area.

The Zombie Claims are located in the southwest portion of the district and consist of several shafts, adits, and prospects within a radius of about two-thirds of a mile. The western shaft is along a N20E, 60NW southern extension of the Mohawk vein. The vein is in a porphyritic latite near its contact with the older Rhyolite of Cottonwood Spring; both are of Tertiary age. The contact is brecciated, silicified, and displays strong iron staining. The mine workings are caved and inaccessable. The dump materials have no visible mineralization, and analysis showed only low metal values. At a prospect to the west, sample 1969 was taken from a brecciated quartz-calcite vein with mineralization within the matrix. The sample had high values for Ba, Mn, Sr and Ag (300ppm) with lessor amounts of Cu and Pb. Another of the Zombie shafts to the northeast was sunk on a small east-west trending vein in the older flows of the Rhyolite of Cottonwood Spring. A sample taken from the shaft dump yielded Ag (200ppm), high manganese, anomalous Pb, Zn, Cu, and minor Sb, and Ba. Stream drainages in the vicinity were high in Pb, Ba, and Sr and one drainage was very high in mercury.

As part of our background examination of the area, five of the six levels in the Mohawk mine were visited during a tour with the mine geologist. A major NE striking vein system in latite has been explored for about 1000 feet of strike length and for about 500 feet along dip. The dip of the vein were averages about 55° to the west. Individual veins expand and contract along strike,



PIGIT

Figure No. 6

reaching more than 40 feet thickness in some places, with good ore ranging from 5-6 feet in width. Samples 1988, 1989, 1990, 1991, 1992 and 1993 were collected at the outcrops and within the stopes at selected intervals. Silver values ranged from 7ppm at the surface to 300ppm in the Luft stope. All of the samples were anomalous in Mn, Ba, Sr and Ag, with lessor amounts of Pb, Zn and Cu and lower values for B, Be and Sb.

The Mohawk mine was discovered in 1920 and had its main period of operation in the late 1950's. Approximately 2,000,000 ounces of silver have been produced from this property to date and it contains another 95,000 ounces of reserves at 13 ounces per ton of probable and possible ore.

Less than a mile to the north of the Mohawk, the Inspiration Mining Co. is operating a six man crew, developing and mining the Sanger Mine. Work is being done at both ends of two parallel veins; the Footwall vein, narrow and of slightly higher grade, and the main Sanger vein, wider, longer and of somewhat lower grade. Gangue minerals consist of barite, calcite and quartz with quartz usually carrying the best values. Sample 1979 is from the Footwall vein and consists of brecciated, iron-stained vuggy material that has very few visible metallic minerals in a matrix of quartz, calcite and barite. Argentite and barite were tentatively identified in hand specimens. Analysis showed Ag (500ppm), Ba, Sr and Pb were anomalous with lessor amounts of Mn, Cu and Zn. Sample 1980 is from the hangingwall-vein and had some clacite and barite but was mostly a brecciated and vuggy quartz with possible argentite. The analysis was high in Ag (200ppm), Ba, Sr and Pb, with lessor amounts of Cu, Zn and Mn. A high-grade stringer within the Sanger north vein was being developed in late spring that carried visible argentite, galena, and chalcopyrite. A fire assay of this sample 1785 and sample 1980 were made for comparative analysis with the E-Spec data. Sample 1980 asayed 57 ounces/ton using E-Spec data and 47 ounces using fire assay methods. The second sample was selected for micro-probe work and was described earlier.

About a half mile NE of the Sanger is the Silver Queen mine. The workings consist of a shaft that was sunk on a N35E striking vein that has a vertical dip and is hosted in the latite. The vein has been exposed to the northeast of the shaft by a series of dozer-cuts along a road. A 650' crosscut was driven from the west perpendicular to and several hundred feet below the shaft. The dump in front of the cross-cut shows very little vein material suggesting that the vein was not intersected at depth, although an underground investigation was not made to confirm this.

Samples from the shaft (1978) and from the exposed portion of the vein in the road-cut (1977) were anomalous in Ag (1500ppm) and (200ppm) as well as B, Sr, Mn, Pb, Zn, Cu, Hg, with lessor amounts of As, Sb and Be. Stream sediment samples from this area sampled drainages below the Tonopah Tunnel and the Silver Queen mine. Analysis from panned concentrates at these locations were high in Hg, Ba, Sr and Y, with lessor values for Pb and Mn.

The Tonopah Tunnel is about one-third of a mile to the NE of the Silver Queen mine and may be on the same vein. The workings consist of two adits driven by the Tonopah Mining Co. in 1935 on one of a series of NE trending veins that can be traced on the surface diagonally thru sections 30 and 19. This particular set of veins was mapped by Stewart (1974) as being inside the Silver Peak caldera. The lower tunnel or adit is 650 feet long and was driven on a vein

that strikes N35^{o}E and dips close to vertical. The vein is 3-4 feet wide at the surface and forms bold outcrops as it crosses the canyons and ridges. At the surface the vein is reddish-brown, gossan like, highly silicified and brecciated with prismatic crystals of barite up to 1/2 inch in length within the matrix. Brecciation extends 5-6 feet into porphyritic latite and along both sides of the vein. Sample 1976 was selected from within the adits and from the upper dump. Analysis of the sample showed high values for Ag (500ppm), Ba, Pb, Zn, Cu, Hg, Sr, with lessor values for antimony and tungsten.

The Black Rock manganese prospects are a series of trenchs, prospects and a small shaft on pipe-like or vein-like bodies cutting tuffaceous lake beds within the porphyritic latite. Some of the vein material is manganese rich chalcedony, other is a vuggy manganese rich quartz. Samples 1981, 1982 and 1983 were taken from these workings and were found to be anomalous in Mn, Ba, Hg and Sb, with minor Ag (except sample 1983 which had 100ppm silver). Sample 1981 had .4ppm gold. Panned concentrate samples from drainages in this area were anomalous in Ba, Mn, Pb, Hg, Sr, Y, with minor Zn and Y. Most of this drainage system is in and along the margins of Argentite Canyon.

A small shaft and bulldozer cuts were examined in the NW 1/4 of section 19, about a half mile NE of Argentite Canyon on the Patience Claims of the Sunshine Mining Co. The shaft is on a N40E structure next to an exposed vein the dozer cut. The exposed vein is 25 feet wide and is hosted in rhyolite flows which are just north of the Silver Peak caldera rim. Visible mineralization includes copper oxides and barite. The vein consists of iron- and manganese-stained, vuggy, and in part gossan-like silica-rich material with brecciation near the margin and into the wall rock. A sample was taken from the dump near the shaft from and the adjacent exposed vein. Analysis of the sample (1987) suggest primary and secondary enrichment of the vein may have occurred. The sample was anomalous in Au (4.2ppm), Ag (700ppm), Hg, Mn, As, Sb, Ba, Cu, Sr with minor Pb, Zn, B and Be. Panned concentrate samples from this area were very high in Hg and anomalous in Pb, Sr, Y and Ba.

In a steep drainage about 150 yards southwest of Argentite Canyon a small unnamed mine was found and examined. Here an 80 foot main adit intercepts a NE-trending vein that outcrops above the workings. A parallel adit off a second drift has a 30 foot winze which follows the vein. Sample 1985 was taken from the vein next to the winze and had 3.2ppm gold. Sample 1986 was taken where the vein was cross-cut in the main adit. Analysis of the quartz vein showed anamalous Mo, Hg, Ba and minor Ag. Panned concentrates from nearby Argentite Canyon were anomalous in Ba, Mn, Pb, Hg, Sr, Y and with minor Zn and Ag.

MINERAL RESOURCE AREAS, LAND CLASSIFICATION

Dyer District:

The geochemistry of the Dyer district shows a distinct base-metal, precious-metal mineralization associated with quartz veins along NW structures. Elements of the same mineralization, especially lead and mercury, are associated with similar rocks and structures and can be extended along the entire western side of the WSA (see Figures 7, 8, 9, 11, 12, 14, 15, 18, 19).

A second very distinct mineral association between tungsten and skarn deposits can be made for the same area. The proximity of the older sediments to granitic rocks is apparent; the location of tungsten mineralization is not apparent. The tungsten anomalies extend for over five miles down the western side of the range and involve five major drainages. The unknown source or sources of tungsten are from the east in the direction of the WSA (see Figure 7).

Six different drainage systems along the same (western) side of the range are anomalous in mercury, one drainage hosts a known mercury deposit. Some anamalous drainages originate far to the east, well within the WSA and near the western boundary of the Silver Peak caldera. The presence of anomalous mercury in these drainages could very well indicate the presence of undiscovered precious metal deposits somewhere in the area served by the drainage system (see figures 8, 17).

Based on our examination of the Dyer district and on the results of sampling of the drainages in the area, we have classified a large area northwest of McAfee Canyon, along the west side of the WSA (Area M-3, Figure 21) as 3-C based on the BLM classification scheme (see Appendix A).

Red Mountain District:

The correlation between the geochemistry and mineralization of the precious-metal deposits of the Red Mountain district and their relationship to the Silver Peak caldera has been made. What may not be apparent but must be considered is the possibility that mineralization might be present in the NE-SW structures that pass to the southwest, thru the Carbron Claims, and extend on, into the WSA. These structures are parallel to mineralized NE-trending structures outside of the WSA, and they have geochemical anomalies associated with them that are similar to the mineralization in the Red Mountain deposits. One small mine with known precious-metal mineralization (sample 1985) is located within or on one of these structures (see Figures 8, 9, 10, 11, 14, 15, 17, 19, 20 and the Geologic Map for the quadrangle by Stewart, 1974).

Anomalous gold values were found in the sample taken from the Black Rock and Patience Claims (samples 1981-1987). This may represent a new area of gold mineralization as heretofore it was thought that gold occurred only to the east in the district. Along with gold, high values were reported for antimony and arsenic, otherwise the mineral assemblage correlates with the rest of the Red Mountain district. This is a small area and values are from rock samples so it is difficult to expand the anomalous area in any specific direction. It is not clear how this anomaly relates to the WSA, but its presence on the margin of the area needs to be considered.

Based on examinations made in the Red Mountain district, and on results of sampling of the drainages between Argentite Canyon and Icehouse Canyon, we have classified a large area northeast of Icehouse Canyon (Area M-2, Figure 21) as 3-C following the BLM classification scheme (see Appendix A). A smaller area south of Mud Springs (Area M-1, Figure 21) has been classified 4-D based on its proximity to known mines to the east.

The only localized area within the WSA without apparent mineralization exposed at surface or revealed by samples from drainages which cut it is in the southeastern quarter especially along the eastern end of McAfee Canyon. This area is covered by a thick layer of air-fall and ash flow tuffs that have no apparent mineralization. This area (Area M-4, Figure 21) has been classified as 2-C following the BLM scheme (see Appendix A).

SUGGESTIONS AND RECOMMENDATIONS

1. If further clarification of our data would be helpful we would be willing to make a traverse of the area with the BLM area geologist.

2. Follow-up sampling of the mercury and tungsten anomalies defined on the west should be done by traversing the two most promising drainages.

3. Examine the area at the head of Icehouse Canyon or west of Mud Springs and trace the trend of the NE structures to see if they extend into and are mineralized within the WSA.

4. Trace the drainage south from Cave Spring along the NE structure and sample the interior drainage.

5. Try to trace the Patience Claim-Black Rock gold mineralization into the WSA. A single traverse from the Black Rock deposits down the NE structure to the WSA on the south should be made.

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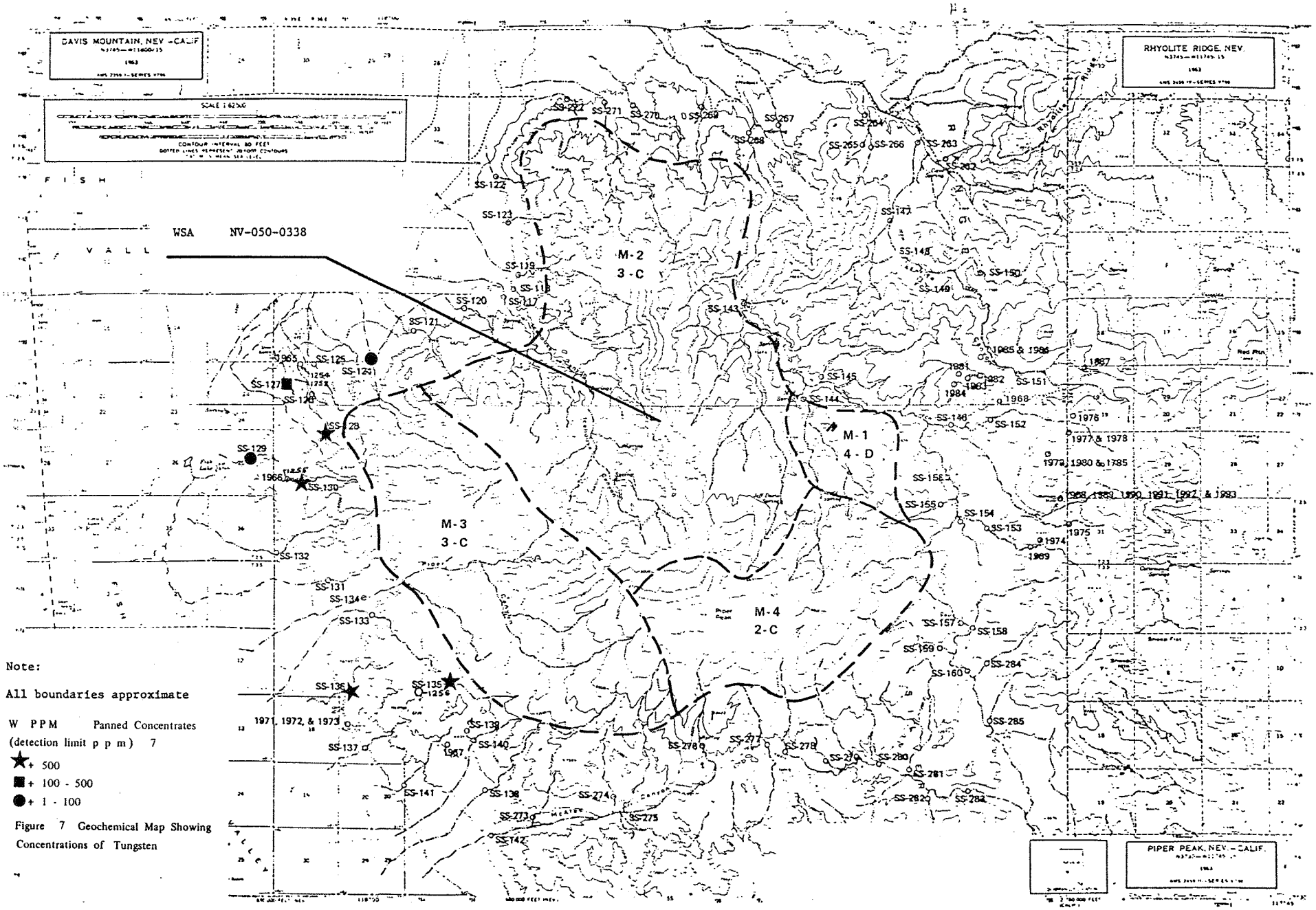


Note:

All boundaries approximate

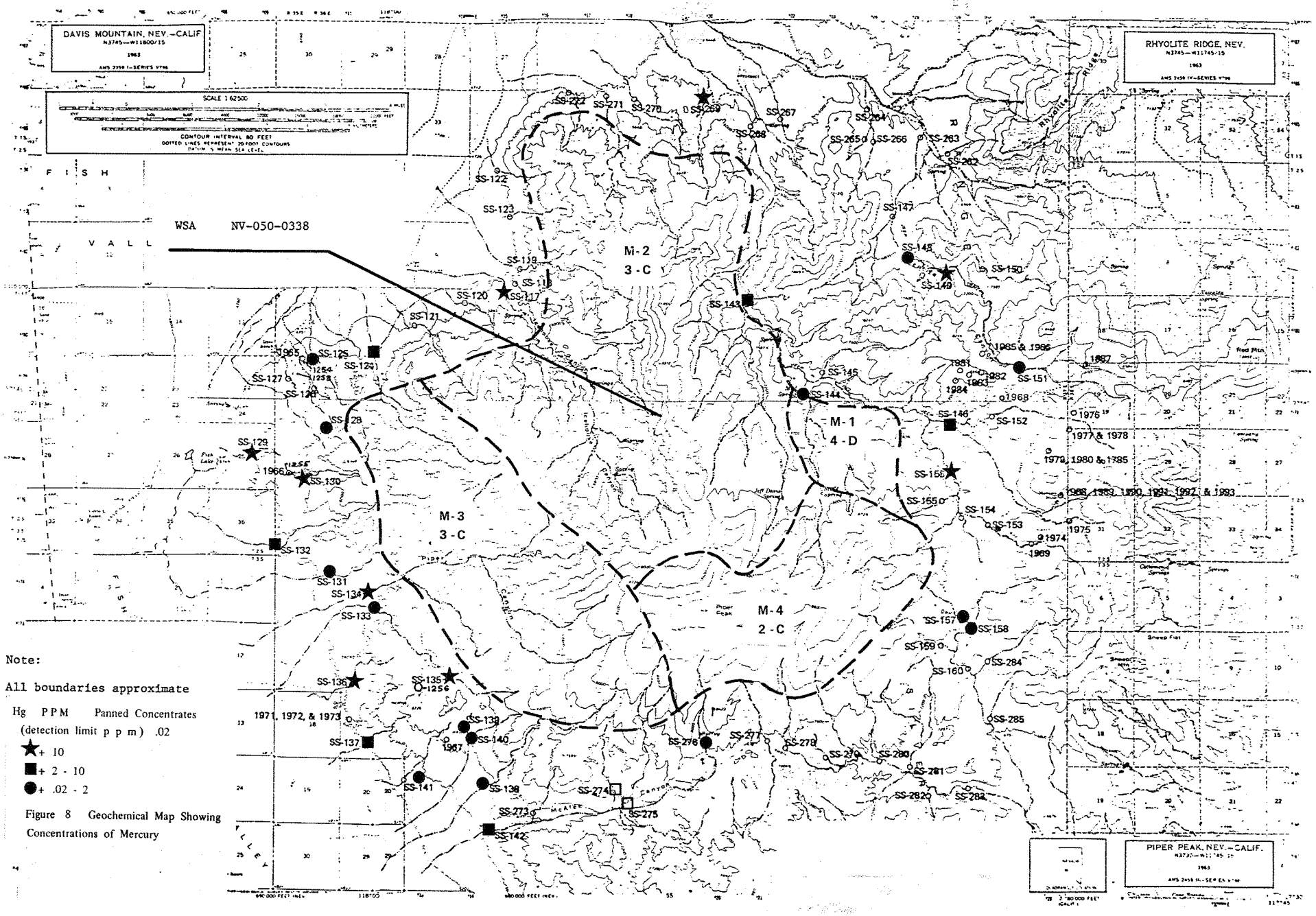
W PPM Panned Concentrates (detection limit p p m) 7

★ + 500

■ + 100 - 500

● + 1 - 100

Figure 7 Geochemical Map Showing Concentrations of Tungsten



Note:

All boundaries approximate

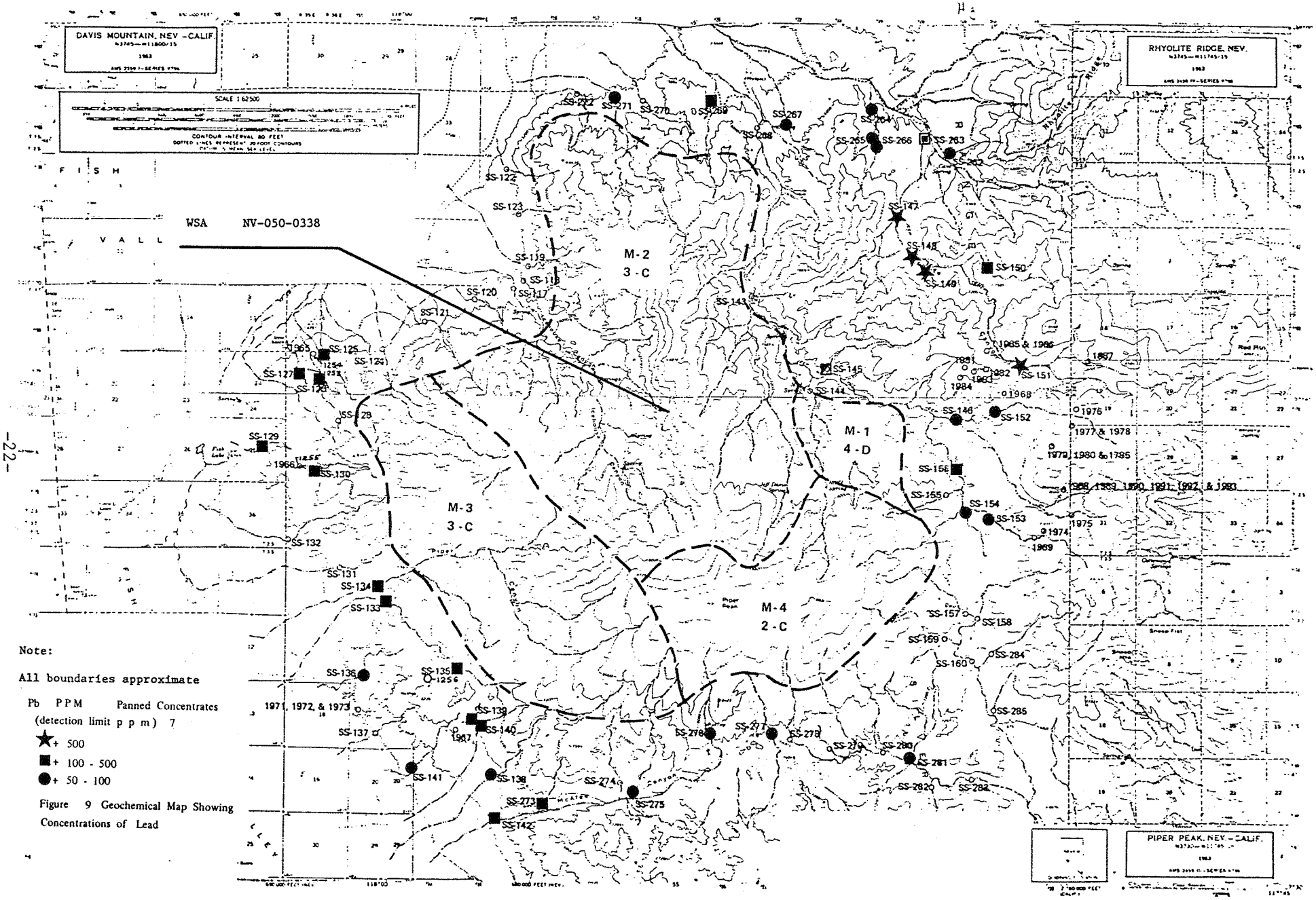
Hg PPM Panned Concentrates (detection limit p p m) .02

★ + 10

■ + 2 - 10

● + .02 - 2

Figure 8 Geochemical Map Showing Concentrations of Mercury



Note:

All boundaries approximate

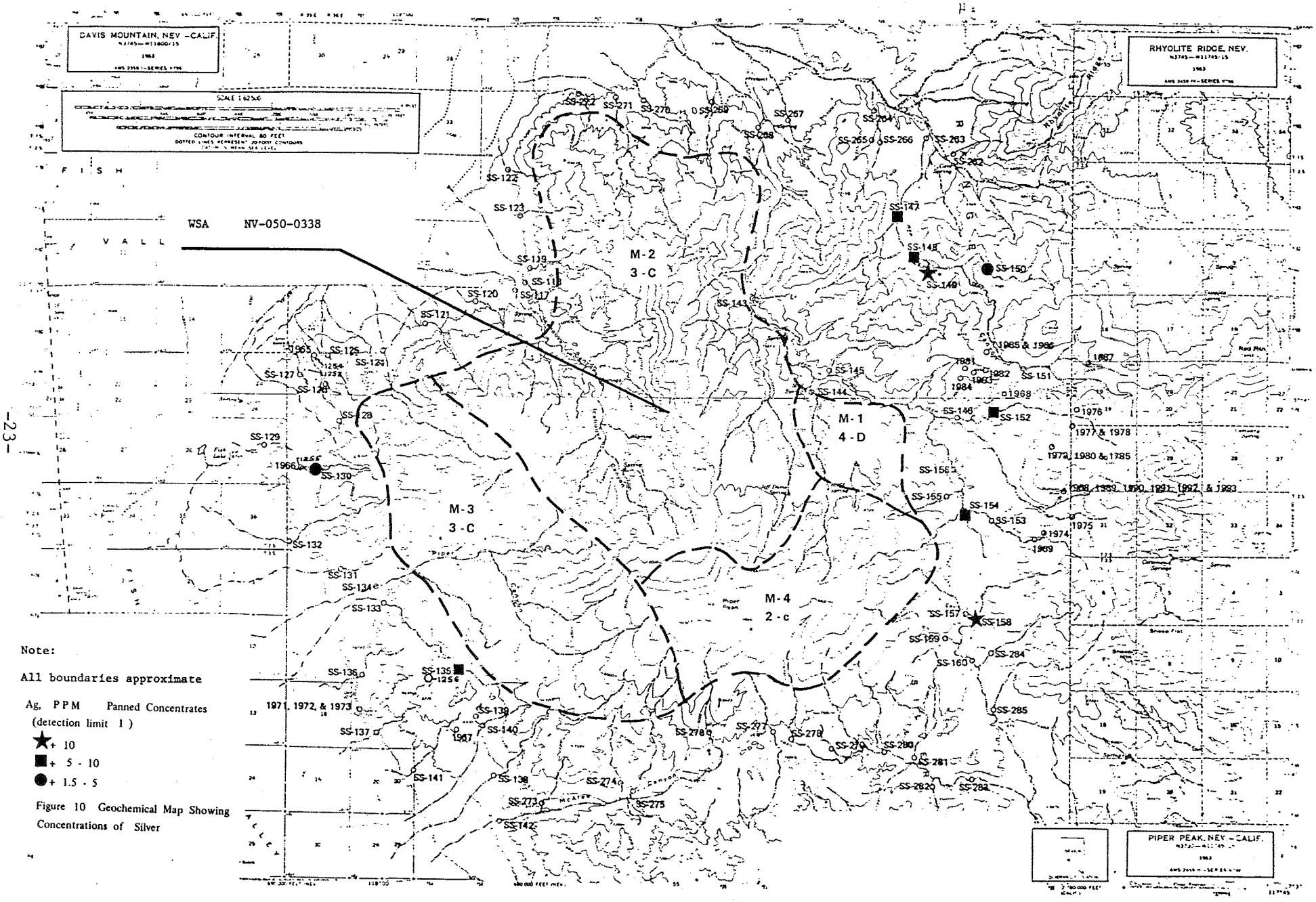
Pb PPM Panned Concentrates (detection limit p p m) 7

★ + 500

■ + 100 - 500

● + 50 - 100

Figure 9 Geochemical Map Showing Concentrations of Lead



Note:

All boundaries approximate

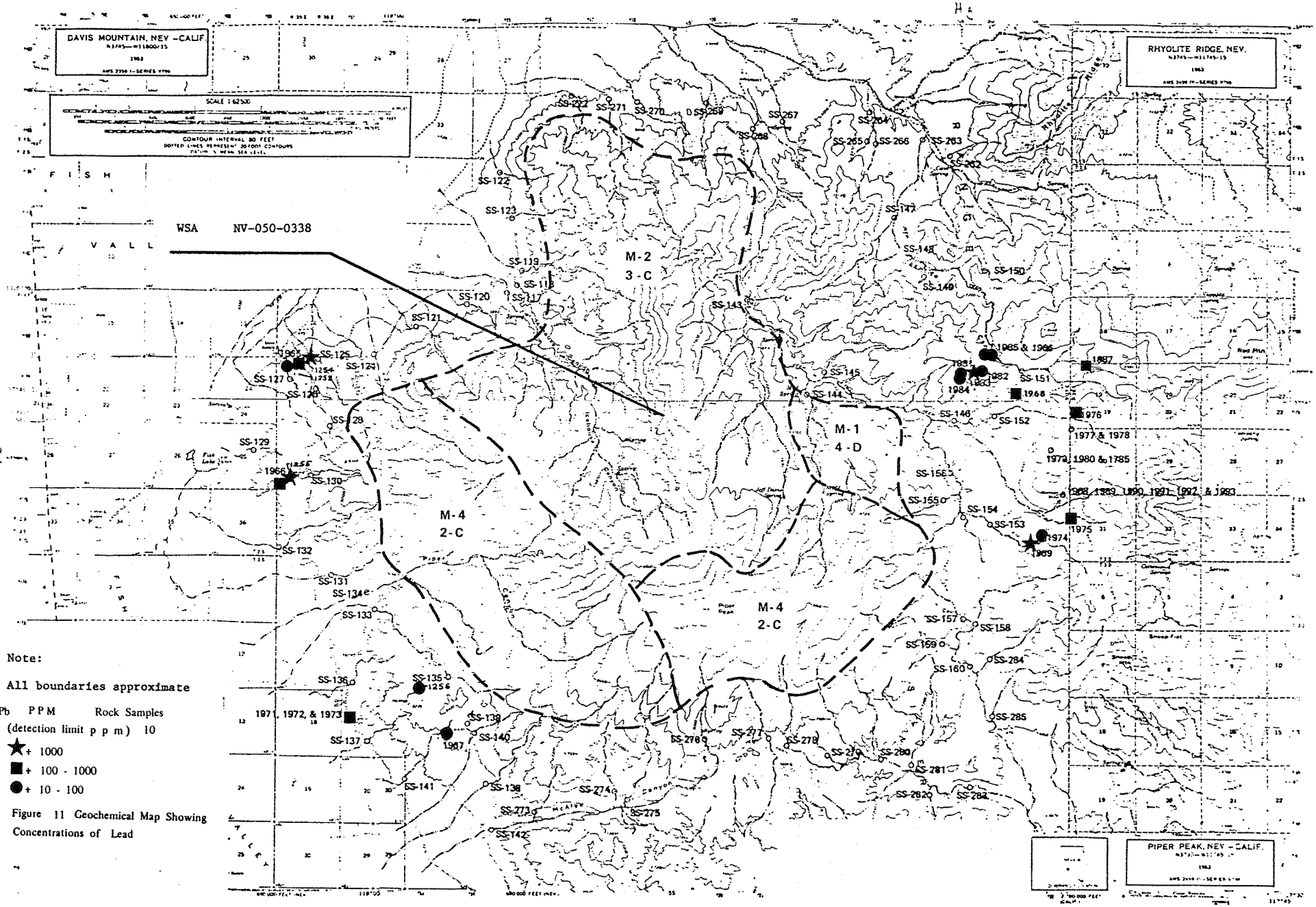
Ag, PPM Panned Concentrates
(detection limit 1)

★ + 10

■ + 5 - 10

● + 1.5 - 5

Figure 10 Geochemical Map Showing Concentrations of Silver



Note:

All boundaries approximate

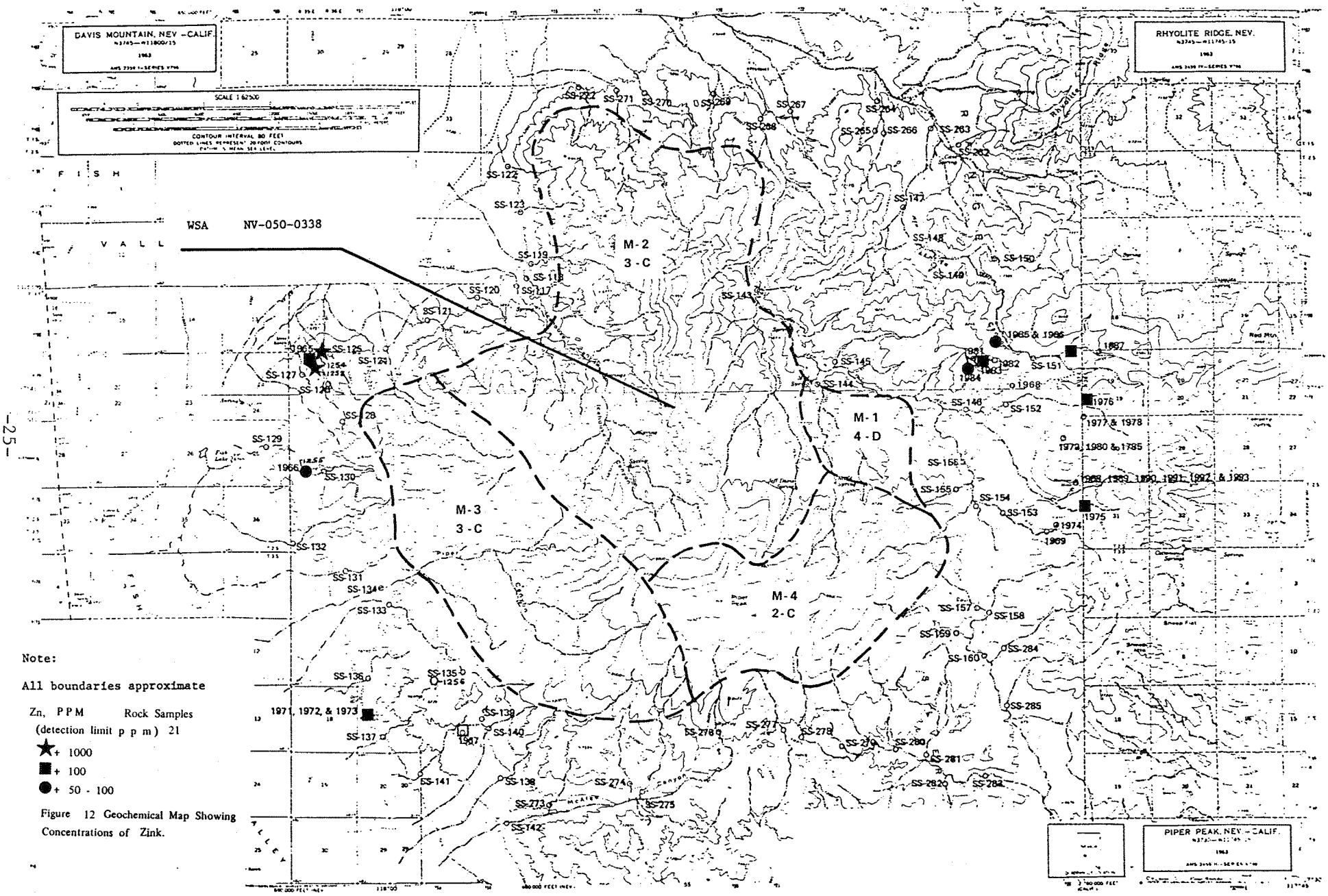
Pb PPM Rock Samples
(detection limit p p m) 10

★ + 1000

■ + 100 - 1000

● + 10 - 100

Figure 11 Geochemical Map Showing Concentrations of Lead



Note:

All boundaries approximate

Zn, PPM Rock Samples
(detection limit p p m) 21

★ + 1000

■ + 100

● + 50 - 100

Figure 12 Geochemical Map Showing Concentrations of Zink.

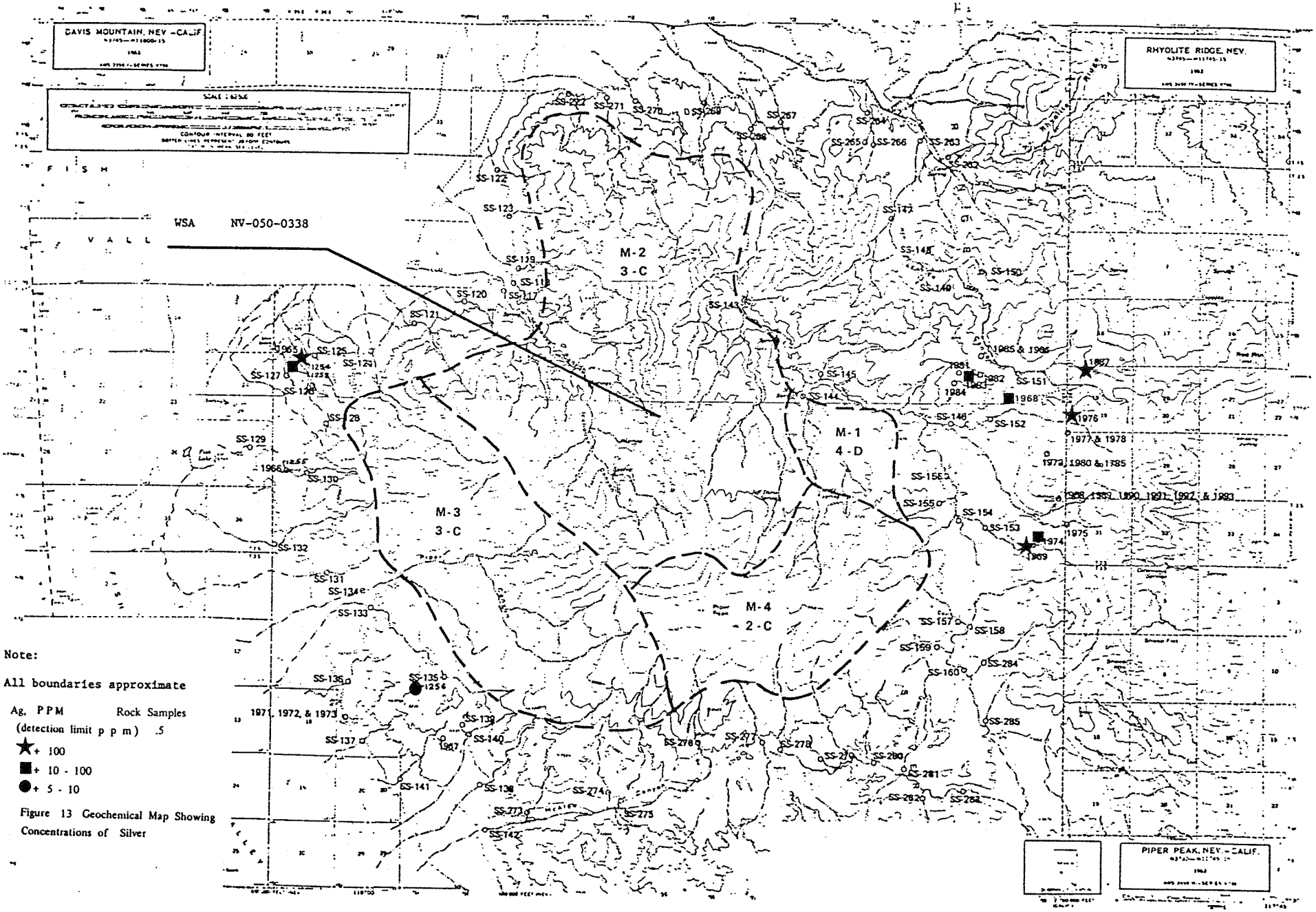
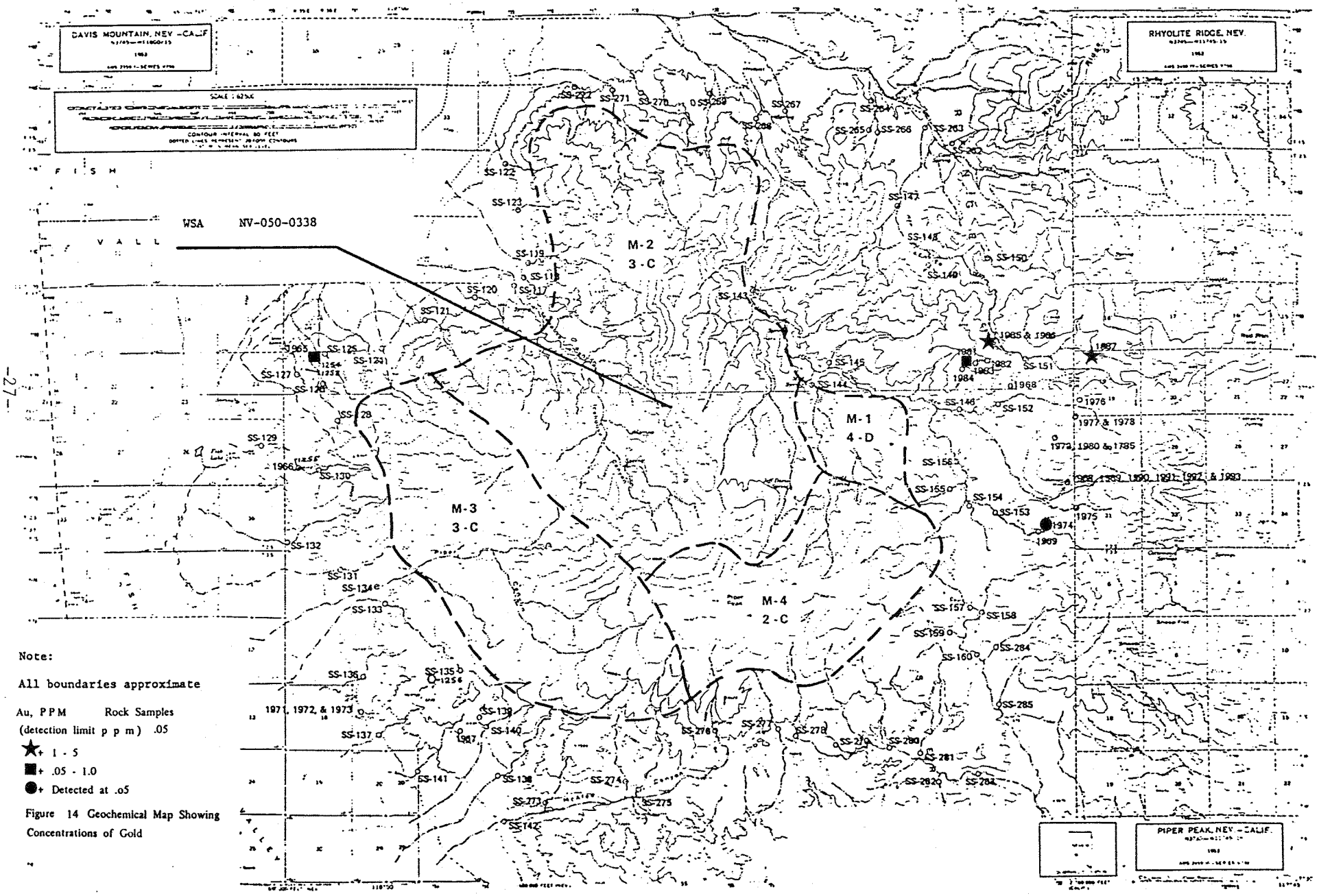


Figure 13 Geochemical Map Showing Concentrations of Silver



Note:

All boundaries approximate

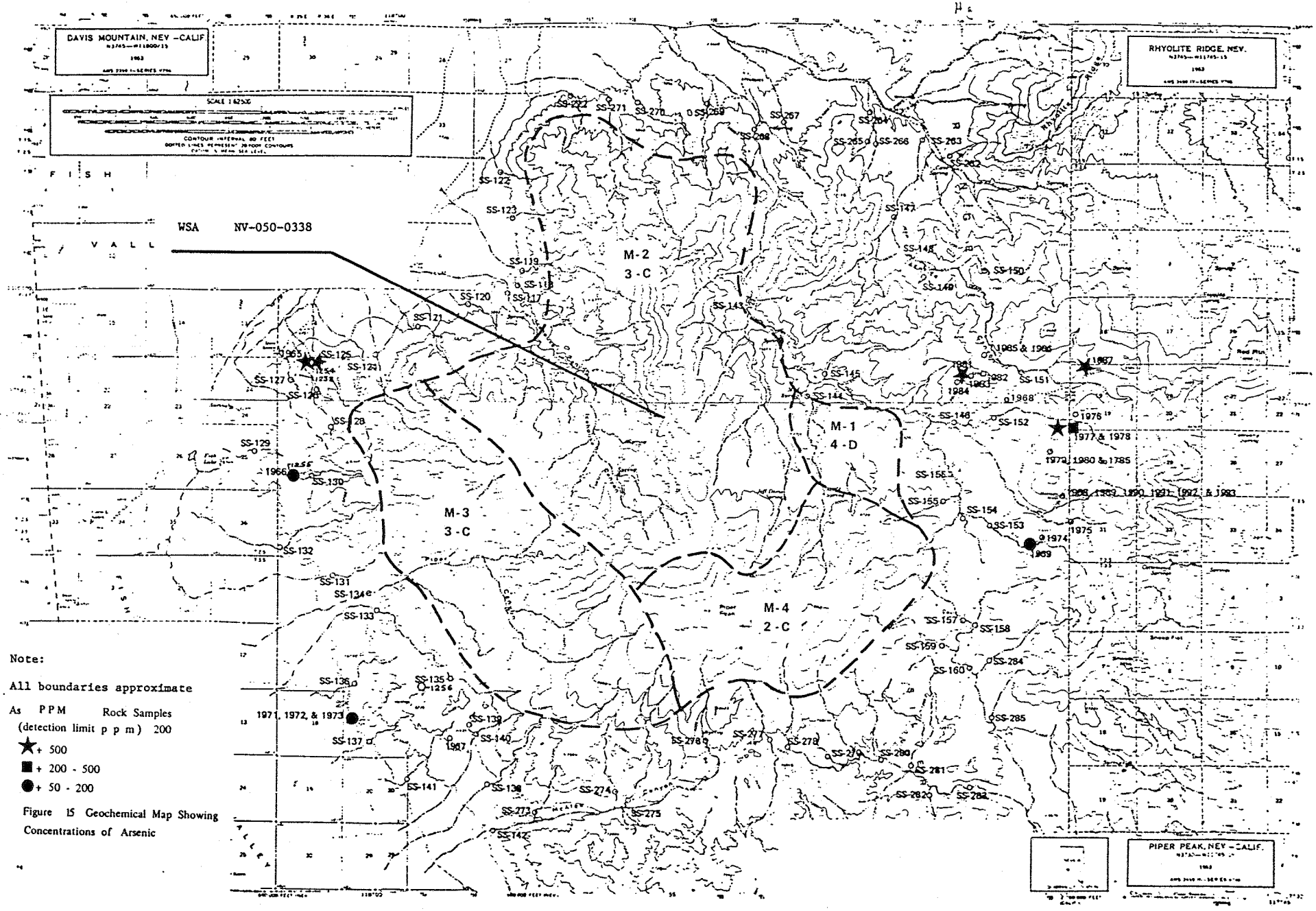
Au, PPM Rock Samples
(detection limit p p m) .05

★+ 1 - 5

■+ .05 - 1.0

●+ Detected at .05

Figure 14 Geochemical Map Showing Concentrations of Gold



Note:

All boundaries approximate

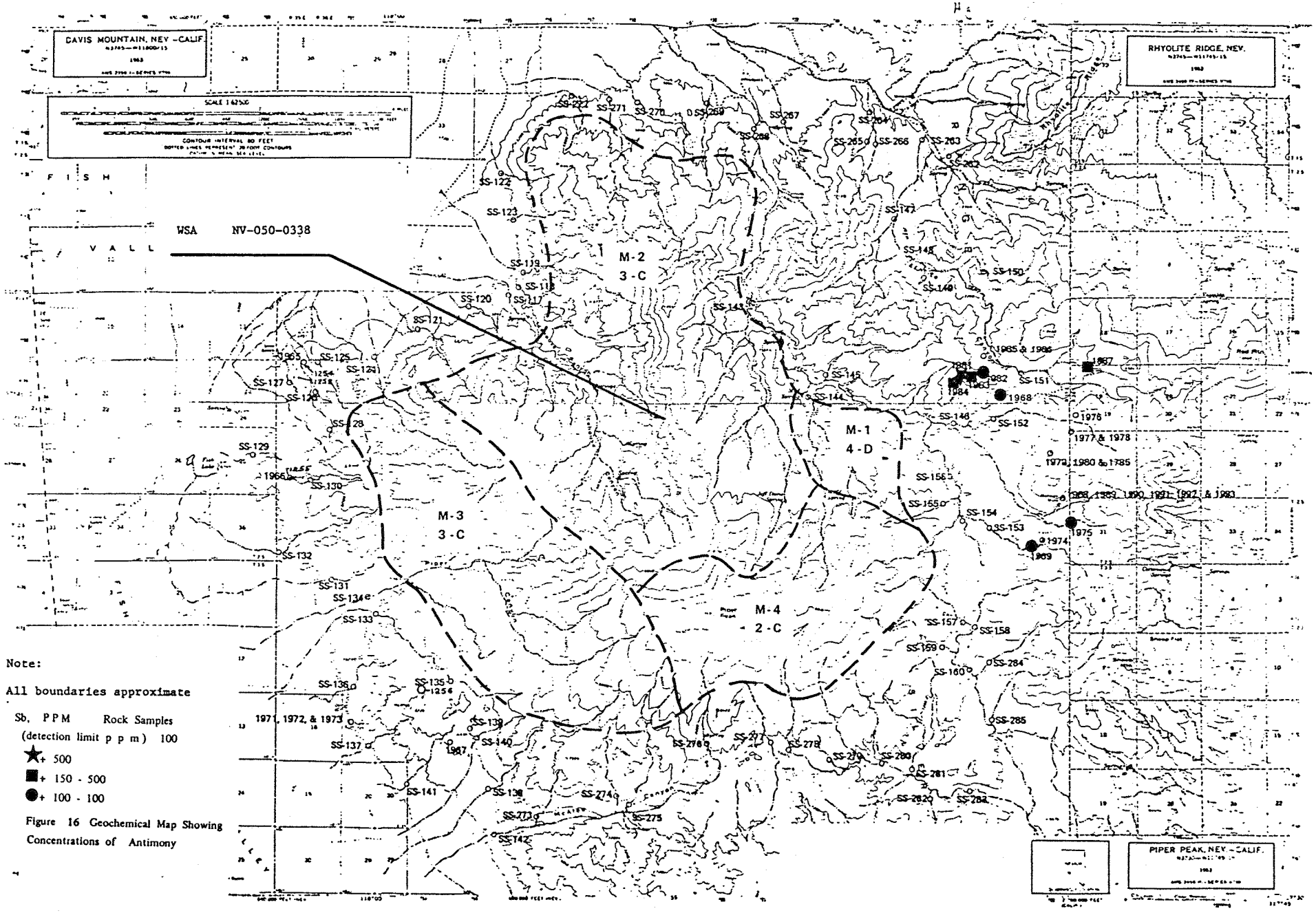
As PPM Rock Samples
(detection limit p p m) 200

★ + 500

■ + 200 - 500

● + 50 - 200

Figure 15 Geochemical Map Showing Concentrations of Arsenic



Note:

All boundaries approximate

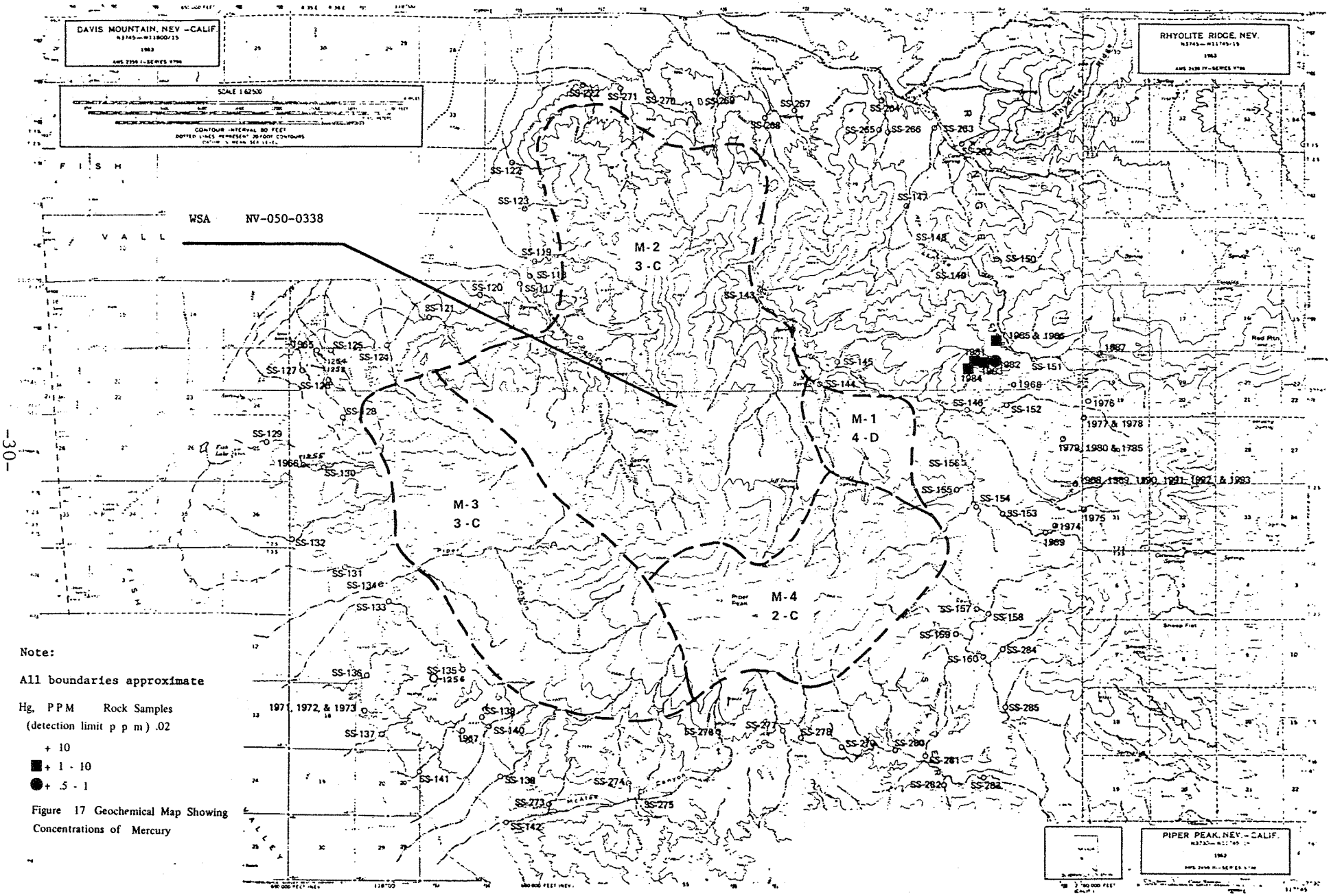
Sb, PPM Rock Samples
(detection limit p p m) 100

★ + 500

■ + 150 - 500

● + 100 - 100

Figure 16 Geochemical Map Showing Concentrations of Antimony



Note:

All boundaries approximate

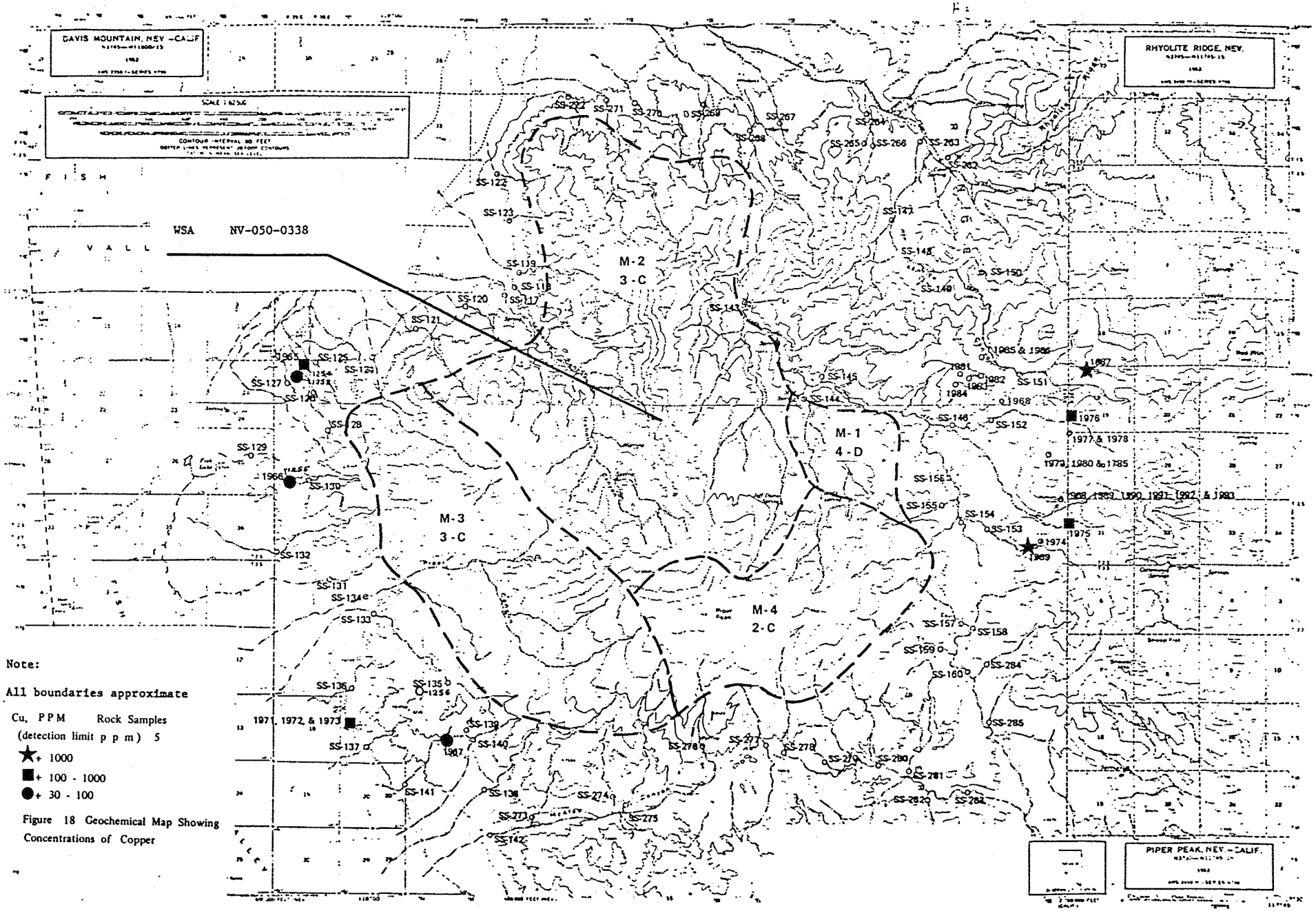
Hg, PPM Rock Samples
(detection limit p p m) .02

+ 10

■ + 1 - 10

● + .5 - 1

Figure 17 Geochemical Map Showing Concentrations of Mercury



Note:

All boundaries approximate

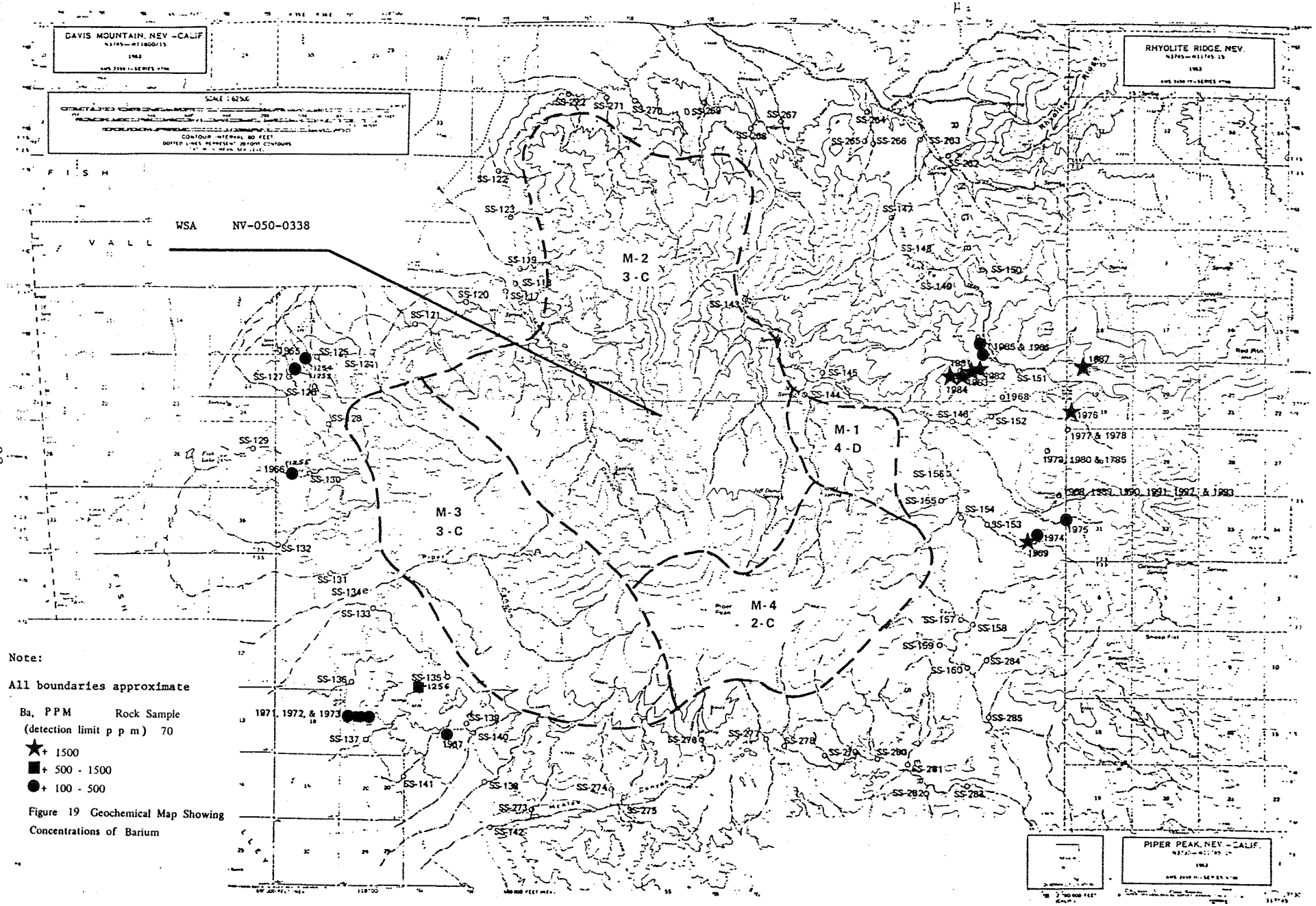
Cu, PPM Rock Samples
(detection limit p p m) 5

★ + 1000

■ + 100 - 1000

● + 30 - 100

Figure 18 Geochemical Map Showing Concentrations of Copper



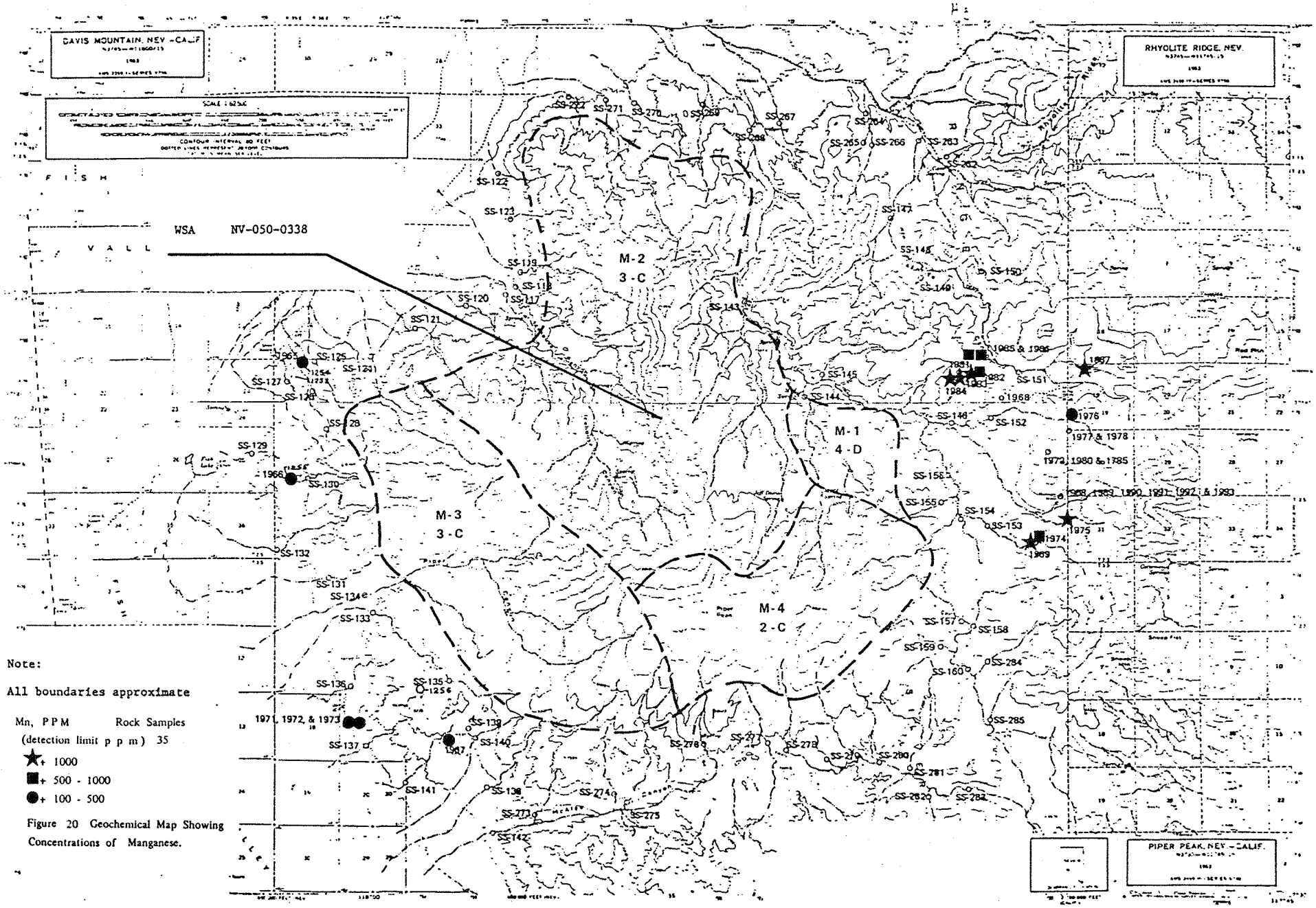
Note:

All boundaries approximate

Ba, PPM Rock Sample
(detection limit p p m) 70

★ + 1500
■ + 500 - 1500
● + 100 - 500

Figure 19 Geochemical Map Showing Concentrations of Barium



Note:

All boundaries approximate

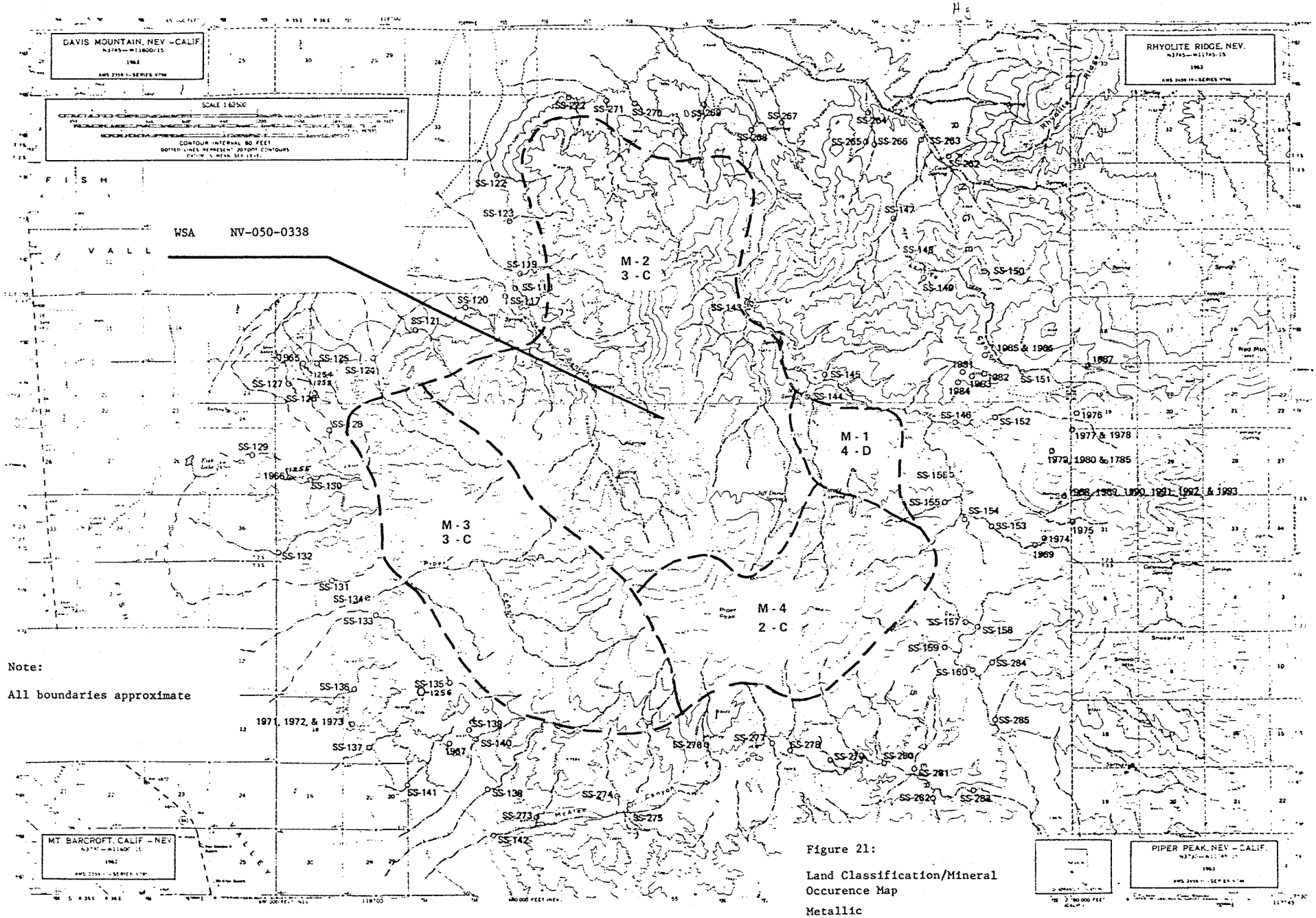
Mn, PPM (detection limit p p m) 35 — Rock Samples

★ + 1000

■ + 500 - 1000

● + 100 - 500

Figure 20 Geochemical Map Showing Concentrations of Manganese.



Note:

All boundaries approximate

Figure 21:

Land Classification/Mineral Occurence Map

Metallic

APPENDIX A

CLASSIFICATION SCHEME

1. The geologic environment and the inferred geologic processes do not indicate favorability for accumlation of mineral resources.

2. The geologic environment and the inferred geologic processes indicate low favorability for accumulation of mineral resources.

3. The geologic environment, the inferred geologic processes, and the reported mineral occurrences indicate moderate favorability for accumulation of mineral resources.

4. The geologic environment, the inferred geologic processes, and the reported mineral occurrences, and the known mines or deposits indicate high favorability for accumulation of mineral resources.

LEVEL OF CONFIDENCE SCHEME

A. The available data are either insufficient and/or cannot be considered as direct evidence to support or refute the possible existence of mineral resources within the respective area.

B. The available data provide indirect evidence to support or refute the possible existence of mineral resources.

C. The available data provide direct evidence, but are quantitatively minimal to support or refute the possible existence of mineral resources.

D. The available data provide abundant direct and indirect evidence to support or refute the possible existence of mineral resources.

Table 1 Data for stream sediment samples, Silver Peak Wilderness Study Area, Esmeralda County, Nevada
[N, not detected; <, detected but below the limit of determination shown; >, determined to be greater than the value shown.]

Sample	X coor-dinate	Y coor-dinate	Fe-pct. s	Mg-pct. s	Ca-pct. s	Ti-pct. s	Mn-ppm s	Ag-ppm s	As-ppm s	Au-ppm s	B-ppm s	Ba-ppm s	Be-ppm s	Bi-ppm s
SS117	41,500	418,100	2	.7	2.0	.30	500	N	N	N	30	700	1.5	N
SS118	41,520	418,100	3	1.0	2.0	.30	700	N	N	N	20	700	1.5	N
SS119	41,520	418,160	3	.7	1.5	.30	500	N	N	N	20	700	1.5	N
SS120	41,400	418,070	5	.7	1.5	.50	1,000	N	N	N	20	1,000	1.0	N
SS121	41,300	418,020	7	.7	1.5	.70	1,000	N	N	N	20	700	1.0	N
SS122	41,500	418,490	3	1.0	1.5	.30	700	N	N	N	30	1,000	1.5	N
SS123	41,580	418,280	3	.7	1.5	.30	500	N	N	N	30	1,000	1.0	N
SS124	41,160	417,940	5	.7	1.5	.30	500	N	N	N	15	700	1.0	N
SS125	41,040	417,940	3	.7	1.5	.50	500	N	N	N	30	500	1.5	N
SS126	41,020	417,870	3	.7	1.5	.30	500	N	N	N	30	500	1.5	N
SS127	40,980	417,890	3	.7	2.0	.30	500	N	N	N	70	500	1.5	N
SS128	41,060	417,760	3	.7	2.0	.30	300	N	N	N	50	300	1.0	N
SS129	40,690	417,710	3	1.0	3.0	.30	500	N	N	N	70	500	1.5	N
SS130	41,010	417,650	3	1.5	5.0	.30	700	N	N	N	30	300	1.5	N
SS131	41,060	417,400	2	.5	1.5	.30	500	N	N	N	30	500	1.5	N
SS132	40,940	417,480	3	.7	1.5	.30	500	N	N	N	30	500	1.5	N
SS133	41,170	417,320	3	.7	1.5	.50	500	N	N	N	30	500	1.5	N
SS134	41,150	417,360	3	.7	1.5	.50	500	N	N	N	50	500	1.5	N
SS135	41,138	417,160	2	.7	5.0	.30	300	N	N	N	100	500	1.5	N
SS136	41,130	417,150	3	.7	2.0	.50	500	.7	N	N	50	500	1.0	N
SS137	41,170	417,000	3	1.0	2.0	.30	500	N	N	N	50	500	1.5	N
SS138	41,450	416,690	2	1.0	7.0	.20	500	N	N	N	70	300	1.0	N
SS139	41,410	417,030	3	1.5	5.0	.30	500	N	N	N	30	300	1.5	N
SS140	41,444	417,040	2	.7	5.0	.20	500	N	N	N	50	500	1.0	N
SS141	41,250	416,920	2	1.0	5.0	.15	500	N	N	N	30	500	1.0	N
SS142	41,520	416,800	2	1.0	2.0	.30	500	N	N	N	50	500	1.5	N
SS143	42,080	416,040	3	.7	1.5	.50	700	N	N	N	30	700	1.5	N
SS144	42,220	417,660	2	.7	1.5	.20	500	N	N	N	30	700	1.5	N
SS145	42,290	417,900	3	.7	1.0	.30	500	N	N	N	50	700	1.0	N
SS146	42,350	417,770	3	.5	1.0	.50	1,000	.7	N	N	20	700	1.5	N
SS147	42,440	418,280	2	.7	1.5	.30	1,000	<.5	N	N	50	700	1.5	N
SS148	42,480	418,180	3	.7	1.5	.30	700	.5	N	N	30	1,000	1.5	N
SS149	42,510	418,120	3	.7	1.0	.30	1,500	1.0	N	N	30	1,500	1.5	N
SS150	42,650	418,130	3	.5	1.0	.30	1,000	.7	N	N	20	1,000	1.5	N
SS151	42,810	417,900	2	.7	1.0	.20	1,000	.5	N	N	30	1,000	1.5	N
SS152	42,670	417,780	5	.5	1.0	.30	1,000	.5	N	N	20	2,000	1.0	N
SS153	42,670	417,520	3	.5	1.5	.30	500	N	N	N	20	700	1.5	N
SS154	42,560	417,520	5	.7	1.5	.70	1,000	.7	N	N	20	700	1.0	N
SS155	42,560	417,580	2	1.0	1.5	.30	700	N	N	N	30	700	1.5	N
SS156	42,580	417,640	3	.7	1.5	.30	500	N	N	N	20	700	1.0	N
SS157	42,600	417,300	3	.7	1.5	.50	700	N	N	N	20	500	1.5	N
SS158	42,640	417,300	2	.5	1.0	.30	500	N	N	N	20	700	1.0	N
SS159	42,570	417,230	2	.7	1.5	.30	500	N	N	N	30	700	1.5	N
SS160	42,620	417,170	7	.7	1.0	.50	1,000	N	N	N	15	500	1.0	N

SS263	42,490	418,360	3	.7	1.5	.30	700	N	N	N	50	700	1.5	N

Table 1 Data for stream sediment samples, Silver Peak Wilderness Study Area, Esmeralda County, Nevada

Sample	Cd-ppm s	Co-ppm s	Cr-ppm s	Cu-ppm s	La-ppm s	Mo-ppm s	Nb-ppm s	Ni-ppm s	Pb-ppm s	Sb-ppm s	Sc-ppm s	Sn-ppm s	Sr-ppm s	V-ppm s
SS117	N	15	100	15	30	N	N	20	20	N	10	N	300	50
SS118	N	15	70	15	30	N	N	15	20	N	10	N	300	70
SS119	N	15	70	20	20	N	N	20	30	N	7	N	300	50
SS120	N	15	150	15	100	N	N	15	20	N	15	N	500	150
SS121	N	30	150	50	70	N	N	20	30	N	10	N	500	200
SS122	N	15	50	30	30	N	N	15	30	N	10	N	200	70
SS123	N	15	70	20	30	N	N	15	20	N	10	N	300	70
SS124	N	15	100	15	20	N	N	15	20	N	7	N	200	70
SS125	N	20	30	15	20	5	N	20	30	N	10	N	200	50
SS126	N	15	30	15	20	N	N	10	20	N	7	N	300	50
SS127	N	15	50	20	30	N	N	20	30	N	10	N	300	50
SS128	N	15	50	50	30	N	N	20	30	N	10	N	300	50
SS129	N	15	70	30	50	N	N	20	30	N	10	N	200	50
SS130	N	15	50	20	20	N	N	15	30	N	5	N	150	50
SS131	N	10	30	15	70	N	N	15	20	N	7	N	200	50
SS132	N	10	50	15	30	N	N	15	20	N	7	N	200	50
SS133	N	20	100	30	50	N	N	20	20	N	15	N	300	70
SS134	N	15	70	20	30	N	N	20	20	N	10	N	200	70
SS135	N	15	70	70	70	5	N	50	30	N	7	N	200	150
SS136	N	20	70	30	50	<5	N	30	30	N	10	N	200	50
SS137	N	15	50	30	50	<5	N	20	50	N	7	N	300	50
SS138	N	15	50	30	30	N	N	30	30	N	7	N	300	50
SS139	N	20	70	70	30	5	N	50	70	N	7	N	200	200
SS140	N	15	50	20	50	N	N	20	50	N	7	N	300	50
SS141	N	10	30	30	20	5	N	30	30	N	7	N	200	50
SS142	N	15	50	30	30	N	N	20	30	N	7	N	300	70
SS143	N	15	30	15	30	N	<20	15	70	N	7	N	300	70
SS144	N	7	30	10	30	5	N	10	30	N	5	N	300	50
SS145	N	10	20	15	50	N	N	10	50	N	7	N	300	50
SS146	N	15	30	15	50	N	N	10	30	N	7	N	200	50
SS147	N	15	50	20	50	N	N	10	50	N	7	N	200	50
SS148	N	10	20	15	50	N	N	10	70	N	7	N	300	50
SS149	N	15	20	20	30	5	N	10	150	N	7	N	200	70
SS150	N	10	20	15	50	N	N	10	70	N	7	N	200	50
SS151	N	10	30	15	30	N	N	15	70	N	5	N	200	30
SS152	N	10	30	15	30	7	N	15	100	N	5	N	300	70
SS153	N	10	30	10	30	N	N	10	30	N	7	N	300	50
SS154	N	20	50	15	50	N	N	15	100	N	15	N	300	100
SS155	N	10	30	20	30	N	N	10	50	N	7	N	300	50
SS156	N	10	20	10	30	N	N	10	20	N	7	N	300	50
SS157	N	10	30	15	30	N	N	10	30	N	7	N	300	50
SS158	N	10	20	10	30	N	N	10	20	N	7	N	500	50
SS159	N	10	20	15	20	N	N	10	30	N	7	N	500	50
SS160	N	20	70	20	30	N	N	20	15	N	10	N	300	150
SS263	N	10	30	15	30	N	N	10	50	N	7	N	300	50

Table 1 Data for stream sediment samples, Silver Peak Wilderness Study Area, Esmeralda County, Nevada

Sample	W-ppm s	Y-ppm s	Zn-ppm s	Zr-ppm s	Th-ppm s	Au-ppm aa	As-ppm aa	Zn-ppm aa	Sb-ppm aa	SI-F	U-INST
SS117	N	15	N	150	N	N	10	60	N	600	.90
SS118	N	15	N	100	N	N	15	95	N	400	1.40
SS119	N	15	N	150	N	N	15	85	N	500	1.10
SS120	N	20	200	200	N	N	10	200	N	300	2.30
SS121	N	30	300	200	N	N	10	230	N	300	2.00
SS122	N	20	N	150	N	N	35	75	N	300	.85
SS123	N	15	N	150	N	N	25	85	N	700	.85
SS124	N	15	N	200	N	N	10	55	N	600	1.10
SS125	N	20	N	150	N	N	15	55	N	600	1.20
SS126	N	15	N	100	N	N	10	50	N	500	.85
SS127	N	20	N	150	N	N	30	75	N	600	.85
SS128	N	20	N	100	N	N	15	65	N	700	2.10
SS129	N	20	N	70	N	N	20	70	N	700	1.20
SS130	N	15	N	100	N	N	15	65	N	900	1.10
SS131	N	20	N	150	N	N	10	40	N	400	1.10
SS132	N	20	N	150	N	N	10	50	N	400	.85
SS133	N	20	N	150	N	N	25	60	N	500	.80
SS134	N	20	N	150	N	N	15	70	N	600	.70
SS135	N	30	N	100	N	<.05	20	55	N	900	2.10
SS136	N	20	N	150	N	N	10	60	N	500	1.30
SS137	N	20	N	100	N	N	10	65	N	700	1.30
SS138	N	20	<200	50	N	N	15	120	N	600	1.40
SS139	N	20	200	100	N	N	20	230	N	800	1.20
SS140	N	15	N	100	N	N	15	90	N	800	1.10
SS141	N	15	N	70	N	N	15	75	N	700	1.30
SS142	N	20	N	100	N	N	15	100	N	600	.85
SS143	N	20	N	300	N	N	15	65	N	300	.60
SS144	N	15	N	100	N	N	10	40	N	400	.70
SS145	N	20	N	200	N	N	15	45	N	600	.85
SS146	N	20	N	200	N	N	10	60	N	500	.80
SS147	N	20	N	200	N	N	35	120	6	700	.85
SS148	N	20	<200	200	N	N	25	160	6	600	.45
SS149	N	20	200	150	N	N	35	210	14	500	.85
SS150	N	20	<200	150	N	N	20	160	6	400	.85
SS151	N	20	<200	100	N	N	15	200	4	500	1.20
SS152	N	15	<200	200	N	N	70	140	6	600	.85
SS153	N	20	N	200	N	N	10	40	N	400	.80
SS154	N	30	N	300	N	N	5	65	N	400	.85
SS155	N	20	N	100	N	N	5	55	N	400	.85
SS156	N	15	N	150	N	N	5	50	N	400	.85
SS157	N	20	N	150	N	N	5	45	N	200	.85
SS158	N	15	N	150	N	.05	5	35	N	300	.85
SS159	N	20	N	150	N	N	5	45	N	400	.65
SS160	N	20	<200	150	N	N	5	100	N	300	.85
SS263	N	20	N	200	N	--	25	110	4	--	--

Table 1 Data for stream sediment samples, Silver Peak Wilderness Study Area, Esmeralda County, Nevada--continued

Sample	X coor-dinate	Y coor-dinate	Fe-pct. s	Mg-pct. s	Ca-pct. s	Ti-pct. s	Mn-ppm s	Ag-ppm s	As-ppm s	Au-ppm s	B-ppm s	Ba-ppm s	Be-ppm s	Bi-ppm s
SS264	42,400	418,480	2	.7	1.5	.30	700	N	N	N	100	500	1.5	N
SS265	42,350	418,440	3	1.0	1.5	.30	700	N	N	N	100	500	1.0	N
SS266	42,400	418,400	2	.7	1.5	.30	500	N	N	N	200	500	1.5	N
SS267	42,180	418,460	3	.5	2.0	.50	1,000	N	N	N	50	700	<1.0	N
SS268	42,100	418,480	3	.7	2.0	.30	700	N	N	N	30	1,000	1.0	N
SS269	42,000	418,600	3	.7	2.0	.50	700	N	N	N	70	1,500	1.0	N
SS270	41,800	418,580	3	1.0	1.5	.30	500	N	N	N	30	700	1.0	N
SS271	41,750	418,540	2	1.0	1.5	.30	500	N	N	N	30	700	1.0	N
SS272	41,680	418,520	3	1.0	1.5	.30	500	N	N	N	50	700	1.5	N
SS273	41,620	416,900	3	1.0	5.0	.30	1,000	N	N	N	30	300	1.5	N
SS274	41,730	416,920	3	.7	2.0	.30	700	N	N	N	70	500	1.5	N
SS275	41,830	416,940	3	1.0	3.0	.30	500	N	N	N	70	500	1.5	N
SS276	41,980	416,980	2	.7	1.5	.20	500	N	N	N	30	500	1.5	N
SS277	42,120	417,020	3	.7	1.5	.50	700	N	N	N	20	500	1.0	N
SS278	42,260	416,980	3	.5	1.0	.50	700	N	N	N	30	300	1.5	N
SS279	41,233	416,990	2	.7	1.5	.30	500	N	N	N	50	700	1.0	N
SS280	42,420	416,940	2	.7	1.5	.30	500	N	N	N	50	700	1.5	N
SS281	42,490	416,970	2	1.0	1.5	.30	500	N	N	N	30	700	1.5	N
SS282	42,540	416,830	5	1.0	1.5	.50	700	N	N	N	30	700	1.5	N
SS283	42,580	416,910	3	1.0	1.5	.30	500	N	N	N	20	1,000	1.0	N
SS284	42,060	417,180	3	.7	1.5	.30	700	N	N	N	20	1,000	1.0	N
SS285	42,080	417,040	3	.7	1.5	.30	700	N	N	N	30	700	1.5	N

Table 1 Data for stream sediment samples, Silver Peak Wilderness Study Area, Esmeralda County, Nevada--continued

Sample	Ca-ppm s	Co-ppm s	Cr-ppm s	Cu-ppm s	La-ppm s	Mo-ppm s	Nb-ppm s	Ni-ppm s	Pb-ppm s	Sb-ppm s	Sc-ppm s	Sn-ppm s	Sr-ppm s	V-ppm s
SS264	N	10	30	10	30	<5	N	10	30	N	5	N	500	30
SS265	N	15	30	15	50	N	N	10	30	N	7	N	500	50
SS266	N	10	20	10	30	N	<20	10	20	N	5	N	200	30
SS267	N	15	70	10	70	<5	N	15	20	N	7	N	500	70
SS268	N	15	50	15	20	N	N	10	20	N	7	N	500	50
SS269	N	20	50	30	30	<5	N	15	20	N	10	N	300	70
SS270	N	15	70	20	30	<5	N	15	20	N	7	N	300	50
SS271	N	15	50	15	30	N	N	15	30	N	7	N	300	50
SS272	N	15	50	20	30	N	N	15	20	N	7	N	300	50
SS273	N	20	70	100	30	N	N	30	20	N	7	N	200	70
SS274	N	15	50	70	50	N	N	30	20	N	7	N	200	70
SS275	N	15	100	50	30	N	N	30	20	N	10	N	300	50
SS276	N	10	50	10	20	N	N	15	30	N	5	N	200	30
SS277	N	15	70	15	30	<5	N	20	20	N	7	N	200	70
SS278	N	10	30	10	30	N	<20	10	20	N	7	N	200	50
SS279	N	7	20	10	30	N	N	10	30	N	5	N	500	30
SS280	N	10	30	10	50	N	N	10	30	N	7	N	300	30
SS281	N	10	20	10	30	N	N	10	30	N	7	N	300	50
SS282	N	15	30	15	50	N	N	10	20	N	10	N	500	100
SS283	N	10	20	10	50	N	N	7	30	N	7	N	500	50
SS284	N	10	30	15	30	N	N	7	30	N	7	N	500	50
SS285	N	10	50	15	50	N	N	10	20	N	7	N	300	70

Table 1 Data for stream sediment samples, Silver Peak Wilderness Study Area, Esmeralda County, Nevada--continued

Sample	W-ppm s	Y-ppm s	Zn-ppm s	Zr-ppm s	Th-ppm s	Au-ppm aa	As-ppm aa	Zn-ppm aa	Sb-ppm aa	SI-F	U-INST
SS264	N	15	N	150	N	--	70	50	N	--	--
SS265	N	20	N	150	N	--	45	60	N	--	--
SS266	N	15	N	150	N	--	55	50	N	--	--
SS267	N	15	N	100	N	--	10	75	N	--	--
SS268	N	15	N	100	N	--	15	50	N	--	--
SS269	N	20	N	150	N	--	30	70	N	--	--
SS270	N	20	N	100	N	--	15	65	N	--	--
SS271	N	15	N	150	N	--	15	60	N	--	--
SS272	N	15	N	100	N	--	15	60	N	--	--
SS273	N	20	N	100	N	--	20	140	N	--	--
SS274	N	20	N	150	N	--	20	110	N	--	--
SS275	N	20	N	150	N	--	20	110	N	--	--
SS276	N	15	N	100	N	--	5	40	N	--	--
SS277	N	20	N	150	N	--	5	50	N	--	--
SS278	N	20	N	200	N	--	5	40	N	--	--
SS279	N	15	N	100	N	--	5	30	N	--	--
SS280	N	20	N	150	N	--	5	30	N	--	--
SS281	N	20	N	150	N	--	5	40	N	--	--
SS282	N	20	N	200	N	--	5	70	N	--	--
SS283	N	20	N	150	N	--	5	40	N	--	--
SS284	N	20	N	150	N	--	5	40	N	--	--
SS285	N	20	N	200	N	--	5	55	N	--	--

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data id:     nn     mm  nfmt  laty  lonx          (options(1-10))
ds-5         23     34     1     0     0   (  0   0  1  8  5  0 -1  0  0  0)


enter title cards on unit  15

title card number   1
("Table 2 Data for concentrate samples, Silver Peak Wilderness Study Area, Esmer
alda County, Nevada")
```

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 enter data id and no. rows,cols
mid,nn,mm = ds-5          23   34


enter column id s (colid(j,k))

X-COORD.Y-COORD.S-FE%   S-MG%   S-CA%   S-TI%   S-MN    S-AG    S-AS    S-AU
S-B     S-BA    S-BE    S-BI    S-CD    S-CO    S-CR    S-CU    S-LA    S-MO
S-NB    S-NI    S-PB    S-SB    S-SC    S-SN    S-SR    S-V     S-W     S-Y
S-ZN    S-ZR    S-TH    INST-HG
```

column ids & data ranges (min/max)

X-COORD.	Y-COORD.	S-FE%	S-MG%	S-CA%	S-TI%	S-MN	S-AG	S-AS	S-AU
0.41233E+05	0.41683E+06	0.30000E+00	0.15000E+00	0.20000E+01	0.20000E+00	0.15000E+03	0.10000E+01	0.50000E+03	0.20000E+02
0.42680E+05	0.41866E+06	0.20000E+01	0.20000E+01	0.20000E+02	0.20000E+01	0.10000E+04	0.10000E+01	0.50000E+03	0.20000E+02

S-B	S-BA	S-BE	S-BI	S-CD	S-CO	S-CR	S-CU	S-LA	S-MO
0.20000E+02	0.50000E+03	0.20000E+01	0.20000E+02	0.50000E+02	0.10000E+02	0.20000E+02	0.10000E+02	0.10000E+03	0.10000E+02
0.70000E+02	0.10000E+05	0.20000E+01	0.20000E+02	0.50000E+02	0.10000E+02	0.70000E+02	0.70000E+02	0.50000E+03	0.15000E+02

S-NB	S-NI	S-PB	S-SB	S-SC	S-SN	S-SR	S-V	S-W	S-Y
0.50000E+02	0.10000E+02	0.20000E+02	0.20000E+03	0.10000E+02	0.20000E+02	0.20000E+03	0.20000E+02	0.10000E+03	0.30000E+02
0.70000E+02	0.20000E+02	0.30000E+03	0.20000E+03	0.50000E+02	0.20000E+02	0.70000E+04	0.20000E+03	0.10000E+03	0.50000E+03

S-ZN	S-ZR	S-TH	INST-HG
0.50000E+03	0.50000E+03	0.20000E+03	0.20000E+00
0.50000E+03	0.20000E+04	0.20000E+03	0.10000E+02

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page no.,first column,last column =     2   13   24

page no.,first column,last column =     3   25   34
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Table 2 - Data for concentrate samples, Silver Peak Wilderness Study Area, Esmeralda County, Nevada
[N, not detected; <, detected but below the limit of determination shown; >, determined to be greater than the value shown.]

Sample	X coor-dinate	Y coor-dinate	Fe-pct. s	Mg-pct. s	Ca-pct. s	Ti-pct. s	Mn-ppm s	Ag-ppm s	As-ppm s	Au-ppm s	B-ppm s	Ba-ppm s
PC117	41,500	418,100	.7	.20	5.0	.7	300	N	N	N	N	10,000
PC118	41,520	418,100	.5	.30	7.0	1.0	300	N	N	N	100	>10,000
PC119	41,520	418,160	1.5	.70	10.0	1.0	500	N	N	N	<20	>10,000
PC120	41,400	418,070	.5	.50	3.0	.3	150	N	N	N	<20	>10,000
PC121	41,300	418,020	.5	.20	5.0	1.0	300	N	N	N	N	>10,000
PC122	41,500	418,149	.7	.20	5.0	1.0	500	N	N	N	N	>10,000
PC123	41,580	418,280	.7	.50	7.0	2.0	500	3.0	N	N	50	>10,000
PC124	41,160	417,940	.5	.30	7.0	>2.0	300	N	N	N	N	>10,000
PC125	41,040	417,940	.3	.30	10.0	>2.0	300	N	N	N	20	2,000
PC126	41,020	417,870	.5	.30	15.0	>2.0	300	N	N	N	<20	700
PC127	40,980	417,890	.5	.30	10.0	2.0	200	N	N	N	70	7,000
PC128	41,060	417,760	.5	.50	15.0	>2.0	300	N	N	N	100	7,000
PC129	40,890	417,710	.7	.50	20.0	>2.0	200	N	N	N	50	10,000
PC130	41,010	417,650	.5	.70	3.0	2.0	200	1.5	N	N	100	2,000
PC131	41,060	417,400	.3	.15	3.0	>2.0	300	N	N	N	30	700
PC132	40,940	417,480	.5	.20	3.0	>2.0	200	N	N	N	<20	700
PC133	41,170	417,320	7.0	.10	3.0	1.5	200	N	<500	N	20	>10,000
PC134	41,150	417,360	.7	.50	5.0	>2.0	500	N	N	N	70	10,000
PC135	41,138	417,160	.3	1.50	15.0	1.5	300	50.0	N	N	30	300
PC136	41,130	417,150	5.0	2.00	10.0	1.0	700	N	N	N	100	500
PC137	41,170	417,000	.7	1.00	20.0	1.5	300	N	N	N	20	200
PC138	41,450	416,890	1.5	2.00	15.0	.7	1,000	N	N	N	50	300
PC139	41,410	417,030	1.0	1.50	20.0	1.0	700	N	N	N	50	150
PC140	41,444	417,040	1.5	2.00	15.0	.7	1,000	N	N	N	20	300
PC141	41,250	416,920	3.0	2.00	15.0	.5	1,500	N	N	N	50	200
PC142	41,520	416,800	1.5	2.00	15.0	.7	1,000	N	N	N	70	500
PC143	42,808	418,040	.7	.20	1.5	.3	200	N	N	N	N	2,000
PC144	42,220	417,860	.5	.50	3.0	2.0	300	N	N	N	<20	1,000
PC145	42,290	417,900	.7	.50	5.0	>2.0	500	N	N	N	30	5,000
PC146	42,550	417,770	.7	.50	5.0	>2.0	700	N	N	N	20	3,000
PC147	42,440	418,280	.5	.50	7.0	1.5	700	5.0	N	N	20	>10,000
PC148	42,480	418,180	3.0	.15	5.0	1.0	700	7.0	<500	N	<20	>10,000
PC149	42,510	418,120	.5	.10	2.0	.7	500	10.0	700	N	20	>10,000
PC150	42,650	418,130	.7	.30	5.0	1.5	300	2.0	N	N	<20	>10,000
PC151	42,810	417,900	.5	.30	5.0	1.5	500	N	N	N	<20	>10,000
PC152	42,670	417,780	.7	.10	2.0	.3	300	7.0	500	N	N	>10,000
PC153	42,670	417,520	.7	.30	5.0	2.0	300	N	N	N	<20	7,000
PC154	42,580	417,520	.7	.20	2.0	.5	200	5.0	N	N	N	5,000
PC155	42,560	417,580	.5	.70	3.0	1.5	500	<1.0	N	N	20	2,000
PC156	42,580	417,640	1.0	.30	3.0	1.5	300	N	N	N	<20	1,500
PC157	42,600	417,300	.3	.70	7.0	2.0	300	N	N	N	<20	2,000
PC158	42,640	417,300	.5	.30	5.0	2.0	300	30.0	N	N	N	1,500
PC159	42,570	417,230	.7	.20	5.0	1.5	200	N	N	N	N	1,500
PC160	42,620	417,170	.5	.15	3.0	.5	150	N	N	N	N	1,500
PC263	42,490	418,360	.7	.30	3.0	.7	300	N	N	N	<20	1,500

Table 2 - Data for concentrate samples, Silver Peak Wilderness Study Area, Esmeralda County, Nevada

Sample	Be-ppm s	Bi-ppm s	Cd-ppm s	Co-ppm s	Cr-ppm s	Cu-ppm s	La-ppm s	Mo-ppm s	Nb-ppm s	Ni-ppm s	Pb-ppm s	Sb-ppm s	Sc-ppm s
PC117	N	N	N	N	20	<10	100	N	N	<10	30	N	<10
PC118	N	N	N	N	50	<10	300	30	N	15	100	N	20
PC119	N	N	N	<10	70	50	500	15	50	10	70	N	20
PC120	N	N	N	N	20	N	200	N	N	N	20	N	10
PC121	N	N	N	N	20	10	150	N	<50	N	20	N	<10
PC122	N	N	N	N	20	10	200	N	<50	10	30	N	15
PC123	N	N	N	<10	50	<10	700	N	<50	N	30	N	20
PC124	N	N	N	10	50	<10	700	N	50	<10	50	N	70
PC125	N	N	N	10	70	<10	500	10	50	<10	150	N	70
PC126	N	N	N	<10	70	N	500	N	50	N	300	N	70
PC127	N	N	N	<10	70	20	300	N	50	10	150	N	30
PC128	N	N	N	10	200	<10	300	<10	70	10	700	N	50
PC129	N	N	N	10	70	20	500	10	100	15	300	N	30
PC130	N	100	N	N	50	2,000	200	N	70	<10	200	N	50
PC131	N	N	N	10	70	N	300	N	70	<10	<20	N	50
PC132	N	N	N	10	50	N	200	N	70	<10	<20	N	50
PC133	N	N	N	150	50	300	150	<10	50	70	300	N	10
PC134	N	N	N	20	100	50	200	N	50	15	200	N	20
PC135	N	100	N	<10	70	50	100	15	50	20	500	N	15
PC136	N	N	N	30	500	100	300	10	<50	100	70	N	20
PC137	N	N	N	N	50	30	300	N	<50	15	30	N	10
PC138	N	N	N	<10	50	50	100	N	N	10	100	N	<10
PC139	N	N	N	10	70	50	200	N	<50	20	300	N	<10
PC140	N	N	N	<10	50	30	150	20	N	10	150	N	<10
PC141	2	N	N	<10	70	50	150	N	N	15	70	N	10
PC142	N	N	N	<10	70	30	150	N	50	20	300	N	15
PC143	<2	N	N	N	20	N	70	N	N	<10	30	N	10
PC144	N	N	N	N	50	N	300	N	50	N	30	N	20
PC145	N	N	N	10	70	10	500	<10	70	N	200	N	50
PC146	N	N	N	<10	70	<10	500	20	50	10	100	N	30
PC147	N	N	N	<10	30	15	300	N	N	<10	1,000	N	30
PC148	N	N	N	10	30	<10	200	N	N	<10	1,500	N	20
PC149	N	N	N	N	20	15	100	N	N	<10	3,000	N	10
PC150	N	N	N	N	30	<10	200	N	<50	<10	300	N	20
PC151	N	N	N	<10	20	<10	200	N	<50	<10	500	N	20
PC152	3	N	N	N	N	<10	50	N	N	N	1,500	N	<10
PC153	N	N	N	N	<20	15	300	N	50	<10	70	N	10
PC154	<2	N	N	N	<20	N	70	N	<50	<10	50	N	<10
PC155	N	N	N	<10	20	10	150	N	<50	N	150	N	20
PC156	N	N	N	N	20	N	200	N	<50	N	30	N	10
PC157	N	N	N	N	50	N	500	N	50	10	70	N	20
PC158	N	N	N	N	30	<10	200	N	50	10	50	N	20
PC159	N	N	N	N	20	N	200	15	50	15	30	N	10
PC160	<2	N	N	N	<20	N	50	10	<50	10	30	N	15
PC263	<2	N	N	N	<20	N	150	N	<50	<10	300	N	15

Table 2 - Data for concentrate samples, Silver Peak Wilderness Study Area, Esmeralda County, Nevada

Sample	Sn-ppm s	Sr-ppm s	V-ppm s	W-ppm s	Y-ppm s	Zn-ppm s	Zr-ppm s	Th-ppm s	Hg-ppm inst
PC117	N	500	30	N	100	N	>2,000	N	>10.00
PC118	N	700	50	N	200	N	>2,000	N	.56
PC119	N	1,000	70	N	200	N	>2,000	N	.24
PC120	N	700	20	N	30	N	2,000	N	.70
PC121	N	1,500	50	N	100	N	>2,000	N	.34
PC122	N	3,000	30	N	150	N	>2,000	N	<.20
PC123	N	2,000	70	N	300	N	>2,000	N	<.20
PC124	N	700	70	100	500	N	>2,000	N	2.10
PC125	20	<200	100	<100	700	N	>2,000	<200	.26
PC126	N	N	150	N	500	N	>2,000	N	<.20
PC127	N	1,000	70	150	200	5,000	>2,000	N	<.20
PC128	N	300	150	2,000	300	N	>2,000	N	.72
PC129	100	500	70	300	200	500	>2,000	N	>10.00
PC130	N	500	70	1,500	200	N	>2,000	300	>10.00
PC131	N	N	100	N	300	N	>2,000	300	.20
PC132	N	<200	100	N	300	N	>2,000	<200	2.00
PC133	N	1,000	50	N	150	N	>2,000	N	.40
PC134	N	200	100	<100	200	N	>2,000	<200	>10.00
PC135	N	300	150	10,000	150	N	2,000	N	>10.00
PC136	N	300	150	1,000	150	N	1,500	<200	>10.00
PC137	N	200	100	<100	200	N	>2,000	N	3.40
PC138	N	200	150	N	100	<500	500	N	.56
PC139	N	300	200	N	200	N	1,500	N	.64
PC140	N	200	150	N	100	N	1,500	N	.50
PC141	N	<200	100	N	50	N	300	N	.24
PC142	N	<200	200	N	150	N	2,000	N	2.10
PC143	N	500	50	N	30	N	>2,000	N	3.00
PC144	N	700	70	N	200	N	>2,000	<200	.24
PC145	N	300	100	N	500	N	>2,000	<200	<.20
PC146	N	200	100	<100	300	N	>2,000	<200	2.20
PC147	N	1,500	70	N	300	N	>2,000	N	<.20
PC148	2,000	1,500	100	N	200	500	>2,000	N	.30
PC149	N	3,000	50	N	150	<500	>2,000	N	>10.00
PC150	<20	700	50	N	200	700	>2,000	<200	<.20
PC151	N	1,500	70	N	200	N	>2,000	N	.40
PC152	N	1,500	30	N	20	500	>2,000	N	<.20
PC153	N	500	70	N	150	N	>2,000	N	<.20
PC154	N	700	50	N	30	N	>2,000	N	<.20
PC155	700	500	50	N	200	N	>2,000	N	<.20
PC156	N	500	70	N	100	N	>2,000	N	>10.00
PC157	N	200	70	N	200	N	>2,000	N	.20
PC158	N	300	70	N	200	N	>2,000	N	.20
PC159	N	1,000	50	N	150	N	>2,000	N	<.20
PC160	N	700	20	N	30	N	>2,000	N	<.20
PC263	N	200	70	N	200	N	>2,000	N	<.20

Table 2 - Data for concentrate samples, Silver Peak Wilderness Study Area, Esmeralda County, Nevada--continued

Sample	X coor-dinate	Y coor-dinate	Fe-pct. s	Mg-pct. s	Ca-pct. s	Ti-pct. s	Mn-ppm s	Ag-ppm s	As-ppm s	Au-ppm s	B-ppm s	Ba-ppm s
PC264	42,400	418,480	.5	.50	7.0	2.0	300	N	N	N	N	700
PC265	42,350	418,440	1.0	.50	5.0	2.0	500	N	N	N	20	1,000
PC266	42,400	418,400	1.5	.50	5.0	1.5	700	N	N	N	70	700
PC267	42,180	418,460	.7	.20	5.0	1.0	300	N	N	N	20	10,000
PC268	42,100	418,480	2.0	.50	5.0	1.0	700	N	N	N	<20	>10,000
PC269	42,000	418,600	.7	.15	3.0	1.0	200	N	N	N	N	>10,000
PC270	41,800	418,580	.5	.30	5.0	.7	200	N	N	N	N	>10,000
PC271	41,750	418,540	.7	.50	7.0	1.5	300	N	N	N	<20	>10,000
PC272	41,680	418,520	.5	.20	3.0	1.0	200	N	N	N	N	>10,000
PC273	41,620	416,900	1.5	2.00	15.0	1.0	1,000	N	N	N	<20	3,000
PC274	41,730	416,920	1.0	.70	20.0	1.5	1,000	N	N	N	50	700
PC275	41,830	416,940	1.0	.50	15.0	1.0	500	N	N	N	<20	700
PC276	41,980	416,980	1.0	.50	5.0	2.0	500	N	N	N	<20	700
PC277	42,120	417,020	1.5	.70	5.0	2.0	700	N	N	N	N	500
PC278	42,260	416,980	.5	.15	2.0	.7	300	N	N	N	N	500
PC279	41,233	416,900	.5	.70	15.0	2.0	500	N	N	N	N	700
PC280	42,420	416,940	.5	.50	10.0	2.0	300	N	N	N	<20	500
PC281	42,490	416,970	.3	.20	5.0	1.0	200	N	N	N	N	1,500
PC282	42,540	416,830	.5	.20	5.0	.5	200	N	N	N	N	1,000
PC283	42,580	416,910	.5	.15	5.0	.2	150	N	N	N	N	1,500
PC284	42,660	417,180	.5	.50	5.0	2.0	500	N	N	N	N	1,000
PC285	42,680	417,040	.5	.30	7.0	1.5	300	N	N	N	N	700

Table 2 - Data for concentrate samples, Silver Peak Wilderness Study Area, Esmeralda County, Nevada--continued

Sample	Be-ppm s	Bi-ppm s	Cd-ppm s	Co-ppm s	Cr-ppm s	Cu-ppm s	La-ppm s	Mo-ppm s	Nb-ppm s	Ni-ppm s	Pb-ppm s	Sb-ppm s	Sc-ppm s
PC264	N	N	N	<10	30	N	500	N	<50	N	70	N	50
PC265	N	N	N	10	50	<10	500	N	50	15	70	N	50
PC266	N	N	N	<10	30	<10	300	N	50	10	70	N	30
PC267	N	N	N	N	20	N	200	N	<50	<10	50	N	20
PC268	N	N	N	10	30	N	300	N	<50	<10	20	N	20
PC269	N	N	N	N	20	15	200	N	<50	N	150	N	15
PC270	N	N	N	N	20	15	300	N	<50	<10	20	N	15
PC271	N	N	N	<10	50	15	300	N	50	15	100	N	20
PC272	N	N	N	N	<20	10	200	N	<50	<10	30	<200	10
PC273	N	N	N	<10	70	30	150	N	<50	20	200	N	10
PC274	N	N	N	<10	70	50	150	10	N	20	30	N	20
PC275	N	N	N	<10	70	70	100	15	N	20	70	N	15
PC276	N	N	N	<10	50	<10	200	N	70	10	50	N	10
PC277	N	N	N	<10	70	N	300	N	70	15	50	N	20
PC278	<2	N	N	N	N	N	200	N	50	N	30	N	<10
PC279	N	N	N	<10	50	<10	500	N	50	N	20	N	10
PC280	N	N	N	N	30	<10	500	N	<50	N	20	N	15
PC281	N	N	N	N	<20	N	200	N	<50	N	50	N	N
PC282	2	N	N	N	N	N	100	15	N	20	30	N	<10
PC283	2	N	N	N	N	N	100	N	N	N	30	N	N
PC284	<2	N	N	<10	20	<10	300	15	N	20	20	N	15
PC285	N	N	N	<10	30	N	200	10	<50	10	20	N	10

Table 2 - Data for concentrate samples, Silver Peak Wilderness Study Area, Esmeralda County, Nevada--continued

Sample	Sn-ppm s	Sr-ppm s	V-ppm s	W-ppm s	Y-ppm s	Zn-ppm s	Zr-ppm s	Th-ppm s	Hg-ppm inst
PC264	N	200	70	N	300	N	>2,000	<200	<.20
PC265	N	<200	100	N	500	N	>2,000	N	<.20
PC266	N	300	70	N	200	N	>2,000	N	<.20
PC267	N	1,000	50	N	200	N	>2,000	N	<.20
PC268	N	1,000	100	N	200	N	>2,000	N	<.20
PC269	N	5,000	70	N	100	N	>2,000	N	>10.00
PC270	N	5,000	50	N	150	N	>2,000	N	1.80
PC271	N	3,000	70	<100	200	N	>2,000	N	1.60
PC272	N	7,000	50	N	150	N	>2,000	N	.40
PC273	N	300	200	N	100	N	>2,000	N	<.20
PC274	N	200	150	N	200	N	>2,000	N	4.40
PC275	N	300	150	N	150	N	>2,000	N	4.00
PC276	<20	200	70	N	300	N	>2,000	N	.54
PC277	20	200	100	N	500	N	>2,000	N	<.20
PC278	N	300	20	N	150	N	>2,000	N	.24
PC279	N	500	70	N	500	N	>2,000	N	<.20
PC280	N	500	70	N	300	N	>2,000	N	<.20
PC281	N	1,000	50	N	100	N	>2,000	N	<.20
PC282	N	1,500	30	N	70	N	2,000	N	<.20
PC283	N	1,500	20	N	30	N	500	N	<.20
PC284	N	500	70	N	200	N	>2,000	<200	<.20
PC285	N	1,000	50	N	150	N	>2,000	N	<.20

Table 3 Data for rock samples, Silver Peak Wilderness Study Area, Esmeralda County, Nevada

[N, not detected; <, detected but below the limit of determination shown; >, determined to be greater than the value shown.]

Sample	X coor-dinate	Y coor-dinate	Fe-pct. s	Mg-pct. s	Ca-pct. s	Ti-pct. s	Mn-ppm s	Ag-ppm s	As-ppm s	Au-ppm s
1971	41,120	417,050	5.00	.20	.30	.150	15	2.0	500	N
1972	41,120	417,050	10.00	.07	.70	.070	100	1.5	200	N
1973	41,080	417,050	.70	.03	.10	.020	100	N	N	N
1974	42,800	417,480	1.00	.10	3.00	.200	1,000	15.0	N	N
1975	42,860	417,520	.70	.15	.07	.050	5,000	200.0	N	N
1976	42,880	417,800	7.00	<.02	.30	.010	200	500.0	<200	N
1977	42,860	417,730	.70	<.02	.15	<.002	>5,000	200.0	300	N
1978	42,860	417,700	.20	<.02	1.00	N	1,500	1,500.0	700	N
1979	42,820	417,700	.20	.05	.05	.002	500	500.0	N	N
1980	42,820	417,700	.30	.05	.20	N	2,000	2,000.0	<200	N
1981	42,550	407,980	.70	.02	5.00	.005	>5,000	7.0	500	N
1982	42,660	417,900	.30	.02	.20	.020	1,000	N	N	N
1983	42,620	417,900	.20	.15	20.00	.015	>5,000	100.0	200	N
1984	42,580	417,800	.70	.03	.15	<.002	5,000	10.0	N	N
1985	42,640	417,920	.20	<.02	<.05	.007	150	3.0	N	N
1986	42,640	417,920	.30	<.02	.05	.050	100	7.0	N	N
1987	41,290	417,920	.50	<.02	3.00	<.002	1,500	700.0	500	N
1988	42,640	417,600	.70	.03	1.00	.005	>5,000	7.0	N	N
1989	42,840	417,680	.30	.02	7.00	N	>5,000	150.0	N	N
1990	42,840	416,800	.30	.02	5.00	N	>5,000	70.0	N	N
1991	42,840	416,800	.15	<.02	3.00	.150	3,000	300.0	N	N
1992	42,840	416,800	.30	.03	10.00	N	5,000	150.0	N	N
1993	42,840	416,800	1.00	.05	7.00	N	>5,000	300.0	500	N
NV1965	40,990	417,980	3.00	.05	1.00	.100	200	50.0	5,000	N
NV1966	40,980	417,650	3.00	.50	5.00	.050	500	2.0	N	N
NV1967	41,360	417,000	7.00	.10	15.00	.030	150	.5	N	N
NV1968	42,860	417,770	1.50	.02	.70	N	500	70.0	N	N
NV1969	42,820	417,460	.70	<.02	7.00	N	>5,000	300.0	200	N
NV1970	47,220	412,340	2.00	2.00	.70	.150	200	<.5	N	N

Table 3 Data for rock samples, Silver Peak Wilderness Study Area, Esmeralda County, Nevada

Sample	B-ppm s	Ba-ppm s	Be-ppm s	Bi-ppm s	Cd-ppm s	Co-ppm s	Cr-ppm s	Cu-ppm s	La-ppm s	Mo-ppm s
1971	70	1,000	1.5	N	N	10	100	3,000	<20	30
1972	70	300	1.0	N	N	50	30	700	<20	15
1973	<10	30	<1.0	N	N	7	10	7	N	N
1974	20	300	10.0	N	N	5	<10	7	30	N
1975	30	200	50.0	N	N	<5	<10	300	20	N
1976	70	>5,000	100.0	N	N	N	N	150	30	N
1977	30	>5,000	70.0	N	N	N	N	500	<20	N
1978	20	>5,000	50.0	N	N	N	N	500	20	10
1979	30	>5,000	70.0	N	N	N	N	150	<20	N
1980	20	>5,000	100.0	N	N	20	N	300	20	N
1981	100	1,500	7.0	N	20	N	N	10	<20	15
1982	10	1,500	7.0	N	N	<5	N	<5	50	N
1983	150	>5,000	7.0	N	300	<5	10	70	20	30
1984	15	1,500	100.0	N	N	N	N	5	50	N
1985	15	150	2.0	N	N	N	N	<5	20	70
1986	30	500	2.0	N	N	<5	N	7	20	500
1987	70	>5,000	50.0	N	N	N	N	1,500	<20	5
1988	20	5,000	30.0	N	N	N	<10	50	<20	N
1989	10	1,500	20.0	N	30	N	N	<5	20	5
1990	10	>5,000	30.0	N	N	N	10	20	<20	N
1991	30	>5,000	30.0	N	N	N	N	500	<20	N
1992	10	500	20.0	N	N	N	N	<5	<20	N
1993	50	2,000	100.0	N	20	N	N	30	20	N
NV1965	30	50	<1.0	N	30	N	<10	150	N	N
NV1966	30	300	1.0	N	N	7	10	30	<20	N
NV1967	100	200	1.0	N	20	N	15	30	N	5
NV1968	70	>5,000	100.0	N	N	N	N	15	<20	10
NV1969	30	>5,000	150.0	N	N	N	N	1,000	N	7
NV1970	30	500	2.0	N	N	7	N	10	<20	N

Table 3 Data for rock samples, Silver Peak Wilderness Study Area, Esmeralda County, Nevada

Sample	Nb-ppm s	Ni-ppm s	Pb-ppm s	Sb-ppm s	Sc-ppm s	Sn-ppm s	Sr-ppm s	V-ppm s	W-ppm s
1971	N	50	50	N	7	N	100	1,500	N
1972	N	500	20	N	<5	N	<100	300	N
1973	N	10	15	N	N	N	N	30	N
1974	N	5	30	<100	<5	N	100	20	N
1975	N	5	500	100	N	N	<100	15	N
1976	N	<5	700	200	N	N	5,000	15	100
1977	N	N	700	200	N	N	>5,000	10	<50
1978	N	N	7,000	<100	N	N	>5,000	15	N
1979	N	N	1,000	100	N	N	5,000	<10	N
1980	N	N	5,000	100	N	N	500	10	N
1981	N	N	100	500	N	N	200	<10	N
1982	N	N	15	100	N	N	<100	10	N
1983	N	10	5,000	200	N	N	5,000	20	<50
1984	N	N	20	200	N	N	N	15	N
1985	N	N	15	N	N	N	N	20	N
1986	N	N	20	N	N	N	100	30	N
1987	N	7	300	200	N	N	>5,000	10	N
1988	N	<5	100	100	N	N	500	30	N
1989	N	N	200	<100	N	N	200	<10	N
1990	N	N	70	100	N	N	500	<10	N
1991	N	N	3,000	100	N	N	5,000	15	N
1992	N	N	300	<100	N	N	200	<10	N
1993	N	N	>20,000	200	N	N	500	<10	N
NV1965	N	<5	500	<100	5	N	100	15	N
NV1966	N	10	30	N	<5	N	<100	30	N
NV1967	N	10	100	N	N	N	<100	70	N
NV1968	N	7	300	100	N	N	200	<10	100
NV1969	N	5	2,000	150	N	N	>5,000	10	N
NV1970	N	15	70	N	<5	N	<100	10	N

Table 3 Data for rock samples, Silver Peak Wilderness Study Area, Esmeralda County, Nevada

Sample	Y-ppm s	Zn-ppm s	Zr-ppm s	Th-ppm s	Au-ppm aa	Hg-ppm inst	As-ppm aa	Zn-ppm aa	Sb-ppm aa
1971	50	N	70	N	N	.54	400	45	16
1972	20	300	50	N	N	.50	200	270	6
1973	<10	N	15	N	N	.50	25	15	2
1974	15	N	100	N	<.05	.34	35	40	2
1975	10	700	70	N	N	.40	10	550	14
1976	<10	500	<10	N	N	.44	150	480	100
1977	<10	1,000	N	N	N	.64	250	880	86
1978	10	3,000	N	N	N	1.30	400	1,700	24
1979	N	500	N	N	N	.50	45	300	46
1980	N	1,500	N	N	.20	.70	170	1,300	46
1981	N	1,000	<10	N	.40	2.30	450	900	140
1982	15	N	10	N	N	.95	10	25	4
1983	<10	5,000	<10	N	N	2.40	200	>2,000	160
1984	10	N	N	N	N	1.10	15	85	8
1985	N	N	<10	N	3.20	3.00	10	10	2
1986	N	N	50	N	N	1.10	50	50	6
1987	N	200	N	N	4.20	.64	350	190	100
1988	N	200	N	N	N	.44	5	230	2
1989	N	1,500	N	N	N	.34	40	1,600	8
1990	N	300	N	N	N	.30	5	330	10
1991	N	500	N	N	N	.20	60	490	68
1992	N	300	N	N	N	.34	40	270	12
1993	N	1,000	N	N	.10	.30	300	>2,000	70
NV1965	10	500	50	N	.30	.04	>2,000	500	78
NV1966	15	N	10	N	N	5.60	15	80	6
NV1967	N	1,000	<10	N	N	.06	25	800	N
NV1968	N	300	N	N	N	.32	95	300	28
NV1969	N	N	N	N	N	<.02	110	100	78
NV1970	<10	N	100	N	N	.02	N	75	4

program publst terminated normally

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$$$
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Silver Peak Conc

D0010 FI R-K STATISTICS - U S G S STATPAC (06/12/80) DATE 8/10/84

TITLE	INPUT ID	N	M	***** OPTIONS *****
	-ds-5 -	67	34	0 0 0 0 0 0 0 0 0 0

NUMBER OF SELECTED COLUMNS = 34

SELECTED COLUMN INDICES

1	2	3	4	5	6	7	8	9	10
11	12	13	14	15	16	17	18	19	20
21	22	23	24	25	26	27	28	29	30
31	32	33	34						

SELECTED COLUMN IDENTIFIERS

X-COORD.	Y-COORD.	S-FE%	S-MG%	S-CA%	S-TI%	S-MN	S-AG	S-AS	S-AU
S-B	S-BA	S-BE	S-BI	S-CD	S-CO	S-CR	S-CU	S-LA	S-MO
S-NB	S-NI	S-PB	S-SB	S-SC	S-SN	S-SR	S-V	S-W	S-Y
S-ZN	S-ZR	S-TH	INST-HG						

NUMBER OF SELECTED ROW PAIRS = 1

SELECTED ROW PAIRS

1- 67

NO	COLUMN	N	H	L	G	B	T	NO OF UNQUAL VALUES	NO OF IMPROPER QUAL VALUES	MINIMUM	MAXIMUM	NO
1	X-COORD.	0	0	0	0	0	0	67	0	40890.000	42810.000	1
2	Y-COORD.	0	0	0	0	0	0	67	0	416800.00	418600.00	2
3	S-FE%	0	0	0	0	0	0	67	0	0.3000000	7.0000000	3
4	S-MG%	0	0	0	0	0	0	67	0	0.1000000	2.0000000	4
5	S-CA%	0	0	0	0	0	0	67	0	1.5000000	20.000000	5
6	S-TI%	0	0	0	10	0	0	57	0	0.2000000	2.0000000	6
7	S-MN	0	0	0	0	0	0	67	0	150.00000	1500.0000	7
8	S-AG	56	0	1	0	0	0	10	0	1.5000000	50.000000	8
9	S-AS	63	0	2	0	0	0	2	0	500.00000	700.00000	9
10	S-AU	67	0	0	0	0	0	0	0			10
11	S-B	22	0	18	0	0	0	27	0	20.000000	100.00000	11
12	S-BA	0	0	0	19	0	0	48	0	150.00000	10000.000	12
13	S-BE	57	0	6	0	0	0	4	0	2.0000000	3.0000000	13
14	S-BI	65	0	0	0	0	0	2	0	100.00000	100.00000	14
15	S-CD	67	0	0	0	0	0	0	0			15
16	S-CO	29	0	24	0	0	0	14	0	10.000000	150.00000	16
17	S-CR	4	0	6	0	0	0	57	0	20.000000	500.00000	17
18	S-CU	21	0	18	0	0	0	28	0	10.000000	2000.0000	18
19	S-LA	0	0	0	0	0	0	67	0	50.000000	700.00000	19
20	S-MO	49	0	3	0	0	0	15	0	10.000000	30.000000	20
21	S-NB	16	0	23	0	0	0	28	0	50.000000	100.00000	21
22	S-NI	16	0	19	0	0	0	32	0	10.000000	100.00000	22
23	S-PB	0	0	2	0	0	0	65	0	20.000000	3000.0000	23
24	S-SB	66	0	1	0	0	0	0	0			24
25	S-SC	2	0	9	0	0	0	56	0	10.000000	70.000000	25
26	S-SN	60	0	2	0	0	0	5	0	20.000000	2000.0000	26
27	S-SR	2	0	5	0	0	0	60	0	200.00000	7000.0000	27
28	S-V	0	0	0	0	0	0	67	0	20.000000	200.00000	28
29	S-W	55	0	5	0	0	0	7	0	100.00000	10000.000	29
30	S-Y	0	0	0	0	0	0	67	0	20.000000	700.00000	30
31	S-ZN	60	0	2	0	0	0	5	0	500.00000	5000.0000	31
32	S-ZR	0	0	0	57	0	0	10	0	300.00000	2000.0000	32
33	S-TH	55	0	10	0	0	0	2	0	300.00000	300.00000	33
34	INST-HG	0	0	28	9	0	0	30	0	0.2000000	4.4000000	34

NO	COLUMN	K1 MEAN	SQRT(K2) STD DEVIATION	K2 VARIANCE	K3	G1
1	X-COORD.	41908.254	[illegible]			

NO	COLUMN	K1 MEAN	SQRT(K2) STD DEVIATION	K2 VARIANCE	K3	G1 SKEWNESS	K4	G2 KURTOSIS	NO
1	X-COORD.	41908.254	621.70426	336516.19	-31667505.	-0.1317839	-2.3191868D+11	-1.5523882	1
2	Y-COORD.	417638.49	565.96965	320321.65	17587114.	0.0970097	-1.4062018D+11	-1.3704875	2
3	S-FE%	0.9492537	1.0527559	1.1082949	4.7410487	4.0634172	23.502951	19.134263	3
4	S-MG%	0.5552239	0.5301611	0.2810708	0.2888675	1.9385419	0.2214307	2.8028922	4
5	S-CA%	7.4104478	5.1697879	26.726707	160.04955	1.1583405	143.17367	0.2004344	5
6	S-TI%	1.2315789	0.5673113	0.3218421	0.0025677	0.0140633	-0.1260547	-1.2169512	6
7	S-MN	430.59701	268.12413	71890.547	31667696.	1.6428911	1.5927625D+10	3.0818213	7
8	S-AG	12.050000	15.674555	245.69167	7853.0125	2.0391569	221178.71	3.6640591	8
9	S-AS	600.00000	141.42136	20000.000					9
10	S-AU								10
11	S-B	47.037037	28.798346	829.34473	17877.037	0.7485019	-474409.12	-0.6897359	11
12	S-BA	2342.7083	2909.3940	8464573.4	4.4216598D+10	1.7954682	1.4600922D+14	2.0378402	12
13	S-BE	2.2500000	0.5000000	0.2500000	0.2500000	2.0000000	0.2500000	4.0000000	13
14	S-BI	100.00000	0.0	0.0					14
15	S-CD								15
16	S-CO	22.142857	37.247317	1387.3626	185851.65	3.5965113	25340934.	13.165660	16
17	S-CR	56.491228	66.507014	4423.1830	1655661.5	5.6281956	7.1619301D+08	36.606674	17
18	S-CU	111.42857	374.21487	140036.77	2.6830128D+08	5.1198779	5.2273481D+11	26.656139	18
19	S-LA	261.04478	153.82137	23661.013	3771713.8	1.0363077	2.8443016D+08	0.5080529	19
20	S-MO	14.666667	5.4989176	30.238095	271.88645	1.6351437	3118.5897	3.4107461	20
21	S-NB	56.785714	12.187903	148.54497	3613.8584	1.9961087	98952.177	4.4844526	21
22	S-NI	18.593750	18.282478	334.24899	22939.441	3.7538565	1625588.4	14.550247	22
23	S-PB	220.15385	456.88310	208742.16	4.2031191D+08	4.4071357	9.8798667D+11	22.674135	23
24	S-SB								24
25	S-SC	23.928571	16.561573	274.28571	7024.6753	1.5463987	113304.93	1.5060605	25
26	S-SN	568.00000	849.65876	721920.00	1.0446488D+09	1.7030865	1.3727757D+12	2.6340344	26
27	S-SR	1026.6667	1287.3395	1657242.9	6.1639511D+09	2.8892154	2.5608447D+13	9.3241851	27
28	S-V	81.194030	43.745905	1913.7042	90699.134	1.0834052	3026147.5	0.8263052	28
29	S-W	2150.0000	3535.8874	12502500.	1.0709790D+11	2.4226220	9.5007548D+14	6.0780516	29
30	S-Y	206.56716	135.17163	18271.370	3539424.0	1.4330980	8.2030421D+08	2.4571558	30
31	S-ZN	1440.0000	1991.9839	3968000.0	1.7592100D+10	2.2256670	7.8117620D+13	4.9614164	31
32	S-ZR	1380.0000	690.89314	477333.33	-2.3113333D+08	-0.7008578	-3.0085429D+11	-1.3204218	32
33	S-TH	300.00000	0.0	0.0					33
34	INST-HG	1.1493333	1.2239195	1.4979788	2.5574045	1.3948931	2.1435263	0.9552509	34

NOTE: THE ABOVE STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY.

D0010 FISHER-K STATISTICS - U S G S STATPAC (06/12/80) DATE 7/20/84

TITLE	INPUT ID	N	M	***** OPTIONS *****
	-ds-6 -	29	38	0 0 0 0 0 0 0 0 0 0

Rucker - Silver Peak

NUMBER OF SELECTED COLUMNS = 38

SELECTED COLUMN INDICES

1	2	3	4	5	6	7	8	9	10
11	12	13	14	15	16	17	18	19	20
21	22	23	24	25	26	27	28	29	30
31	32	33	34	35	36	37	38		

SELECTED COLUMN IDENTIFIERS

X-COORD.	Y-COORD.	S-FE%	S-MG%	S-CA%	S-TI%	S-MN	S-AG	S-AS	S-AU
S-B	S-BA	S-BE	S-BI	S-CD	S-CO	S-CR	S-CU	S-LA	S-MO
S-NB	S-NI	S-PB	S-SB	S-SC	S-SN	S-SR	S-V	S-W	S-Y
S-ZN	S-ZR	S-TH	AA-AU-P	INST-HG	AA-AS-P	AA-ZN-P	AA-SB-P		

NUMBER OF SELECTED ROW PAIRS = 1

SELECTED ROW PAIRS

1- 29

D0010 FISHER-K STATISTICS - U S G S STATPAC (06/12/80) DATE 7/20/84

NO	COLUMN	N	H	L	G	B	T	NO OF UNQUAL VALUES	NO OF IMPROPER QUAL VALUES	MINIMUM	MAXIMUM	NO
1	X-COORD.	0	0	0	0	0	0	29	0	40980.000	47228.000	1
2	Y-COORD.	0	0	0	0	0	0	29	0	407980.00	417980.00	2
3	S-FE%	0	0	0	0	0	0	29	0	0.1500000	10.000000	3
4	S-MG%	0	0	8	0	0	0	21	0	0.0200000	2.0000000	4
5	S-CA%	0	0	1	0	0	0	28	0	0.0500000	20.000000	5
6	S-TI%	8	0	3	0	0	0	18	0	0.0020000	0.2000000	6
7	S-MN	0	0	0	8	0	0	21	0	15.000000	5000.0000	7
8	S-AG	2	0	1	0	0	0	26	0	0.5000000	2000.0000	8
9	S-AS	17	0	2	0	0	0	10	0	200.00000	5000.0000	9
10	S-AU	29	0	0	0	0	0	0	0			10
11	S-B	0	0	1	0	0	0	28	0	10.000000	150.00000	11
12	S-BA	0	0	0	11	0	0	18	0	30.000000	5000.0000	12
13	S-BE	0	0	2	0	0	0	27	0	1.0000000	150.00000	13
14	S-BI	29	0	0	0	0	0	0	0			14
15	S-CD	23	0	0	0	0	0	6	0	20.000000	300.00000	15
16	S-CO	18	0	4	0	0	0	7	0	5.0000000	50.000000	16
17	S-CR	18	0	4	0	0	0	7	0	10.000000	100.00000	17
18	S-CU	0	0	4	0	0	0	25	0	5.0000000	3000.0000	18
19	S-LA	4	0	13	0	0	0	12	0	20.000000	50.000000	19
20	S-MO	17	0	0	0	0	0	12	0	5.0000000	500.00000	20
21	S-NB	29	0	0	0	0	0	0	0			21
22	S-NI	14	0	3	0	0	0	12	0	5.0000000	500.00000	22
23	S-PB	0	0	0	1	0	0	28	0	15.000000	7000.0000	23
24	S-SB	8	0	5	0	0	0	16	0	100.00000	500.00000	24
25	S-SC	23	0	4	0	0	0	2	0	5.0000000	7.0000000	25
26	S-SN	29	0	0	0	0	0	0	0			26
27	S-SR	3	0	6	4	0	0	16	0	100.00000	5000.0000	27
28	S-V	0	0	7	0	0	0	22	0	10.000000	1500.0000	28
29	S-W	25	0	2	0	0	0	2	0	100.00000	100.00000	29
30	S-Y	15	0	5	0	0	0	9	0	10.000000	50.000000	30
31	S-ZN	10	0	0	0	0	0	19	0	200.00000	5000.0000	31
32	S-ZR	14	0	5	0	0	0	10	0	10.000000	100.00000	32
33	S-TH	29	0	0	0	0	0	0	0			33
34	AA-AU-P	22	0	1	0	0	0	6	0	0.1000000	4.2000000	34
35	INST-HG	0	0	1	0	0	0	28	0	0.0200000	5.6000000	35
36	AA-AS-P	1	0	0	1	0	0	27	0	5.0000000	450.00000	36
37	AA-ZN-P	0	0	0	2	0	0	27	0	10.000000	1700.0000	37
38	AA-SB-P	1	0	0	0	0	0	28	0	2.0000000	160.00000	38

D0010 FISHER-K STATISTICS - U S G S STATPAC (06/12/80)

DATE 7/20/84

NO	COLUMN	K1 MEAN	SQRT(K2) STD DEVIATION	K2 VARIANCE	K3	G1 SKEWNESS	K4	G2 KURTOSIS	NO
1	X-COORD.	42526.828	1153.6621	1330936.1	3.2585116D+09	2.1221860	1.6917718D+13	9.5505271	1
2	Y-COORD.	416993.10	2019.5015	4078386.5	-3.1606435D+10	-3.8374520	2.5744579D+14	15.477793	2
3	S-FE%	1.6775862	2.4787521	6.1442118	33.693609	2.2123216	164.98186	4.3702254	3
4	S-MG%	0.1757143	0.4316894	0.1863557	0.3351207	4.1656921	0.6273895	18.065576	4
5	S-CA%	3.4525000	4.8877842	23.890434	240.54492	2.0599664	2546.9608	4.4624583	5
6	S-TI%	0.0602222	0.0626602	0.0039263	2.5813044D-04	1.0492135	-2.5546595D-06	-0.1657166	6
7	S-MN	1319.7619	1715.6343	2943401.2	7.6158286D+09	1.5081445	8.6346146D+12	0.9966531	7
8	S-AG	274.80769	477.25425	227771.62	2.9637733D+08	2.7264376	3.9400747D+11	7.5946056	8
9	S-AS	860.00000	1464.5439	2144888.9	9.6846000D+09	3.0830068	4.4312987D+13	9.6321098	9
10	S-AU								10
11	S-B	41.785714	33.972055	1154.1005	61889.499	1.5785252	3359119.3	2.5219597	11
12	S-BA	946.11111	1188.5143	1412566.3	4.2732031D+09	2.5453075	1.5818084D+13	7.9274984	12
13	S-BE	41.166667	42.380648	1838.7500	72575.180	0.9204582	-551728.27	-0.1631849	13
14	S-BI								14
15	S-CD	70.000000	112.78298	12720.000	3499200.0	2.4391477	9.6435600D+08	5.9602320	15
16	S-CO	15.142857	16.159915	261.14286	9255.7429	2.1932799	332352.34	4.8735165	16
17	S-CR	26.428571	33.255862	1105.9524	88442.857	2.4046846	7211470.2	5.8959115	17
18	S-CU	361.64000	660.77637	436625.41	8.8797046D+08	3.0777619	2.0516968D+12	10.762054	18
19	S-LA	26.666667	11.547005	133.33333	2521.2121	1.6375753	24242.424	1.3636364	19
20	S-MO	58.500000	140.26177	19673.364	9275413.1	3.3613624	4.4340389D+09	11.456244	20
21	S-NB								21
22	S-NI	52.833333	141.35760	19981.970	9657289.0	3.4189896	4.6962693D+09	11.761871	22
23	S-PB	969.82143	1810.4683	3277795.3	1.3840424D+10	2.3322583	5.0802588D+13	4.7284867	23
24	S-SB	165.62500	101.19083	10239.583	2694419.6	2.6004099	8.7225418D+08	8.3191411	24
25	S-SC	6.0000000	1.4142136	2.0000000					25
26	S-SN								26
27	S-SR	1450.0000	2122.2629	4504000.0	1.2028343D+10	1.2583696	-9.3187727D+12	-0.4593693	27
28	S-V	100.00000	318.60186	101507.14	1.4357652D+08	4.4395455	2.0787724D+11	20.175009	28
29	S-W	100.00000	0.0	0.0					29
30	S-Y	17.222222	12.774758	163.19444	5415.6746	2.5977330	190389.38	7.1487810	30
31	S-ZN	1015.7895	1174.3855	1379181.3	4.2315975D+09	2.6125964	1.4144655D+13	7.4361758	31
32	S-ZR	52.500000	33.603075	1129.1667	2604.1667	0.0686328	-1413854.2	-1.1088901	32
33	S-TH								33
34	AA-AU-P	1.4000000	1.8121810	3.2840000	6.4583999	1.0852261	-11.854200	-1.0991727	34
35	INST-HG	0.9039286	1.1724755	1.3746988	4.5803933	2.8417864	17.578190	9.3016292	35
36	AA-AS-P	128.33333	141.41456	19998.077	3094542.7	1.0942439	-39730867.	-0.0993463	36
37	AA-ZN-P	430.18519	478.41180	228877.85	1.6490488D+08	1.5060100	8.3251460D+10	1.5892211	37
38	AA-SB-P	40.214286	45.370375	2058.4709	111613.53	1.1950876	2447947.1	0.5777136	38

NOTE: THE ABOVE STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY.

Silver Peak Seds

D0036 GRAPHICAL ANALYSIS - U S G S STATPAC (02/07/82) DATE 7/20/84

TITLE	INPUT ID	N	M	***** OPTIONS ****
Nevada data	-ds-4 -	67	39	1 0 0 0 2 1 0 0 0 0

VARIABLE NO. 9 CONTAINS NO VALID DATA POINTS. THEREFORE THIS VARIABLE WILL BE SKIPPED.

VARIABLE NO. 10 CONTAINS NO VALID DATA POINTS. THEREFORE THIS VARIABLE WILL BE SKIPPED.

VARIABLE NO. 14 CONTAINS NO VALID DATA POINTS. THEREFORE THIS VARIABLE WILL BE SKIPPED.

VARIABLE NO. 15 CONTAINS NO VALID DATA POINTS. THEREFORE THIS VARIABLE WILL BE SKIPPED.

VARIABLE NO. 21 CONTAINS NO VALID DATA POINTS. THEREFORE THIS VARIABLE WILL BE SKIPPED.

VARIABLE NO. 24 CONTAINS NO VALID DATA POINTS. THEREFORE THIS VARIABLE WILL BE SKIPPED.

VARIABLE NO. 26 CONTAINS NO VALID DATA POINTS. THEREFORE THIS VARIABLE WILL BE SKIPPED.

VARIABLE NO. 29 CONTAINS NO VALID DATA POINTS. THEREFORE THIS VARIABLE WILL BE SKIPPED.

VARIABLE NO. 33 CONTAINS NO VALID DATA POINTS. THEREFORE THIS VARIABLE WILL BE SKIPPED.

THE MAX AND MIN -0.13010E+01 FOR VARIABLE NO. 34 ARE THE SAME. THEREFORE THIS VARIABLE WILL BE SKIPPED.

D0036 GRAPHICAL ANALYSIS - U S G S STATPAC (02/07/82) DATE 7/20/84

TITLE	INPUT ID		N	M	***** OPTIONS ****
Nevada data	-ds-4	-	67	39	1 0 0 0 2 1 0 0 0 0

NUMBER OF SELECTED VARIABLES = 27

SELECTED VARIABLE INDICES

3	4	5	6	7	8	11	12	13	16
17	18	19	20	22	23	25	27	28	30
31	32	35	36	37	38	39			

SELECTED VARIABLE IDENTIFIERS

S-FE%	S-MG%	S-CA%	S-TI%	S-MN	S-AG	S-B	S-BA	S-BE	S-CO
S-CR	S-CU	S-LA	S-MO	S-NI	S-PB	S-SC	S-SR	S-V	S-Y
S-ZN	S-ZR	AA-AS-P	AA-ZN-P	AA-SB-P	SI-F	U-INST			

SELECTED ROW PAIRS
1 TO 67

LOWER BOUNDARIES OF THE LOWEST CLASSES

0.25000	-0.41700	-0.08400	-0.91700	2.41600	-0.41700	1.08300	2.41600	-0.08400	0.75000
1.25000	0.91600	1.25000	0.58300	0.75000	1.08300	0.58300	2.08300	1.41600	1.08300
2.25000	1.58300	0.58300	1.41600	0.58300	2.25000	-0.41700			

CLASS INTERVALS

0.16667	0.16667	0.16667	0.16667	0.16667	0.16667	0.16667	0.16667	0.16667	0.16667
0.16667	0.16667	0.16667	0.16667	0.16667	0.16667	0.16667	0.16667	0.16667	0.16667
0.16667	0.16667	0.16667	0.16667	0.16667	0.16667	0.16667			

D0036 GRAPHICAL ANALYSIS - U S G S STATPAC (02/07/82) DATE 7/20/84

Nevada data

FREQUENCY TABLE FOR VARIABLE 3 (S-FE%)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		0	0	0.00	0.00		
	L		0	0	0.00	0.00		
	T		0	0	0.00	0.00	3.91	3.91
2.500E-01	-	4.167E-01	20	20	29.85	29.85	22.33	0.24
4.167E-01	-	5.833E-01	40	60	59.70	89.55	30.43	3.01
5.833E-01	-	7.500E-01	5	65	7.46	97.01	9.63	2.23
7.500E-01	-	9.167E-01	2	67	2.99	100.00	0.69	2.45
	G		0	67	0.00	100.00	3.91	3.91
	H		0	67				
	B		0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 3 (S-FE%)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
2.154E+00 XXXXXXXXXXXXXXXXXXXXXXXXXXXXX
3.162E+00 XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
4.642E+00 XXXXXXX
6.813E+00 XXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 2.00000E+00
MAXIMUM ANTILOG = 7.00000E+00
GEOMETRIC MEAN = 2.83202E+00
GEOMETRIC DEVIATION = 1.34528E+00
VARIANCE OF LOGS = 1.65925E-02

PERCENT TABLE FOR VARIABLE 3 (S-FE%) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	5.933340E-01	3.920433E+00
95.00	7.050009E-01	5.069918E+00
98.00	1.000000E+35	1.000000E+35

D0036 GRAPHICAL ANALYSIS - U S G S STATPAC (02/07/82) DATE 7/20/84

Nevada data

FREQUENCY TABLE FOR VARIABLE 4 (S-MG%)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
		N	0	0	0.00	0.00		
		L	0	0	0.00	0.00		
		T	0	0	0.00	0.00	0.17	0.17
-4.170E-01	-	-2.503E-01	8	8	11.94	11.94	7.42	0.05
-2.503E-01	-	-8.367E-02	40	48	59.70	71.64	35.71	0.52
-8.367E-02	-	8.300E-02	17	65	25.37	97.01	22.02	1.14
8.300E-02	-	2.497E-01	2	67	2.99	100.00	1.68	0.06
		G	0	67	0.00	100.00	0.17	0.17
		H	0	67				
		B	0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 4 (S-MG%)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
4.638E-01 XXXXXXXXXXXX
6.808E-01 XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
9.992E-01 XXXXXXXXXXXXXXXXXXXXXXXXX
1.467E+00 XXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 5.00000E-01
MAXIMUM ANTILOG = 1.50000E+00
GEOMETRIC MEAN = 7.53067E-01
GEOMETRIC DEVIATION = 1.27408E+00
VARIANCE OF LOGS = 1.10662E-02

PERCENT TABLE FOR VARIABLE 4 (S-MG%) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	3.692248E-02	1.088736E+00
95.00	6.976568E-02	1.174264E+00
98.00	1.000000E+35	1.000000E+35

D0036 GRAPHICAL ANALYSIS - U S G S STATPAC (02/07/82) DATE 7/20/84

Nevada data

FREQUENCY TABLE FOR VARIABLE 5 (S-CA%)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		0	0	0.00	0.00		
	L		0	0	0.00	0.00		
	T		0	0	0.00	0.00	3.16	3.16
-8.400E-02	-	8.267E-02	9	9	13.43	13.43	10.86	0.32
8.267E-02	-	2.493E-01	38	47	56.72	70.15	20.94	13.89
2.493E-01	-	4.160E-01	11	58	16.42	86.57	20.03	4.07
4.160E-01	-	5.827E-01	2	60	2.99	89.55	9.50	5.92
5.827E-01	-	7.493E-01	6	66	8.96	98.51	2.23	6.38
7.493E-01	-	9.160E-01	1	67	1.49	100.00	0.27	1.94
	G		0	67	0.00	100.00	3.16	3.16
	H		0	67				
	B		0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 5 (S-CA%)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
9.985E-01 XXXXXXXXXXXXX
1.466E+00 XXXXXXXXXXXX
```

D0036 GRAPHICAL ANALYSIS - U S G S STATPAC (02/07/82) DATE 7/20/84

Nevada data

FREQUENCY TABLE FOR VARIABLE 7 (S-MN)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		0	0	0.00	0.00		
	L		0	0	0.00	0.00		
	T		0	0	0.00	0.00	0.18	0.18
2.416E+00	-	2.583E+00	2	2	2.99	2.99	3.96	0.97
2.583E+00	-	2.749E+00	35	37	52.24	55.22	21.69	8.16
2.749E+00	-	2.916E+00	18	55	26.87	82.09	29.85	4.71
2.916E+00	-	3.083E+00	11	66	16.42	98.51	10.40	0.03
3.083E+00	-	3.249E+00	1	67	1.49	100.00	0.91	0.01
	G		0	67	0.00	100.00	0.18	0.18
	H		0	67				
	B		0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 7 (S-MN)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
3.157E+02 XXX
4.634E+02 XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
6.802E+02 XXXXXXXXXXXXXXXXXXXXXXXXXX
9.985E+02 XXXXXXXXXXXXXXXX
1.466E+03 X
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 3.00000E+02
MAXIMUM ANTILOG = 1.50000E+03
GEOMETRIC MEAN = 6.13974E+02
GEOMETRIC DEVIATION = 1.35953E+00
VARIANCE OF LOGS = 1.77926E-02

PERCENT TABLE FOR VARIABLE 7 (S-MN) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	2.996304E+00	9.915262E+02
95.00	3.047062E+00	1.114453E+03
98.00	3.077516E+00	1.195409E+03

D0036 GRAPHICAL ANALYSIS - U S G S STATPAC (02/07/82) DATE 7/20/84

Nevada data

FREQUENCY TABLE FOR VARIABLE 8 (S-AG)

LOG LIMITS LOWER - UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
N	58	58	86.57	86.57		
L	1	59	1.49	88.06		
T	0	59	0.00	88.06	0.32	0.32
-4.170E-01 - -2.503E-01	3	62	4.48	92.54	51.52	45.69
-2.503E-01 - -8.367E-02	4	66	5.97	98.51	15.16	8.22
-8.367E-02 - 8.300E-02	1	67	1.49	100.00	0.00	693.33
G	0	67	0.00	100.00	0.00	0.00
H	0	67				
B	0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 8 (S-AG)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
4.638E-01 XXXX
6.308E-01 XXXXXX
9.992E-01 X
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

```
MINIMUM ANTILOG      =  5.00000E-01
MAXIMUM ANTILOG      =  1.00000E+00
GEOMETRIC MEAN       =  6.45153E-01
GEOMETRIC DEVIATION  =  1.27516E+00
VARIANCE OF LOGS     =  1.11442E-02
```

PERCENT TABLE FOR VARIABLE 8 (S-AG) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.000000E+35	1.000000E+35
95.00	-1.815329E-01	6.532898E-01
98.00	-9.783269E-02	7.953022E-01

D0036 GRAPHICAL ANALYSIS - U S G S STATPAC (02/07/82) DATE 7/20/84

Nevada data

FREQUENCY TABLE FOR VARIABLE 11 (S-B)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		0	0	0.00	0.00		
	L		0	0	0.00	0.00		
	T		0	0	0.00	0.00	1.40	1.40
1.083E+00	-	1.250E+00	2	2	2.99	2.99	5.15	1.93
1.250E+00	-	1.416E+00	15	17	22.39	25.37	12.90	0.34
1.416E+00	-	1.583E+00	27	44	40.30	65.67	19.09	3.28
1.583E+00	-	1.750E+00	13	57	19.40	85.07	16.69	0.81
1.750E+00	-	1.916E+00	6	63	8.96	94.03	8.62	0.80
1.916E+00	-	2.083E+00	3	66	4.48	98.51	2.63	0.05
2.083E+00	-	2.250E+00	0	66	0.00	98.51	0.47	0.47
2.250E+00	-	2.416E+00	1	67	1.49	100.00	0.05	16.84
	G		0	67	0.00	100.00	1.40	1.40
	H		0	67				
	B		0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 11 (S-B)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
1.467E+01 XXX
2.153E+01 XXXXXXXXXXXXXXXXXXXXXX
3.160E+01 XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
4.638E+01 XXXXXXXXXXXXXXXXXXXX
6.808E+01 XXXXXXXXX
9.992E+01 XXXX
1.467E+02
2.153E+02 X
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 1.50000E+01
MAXIMUM ANTILOG = 2.00000E+02
GEOMETRIC MEAN = 3.47072E+01
GEOMETRIC DEVIATION = 1.67723E+00
VARIANCE OF LOGS = 5.04423E-02

PERCENT TABLE FOR VARIABLE 11 (S-B) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.841335E+00	6.939607E+01
95.00	1.952446E+00	8.962851E+01
98.00	2.064113E+00	1.159079E+02

D0036 GRAPHICAL ANALYSIS - U S G S STATPAC (02/07/82) DATE 7/20/84

Nevada data

FREQUENCY TABLE FOR VARIABLE 12 (S-BA)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		0	0	0.00	0.00		
	L		0	0	0.00	0.00		
	T		0	0	0.00	0.00	0.69	0.69
2.416E+00	-	2.583E+00	6	6	8.96	8.96	5.68	0.02
2.583E+00	-	2.749E+00	23	29	34.33	43.28	19.15	0.77
2.749E+00	-	2.916E+00	26	55	38.81	82.09	25.35	0.02
2.916E+00	-	3.083E+00	9	64	13.43	95.52	13.21	1.34
3.083E+00	-	3.249E+00	2	66	2.99	98.51	2.69	0.18
3.249E+00	-	3.416E+00	1	67	1.49	100.00	0.22	2.78
	G		0	67	0.00	100.00	0.69	0.69
	H		0	67				
	B		0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 12 (S-BA)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
3.157E+02 XXXXXXXXX
4.634E+02 XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
6.802E+02 XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
9.985E+02 XXXXXXXXXXXXX
1.466E+03 XXX
2.151E+03 X
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 3.00000E+02
MAXIMUM ANTILOG = 2.00000E+03
GEOMETRIC MEAN = 6.30195E+02
GEOMETRIC DEVIATION = 1.46374E+00
VARIANCE OF LOGS = 2.73781E-02

PERCENT TABLE FOR VARIABLE 12 (S-BA) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	3.014149E+00	1.033117E+03
95.00	3.076187E+00	1.191754E+03
98.00	3.221002E+00	1.663419E+03

D0036 GRAPHICAL ANALYSIS - U S G S STATPAC (02/07/82) DATE 7/20/84

Nevada data

FREQUENCY TABLE FOR VARIABLE 13 (S-BE)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
		N	0	0	0.00	0.00		
		L	1	1	1.49	1.49		
		T	0	1	0.00	1.49	0.79	0.79
-8.400E-02	-	8.267E-02	24	25	35.82	37.31	24.23	0.00
8.267E-02	-	2.493E-01	42	67	62.69	100.00	41.99	0.00
		G	0	67	0.00	100.00	0.00	0.00
		H	0	67				
		B	0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 13 (S-BE)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
9.985E-01 XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
1.466E+00 XXXXXXXXXXXXXXXXXXXX
```

D0036 GRAPHICAL ANALYSIS - U S G S STATPAC (02/07/82) DATE 7/20/84

Nevada data

FREQUENCY TABLE FOR VARIABLE 16 (S-CO)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		0	0	0.00	0.00		
	L		0	0	0.00	0.00		
	T		0	0	0.00	0.00	0.08	0.08
7.500E-01	-	9.167E-01	2	2	2.99	2.99	3.01	0.34
9.167E-01	-	1.083E+00	24	26	35.82	38.81	21.98	0.18
1.083E+00	-	1.250E+00	32	58	47.76	86.57	31.97	0.00
1.250E+00	-	1.417E+00	8	66	11.94	98.51	9.42	0.21
1.417E+00	-	1.583E+00	1	67	1.49	100.00	0.54	0.39
	G		0	67	0.00	100.00	0.08	0.08
	H		0	67				
	B		0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 16 (S-CO)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
6.813E+00 XXX
1.000E+01 XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
1.468E+01 XXXXXXXXXXXXXXXXXXXX
```

D0036 GRAPHICAL ANALYSIS - U S G S STATPAC (02/07/82) DATE 7/20/84

Nevada data

FREQUENCY TABLE FOR VARIABLE 17 (S-CR)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		0	0	0.00	0.00		
	L		0	0	0.00	0.00		
	T		0	0	0.00	0.00	3.22	3.22
1.250E+00	-	1.417E+00	11	11	16.42	16.42	8.47	0.76
1.417E+00	-	1.583E+00	19	30	28.36	44.78	16.26	0.46
1.583E+00	-	1.750E+00	18	48	26.87	71.64	18.81	0.03
1.750E+00	-	1.917E+00	13	61	19.40	91.04	13.11	0.00
1.917E+00	-	2.083E+00	4	65	5.97	97.01	5.51	0.41
2.083E+00	-	2.250E+00	2	67	2.99	100.00	1.63	0.09
	G		0	67	0.00	100.00	3.22	3.22
	H		0	67				
	B		0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 17 (S-CR)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
2.154E+01 XXXXXXXXXXXXXXXX
3.162E+01 XXXXXXXXXXXXXXXXXXXXXXXXXXXX
4.642E+01 XXXXXXXXXXXXXXXXXXXXXXXXXXXX
6.813E+01 XXXXXXXXXXXXXXXXXXX
1.000E+02 XXXXXX
1.468E+02 XXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

```
MINIMUM ANTILOG      =  2.00000E+01
MAXIMUM ANTILOG      =  1.50000E+02
GEOMETRIC MEAN       =  4.27850E+01
GEOMETRIC DEVIATION  =  1.69491E+00
VARIANCE OF LOGS     =  5.25077E-02
```

PERCENT TABLE FOR VARIABLE 17 (S-CR) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.907694E+00	8.085253E+01
95.00	2.027085E+00	1.064351E+02
98.00	1.000000E+35	1.000000E+35

D0036 GRAPHICAL ANALYSIS - U S G S STATPAC (02/07/82) DATE 7/20/84

Nevada data

FREQUENCY TABLE FOR VARIABLE 18 (S-CU)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		0	0	0.00	0.00		
	L		0	0	0.00	0.00		
	T		0	0	0.00	0.00	4.42	4.42
9.160E-01	-	1.083E+00	13	13	19.40	19.40	9.81	1.04
1.083E+00	-	1.249E+00	26	39	38.81	58.21	16.88	4.93
1.249E+00	-	1.416E+00	12	51	17.91	76.12	17.94	1.97
1.416E+00	-	1.583E+00	9	60	13.43	89.55	11.78	0.66
1.583E+00	-	1.749E+00	3	63	4.48	94.03	4.78	0.66
1.749E+00	-	1.916E+00	3	66	4.48	98.51	1.20	2.72
1.916E+00	-	2.083E+00	1	67	1.49	100.00	0.20	3.13
	G		0	67	0.00	100.00	4.42	4.42
	H		0	67				
	B		0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 18 (S-CU)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
9.985E+00 XXXXXXXXXXXXXXXXXX
1.466E+01 XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
2.151E+01 XXXXXXXXXXXXXXXXXX
3.157E+01 XXXXXXXXXXXXX
4.634E+01 XXXX
6.802E+01 XXXX
9.985E+01 X
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 1.00000E+01
MAXIMUM ANTILOG = 1.00000E+02
GEOMETRIC MEAN = 1.86382E+01
GEOMETRIC DEVIATION = 1.71379E+00
VARIANCE OF LOGS = 5.53302E-02

PERCENT TABLE FOR VARIABLE 18 (S-CU) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.599335E+00	3.974978E+01
95.00	1.785446E+00	6.101634E+01
98.00	1.897113E+00	7.890656E+01

D0036 GRAPHICAL ANALYSIS - U S G S STATPAC (02/07/82) DATE 7/20/84

Nevada data

FREQUENCY TABLE FOR VARIABLE 19 (S-LA)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		0	0	0.00	0.00		
	L		0	0	0.00	0.00		
	T		0	0	0.00	0.00	2.30	2.30
1.250E+00	-	1.417E+00	9	9	13.43	13.43	12.43	0.95
1.417E+00	-	1.583E+00	36	45	53.73	67.16	26.03	3.82
1.583E+00	-	1.750E+00	17	62	25.37	92.54	20.01	0.45
1.750E+00	-	1.917E+00	4	66	5.97	98.51	5.63	0.47
1.917E+00	-	2.083E+00	1	67	1.49	100.00	0.59	0.28
	G		0	67	0.00	100.00	2.30	2.30
	H		0	67				
	B		0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 19 (S-LA)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
2.154E+01 XXXXXXXXXXXXX
3.162E+01 XXXXXXXXXXXX
```

D0036 GRAPHICAL ANALYSIS - U S G S STATPAC (02/07/82)

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Nevada data

FREQUENCY TABLE FOR VARIABLE 20 (S-MO)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		53	53	79.10	79.10		
	L		7	60	10.45	89.55		
	T		0	60	0.00	89.55	0.00	0.00
5.830E-01	-	7.497E-01	6	66	8.96	98.51	66.78	55.32
7.497E-01	-	9.163E-01	1	67	1.49	100.00	0.22	2.76
	G		0	67	0.00	100.00	0.00	0.00
	H		0	67				
	B		0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 20 (S-MO)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
4.638E+00 XXXXXXXXX
6.808E+00 X
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 5.00000E+00
MAXIMUM ANTILOG = 7.00000E+00
GEOMETRIC MEAN = 5.24621E+00
GEOMETRIC DEVIATION = 1.13562E+00
VARIANCE OF LOGS = 3.05048E-03

PERCENT TABLE FOR VARIABLE 20 (S-MO) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.000000E+35	1.000000E+35
95.00	1.000000E+35	1.000000E+35
98.00	1.000000E+35	1.000000E+35

D0036 GRAPHICAL ANALYSIS - U S G S STATPAC (02/07/82) DATE 7/20/84

Nevada data

FREQUENCY TABLE FOR VARIABLE 22 (S-NI)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
		N	0	0	0.00	0.00		
		L	0	0	0.00	0.00		
		T	0	0	0.00	0.00	0.83	0.83
7.500E-01	-	9.167E-01	2	2	2.99	2.99	5.07	1.86
9.167E-01	-	1.083E+00	25	27	37.31	40.30	15.73	5.47
1.083E+00	-	1.250E+00	18	45	26.87	67.16	23.09	1.12
1.250E+00	-	1.417E+00	14	59	20.90	88.06	16.08	0.27
1.417E+00	-	1.583E+00	6	65	8.96	97.01	5.31	0.09
1.583E+00	-	1.750E+00	2	67	2.99	100.00	0.89	1.39
		G	0	67	0.00	100.00	0.83	0.83
		H	0	67				
		B	0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 22 (S-NI)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
6.813E+00 XXX
1.000E+01 XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
1.468E+01 XXXXXXXXXXXXXXXXXXXXXXXXXXX
2.154E+01 XXXXXXXXXXXXXXXXXXXXX
3.162E+01 XXXXXXXXX
4.642E+01 XXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 7.00000E+00
MAXIMUM ANTILOG = 5.00000E+01
GEOMETRIC MEAN = 1.47631E+01
GEOMETRIC DEVIATION = 1.53704E+00
VARIANCE OF LOGS = 3.48510E-02

PERCENT TABLE FOR VARIABLE 22 (S-NI) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.452779E+00	2.836476E+01
95.00	1.545835E+00	3.514268E+01
98.00	1.000000E+35	1.000000E+35

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Nevada data

FREQUENCY TABLE FOR VARIABLE 23 (S-PB)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
		N	0	0	0.00	0.00		
		L	0	0	0.00	0.00		
		T	0	0	0.00	0.00	1.91	1.91
1.083E+00	-	1.250E+00	1	1	1.49	1.49	7.11	5.25
1.250E+00	-	1.416E+00	25	26	37.31	38.81	16.42	4.48
1.416E+00	-	1.583E+00	27	53	40.30	79.10	20.71	1.91
1.583E+00	-	1.750E+00	6	59	8.96	88.06	14.27	4.79
1.750E+00	-	1.916E+00	5	64	7.46	95.52	5.36	0.02
1.916E+00	-	2.083E+00	2	66	2.99	98.51	1.10	0.74
2.083E+00	-	2.250E+00	1	67	1.49	100.00	0.13	5.85
		G	0	67	0.00	100.00	1.91	1.91
		H	0	67				
		B	0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 23 (S-PB)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
1.467E+01 X
2.153E+01 XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
3.160E+01 XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
4.638E+01 XXXXXXXXX
6.808E+01 XXXXXXX
9.992E+01 XXX
1.467E+02 X
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 1.50000E+01
MAXIMUM ANTILOG = 1.50000E+02
GEOMETRIC MEAN = 3.02198E+01
GEOMETRIC DEVIATION = 1.61671E+00
VARIANCE OF LOGS = 4.35279E-02

PERCENT TABLE FOR VARIABLE 23 (S-PB) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.793001E+00	6.208711E+01
95.00	1.904668E+00	8.029127E+01
98.00	2.054669E+00	1.134145E+02

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Nevada data

FREQUENCY TABLE FOR VARIABLE 25 (S-SC)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		0	0	0.00	0.00		
	L		0	0	0.00	0.00		
	T		0	0	0.00	0.00	0.24	0.24
5.830E-01	-	7.497E-01	8	8	11.94	11.94	7.94	0.00
7.497E-01	-	9.163E-01	41	49	61.19	73.13	34.69	1.15
9.163E-01	-	1.083E+00	15	64	22.39	95.52	22.12	2.29
1.083E+00	-	1.250E+00	3	67	4.48	100.00	2.01	0.49
	G		0	67	0.00	100.00	0.24	0.24
	H		0	67				
	B		0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 25 (S-SC)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
4.638E+00 XXXXXXXXXXXX
6.308E+00 XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
9.992E+00 XXXXXXXXXXXXXXXXXXXXX
1.407E+01 XXXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 5.00000E+00
MAXIMUM ANTILOG = 1.50000E+01
GEOMETRIC MEAN = 7.53616E+00
GEOMETRIC DEVIATION = 1.28661E+00
VARIANCE OF LOGS = 1.19785E-02

PERCENT TABLE FOR VARIABLE 25 (S-SC) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.041890E+00	1.101260E+01
95.00	1.079112E+00	1.199809E+01
98.00	1.000000E+35	1.000000E+35

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Nevada data

FREQUENCY TABLE FOR VARIABLE 27 (S-SR)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		0	0	0.00	0.00		
	L		0	0	0.00	0.00		
	T		0	0	0.00	0.00	0.30	0.30
2.083E+00	-	2.250E+00	1	1	1.49	1.49	4.69	2.90
2.250E+00	-	2.416E+00	22	23	32.84	34.33	21.40	0.02
2.416E+00	-	2.583E+00	32	55	47.76	82.09	28.37	0.46
2.583E+00	-	2.750E+00	12	67	17.91	100.00	12.24	0.00
	G		0	67	0.00	100.00	0.30	0.30
	H		0	67				
	B		0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 27 (S-SR)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
1.467E+02 X
2.153E+02 XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
3.160E+02 XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
4.633E+02 XXXXXXXXXXXXXXXXXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 1.50000E+02
MAXIMUM ANTILOG = 5.00000E+02
GEOMETRIC MEAN = 2.84801E+02
GEOMETRIC DEVIATION = 1.38649E+00
VARIANCE OF LOGS = 2.01400E-02

PERCENT TABLE FOR VARIABLE 27 (S-SR) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.000000E+35	1.000000E+35
95.00	1.000000E+35	1.000000E+35
98.00	1.000000E+35	1.000000E+35

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Nevada data

FREQUENCY TABLE FOR VARIABLE 28 (S-V)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
		N	0	0	0.00	0.00		
		L	0	0	0.00	0.00		
		T	0	0	0.00	0.00	1.48	1.48
1.416E+00	-	1.583E+00	6	6	8.96	8.96	8.46	0.71
1.583E+00	-	1.749E+00	38	44	56.72	65.67	21.54	12.57
1.749E+00	-	1.916E+00	16	60	23.88	89.55	23.05	2.15
1.916E+00	-	2.083E+00	2	62	2.99	92.54	10.36	6.75
2.083E+00	-	2.249E+00	3	65	4.48	97.01	1.95	0.57
2.249E+00	-	2.416E+00	2	67	2.99	100.00	0.16	21.66
		G	0	67	0.00	100.00	1.48	1.48
		H	0	67				
		B	0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 28 (S-V)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
3.157E+01 XXXXXXXXX
4.634E+01 XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
6.802E+01 XXXXXXXXXXXXXXXXXXXXXXXX
9.985E+01 XXX
1.466E+02 XXXX
2.151E+02 XXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 3.00000E+01
MAXIMUM ANTILOG = 2.00000E+02
GEOMETRIC MEAN = 5.78523E+01
GEOMETRIC DEVIATION = 1.48664E+00
VARIANCE OF LOGS = 2.96544E-02

PERCENT TABLE FOR VARIABLE 28 (S-V) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.941001E+00	8.729735E+01
95.00	2.174335E+00	1.493946E+02
98.00	1.000000E+35	1.000000E+35

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Nevada data

FREQUENCY TABLE FOR VARIABLE 30 (S-Y)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		0	0	0.00	0.00		
	L		0	0	0.00	0.00		
	T		0	0	0.00	0.00	0.37	0.37
1.083E+00	-	1.250E+00	21	21	31.34	31.34	25.91	0.93
1.250E+00	-	1.416E+00	43	64	64.18	95.52	39.20	0.37
1.416E+00	-	1.583E+00	3	67	4.48	100.00	1.53	1.41
	G		0	67	0.00	100.00	0.37	0.37
	H		0	67				
	B		0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 30 (S-Y)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
1.467E+01 XXXXXXXXXXXXXXXXXXXXXXXXXXXXX
2.153E+01 XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
3.160E+01 XXXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 1.50000E+01
MAXIMUM ANTILOG = 3.00000E+01
GEOMETRIC MEAN = 1.86104E+01
GEOMETRIC DEVIATION = 1.18405E+00
VARIANCE OF LOGS = 5.38326E-03

PERCENT TABLE FOR VARIABLE 30 (S-Y) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.401993E+00	2.523439E+01
95.00	1.414977E+00	2.600024E+01
98.00	1.000000E+35	1.000000E+35

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Nevada data

FREQUENCY TABLE FOR VARIABLE 31 (S-ZN)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		57	57	85.07	85.07		
	L		6	63	8.96	94.03		
	T		0	63	0.00	94.03	0.42	0.42
2.250E+00	-	2.417E+00	3	66	4.48	98.51	0.00	0.00
2.417E+00	-	2.583E+00	1	67	1.49	100.00	66.58	64.59
	G		0	67	0.00	100.00	0.00	0.00
	H		0	67				
	B		0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 31 (S-ZN)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
2.154E+02 XXXX
3.162E+02 X
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 2.00000E+02
MAXIMUM ANTILOG = 3.00000E+02
GEOMETRIC MEAN = 2.21336E+02
GEOMETRIC DEVIATION = 1.22474E+00
VARIANCE OF LOGS = 7.75187E-03

PERCENT TABLE FOR VARIABLE 31 (S-ZN) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.000000E+35	1.000000E+35
95.00	1.000000E+35	1.000000E+35
98.00	1.000000E+35	1.000000E+35

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Nevada data

FREQUENCY TABLE FOR VARIABLE 32 (S-ZR)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
		N	0	0	0.00	0.00		
		L	0	0	0.00	0.00		
		T	0	0	0.00	0.00	0.00	0.00
1.583E+00	-	1.750E+00	1	1	1.49	1.49	0.20	3.31
1.750E+00	-	1.916E+00	2	3	2.99	4.48	3.59	0.71
1.916E+00	-	2.083E+00	19	22	28.36	32.84	18.90	0.00
2.083E+00	-	2.250E+00	30	52	44.78	77.61	29.16	0.02
2.250E+00	-	2.416E+00	13	65	19.40	97.01	13.31	0.01
2.416E+00	-	2.583E+00	2	67	2.99	100.00	1.84	0.01
		G	0	67	0.00	100.00	0.00	0.00
		H	0	67				
		B	0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 32 (S-ZR)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
4.633E+01 X
6.808E+01 XXX
9.992E+01 XXXXXXXXXXXXXXXXXXXXXXXXXXXX
1.467E+02 XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
2.153E+02 XXXXXXXXXXXXXXXXXXX
3.160E+02 XXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 5.00000E+01
MAXIMUM ANTILOG = 3.00000E+02
GEOMETRIC MEAN = 1.38797E+02
GEOMETRIC DEVIATION = 1.38899E+00
VARIANCE OF LOGS = 2.03626E-02

PERCENT TABLE FOR VARIABLE 32 (S-ZR) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	2.356078E+00	2.270275E+02
95.00	2.399027E+00	2.506267E+02
98.00	1.000000E+35	1.000000E+35

D0036 GR. CAL ANALYSIS - U S G S STATPAC (02/07/82) DATE 8/10/84

SilverPeak

FREQUENCY TABLE FOR VARIABLE 3 (S-FE%)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
		N	0	0	0.00	0.00		
		L	0	0	0.00	0.00		
		T	0	0	0.00	0.00	3.34	3.34
-5.840E-01	-	-4.173E-01	5	5	7.46	7.46	6.78	0.47
-4.173E-01	-	-2.507E-01	26	31	38.81	46.27	12.53	14.48
-2.507E-01	-	-8.400E-02	18	49	26.87	73.13	16.07	0.23
-8.400E-02	-	8.267E-02	6	55	8.96	82.09	14.30	4.81
8.267E-02	-	2.493E-01	7	62	10.45	92.54	8.82	0.38
2.493E-01	-	4.160E-01	1	63	1.49	94.03	3.78	2.04
4.160E-01	-	5.827E-01	2	65	2.99	97.01	1.12	0.69
5.827E-01	-	7.493E-01	1	66	1.49	98.51	0.23	2.57
7.493E-01	-	9.160E-01	1	67	1.49	100.00	0.04	25.58
		G	0	67	0.00	100.00	3.34	3.34
		H	0	67				
		B	0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 3 (S-FE%)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
3.157E-01 XXXXXXX
4.634E-01 XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
6.802E-01 XXXXXXXXXXXXXXXXXXXXXXXXXXX
9.985E-01 XXXXXXXXX
1.466E+00 XXXXXXXXXX
2.151E+00 X
3.157E+00 XXX
4.634E+00 X
6.803E+00 X
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 3.00000E-01
MAXIMUM ANTILOG = 7.00000E+00
GEOMETRIC MEAN = 7.28996E-01
GEOMETRIC DEVIATION = 1.86771E+00
VARIANCE OF LOGS = 7.36083E-02

PERCENT TABLE FOR VARIABLE 3 (S-FE%) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	2.088587E-01	1.617554E+00

Silver Peak Conc.

D0036 GR CAL ANALYSIS - U S G S STATPAC (02/07/82) DATE 8/10/84

TITLE	INPUT ID	N	M	***** OPTIONS ****
SilverPeak	-ds-5 -	67	34	1 0 0 0 2 1 0 0 0 0

VARIABLE NO. 10 CONTAINS NO VALID DATA POINTS. THEREFORE THIS VARIABLE WILL BE SKIPPED.

THE MAX AND MIN 0.20000E+01 FOR VARIABLE NO. 14 ARE THE SAME. THEREFORE THIS VARIABLE WILL BE SKIPPED.

VARIABLE NO. 15 CONTAINS NO VALID DATA POINTS. THEREFORE THIS VARIABLE WILL BE SKIPPED.

VARIABLE NO. 24 CONTAINS NO VALID DATA POINTS. THEREFORE THIS VARIABLE WILL BE SKIPPED.

THE MAX AND MIN 0.24771E+01 FOR VARIABLE NO. 33 ARE THE SAME. THEREFORE THIS VARIABLE WILL BE SKIPPED.

D0036 GRAPHICAL ANALYSIS - U S G S STATPAC (02/07/82) DATE 7/20/84

Nevada data

FREQUENCY TABLE FOR VARIABLE 35 (AA-AS-P)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		0	0	0.00	0.00		
	L		0	0	0.00	0.00		
	T		0	0	0.00	0.00	2.99	2.99
5.830E-01	-	7.497E-01	17	17	25.37	25.37	5.25	26.29
7.497E-01	-	9.163E-01	0	17	0.00	25.37	9.67	9.67
9.163E-01	-	1.083E+00	13	30	19.40	44.78	13.42	0.01
1.083E+00	-	1.250E+00	17	47	25.37	70.15	14.00	0.64
1.250E+00	-	1.416E+00	11	58	16.42	86.57	11.00	0.00
1.416E+00	-	1.583E+00	5	63	7.46	94.03	6.51	0.35
1.583E+00	-	1.750E+00	2	65	2.99	97.01	2.90	0.28
1.750E+00	-	1.916E+00	2	67	2.99	100.00	1.27	0.42
	G		0	67	0.00	100.00	2.99	2.99
	H		0	67				
	B		0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 35 (AA-AS-P)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
4.638E+00 XXXXXXXXXXXXXXXXXXXXXXXXX
6.808E+00
9.992E+00 XXXXXXXXXXXXXXXXXXX
1.467E+01 XXXXXXXXXXXXXXXXXXXXXXXXX
2.153E+01 XXXXXXXXXXXXXXXX
3.160E+01 XXXXXXX
4.638E+01 XXX
6.808E+01 XXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 5.00000E+00
MAXIMUM ANTILOG = 7.00000E+01
GEOMETRIC MEAN = 1.28274E+01
GEOMETRIC DEVIATION = 2.03667E+00
VARIANCE OF LOGS = 9.54314E-02

PERCENT TABLE FOR VARIABLE 35 (AA-AS-P) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.493002E+00	3.111729E+01
95.00	1.637169E+00	4.336794E+01
98.00	1.000000E+35	1.000000E+35

D0036 GRAPHICAL ANALYSIS - U S G S STATPAC (02/07/82) DATE 7/20/84

Nevada data

FREQUENCY TABLE FOR VARIABLE 36 (AA-ZN-P)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		0	0	0.00	0.00		
	L		0	0	0.00	0.00		
	T		0	0	0.00	0.00	1.66	1.66
1.416E+00	-	1.583E+00	3	3	4.48	4.48	6.08	1.56
1.583E+00	-	1.749E+00	23	26	34.33	38.81	14.57	4.87
1.749E+00	-	1.916E+00	21	47	31.34	70.15	19.97	0.05
1.916E+00	-	2.083E+00	11	58	16.42	86.57	15.64	1.38
2.083E+00	-	2.249E+00	4	62	5.97	92.54	7.00	1.29
2.249E+00	-	2.416E+00	5	67	7.46	100.00	2.07	4.13
	G		0	67	0.00	100.00	1.66	1.66
	H		0	67				
	B		0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 36 (AA-ZN-P)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
3.157E+01 XXXX
4.634E+01 XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
6.802E+01 XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
9.985E+01 XXXXXXXXXXXXXXXX
1.466E+02 XXXXXX
2.151E+02 XXXXXXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 3.00000E+01
MAXIMUM ANTILOG = 2.30000E+02
GEOMETRIC MEAN = 6.96981E+01
GEOMETRIC DEVIATION = 1.65014E+00
VARIANCE OF LOGS = 4.73156E-02

PERCENT TABLE FOR VARIABLE 36 (AA-ZN-P) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	2.173502E+00	1.508348E+02
95.00	1.000000E+35	1.000000E+35
98.00	1.000000E+35	1.000000E+35

D0036 GRAPHICAL ANALYSIS - U S G S STATPAC (02/07/82) DATE 7/20/84

Nevada data

FREQUENCY TABLE FOR VARIABLE 37 (AA-SB-P)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		60	60	89.55	89.55		
	L		0	60	0.00	89.55		
	T		0	60	0.00	89.55	62.28	62.28
5.830E-01	-	7.497E-01	2	62	2.99	92.54	4.34	1.26
7.497E-01	-	9.163E-01	4	66	5.97	98.51	0.37	35.50
9.163E-01	-	1.083E+00	0	66	0.00	98.51	0.00	0.00
1.083E+00	-	1.250E+00	1	67	1.49	100.00	0.01	87.54
	G		0	67	0.00	100.00	0.00	0.00
	H		0	67				
	B		0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 37 (AA-SB-P)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
4.638E+00 XXX
6.308E+00 XXXXXX
9.992E+00
1.467E+01 X
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 4.00000E+00
MAXIMUM ANTILOG = 1.40000E+01
GEOMETRIC MEAN = 6.03125E+00
GEOMETRIC DEVIATION = 1.51837E+00
VARIANCE OF LOGS = 3.28979E-02

PERCENT TABLE FOR VARIABLE 37 (AA-SB-P) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.000000E+35	1.000000E+35
95.00	3.184171E-01	6.582898E+00
98.00	9.021673E-01	7.983022E+00

D0036 GRAPHICAL ANALYSIS - U S G S STATPAC (02/07/82) DATE 7/20/84

Nevada data

FREQUENCY TABLE FOR VARIABLE 38 (SI-F)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		0	0	0.00	0.00		
	L		0	0	0.00	0.00		
	T		0	0	0.00	0.00	0.06	0.06
2.250E+00	-	2.417E+00	1	1	2.27	2.27	1.26	0.05
2.417E+00	-	2.583E+00	6	7	13.64	15.91	8.51	0.74
2.583E+00	-	2.750E+00	17	24	38.64	54.55	18.35	0.10
2.750E+00	-	2.917E+00	18	42	40.91	95.45	12.76	2.15
2.917E+00	-	3.083E+00	2	44	4.55	100.00	3.05	0.36
	G		0	44	0.00	100.00	0.06	0.06
	H		0	44				
	B		23	67				

TOTALS LESS H AND B 44

HISTOGRAM FOR VARIABLE 38 (SI-F)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
2.154E+02 XX
3.162E+02 XXXXXXXXXXXXXX
4.642E+02 XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
6.813E+02 XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
1.000E+03 XXXXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

```
MINIMUM ANTILOG      =  2.00000E+02
MAXIMUM ANTILOG      =  9.00000E+02
GEOMETRIC MEAN       =  4.97110E+02
GEOMETRIC DEVIATION  =  1.40356E+00
VARIANCE OF LOGS     =  2.21340E-02
```

PERCENT TABLE FOR VARIABLE 38 (SI-F) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	2.894446E+00	7.842341E+02
95.00	2.914816E+00	8.218946E+02
98.00	1.000000E+35	1.000000E+35

D0036 GRAPHICAL ANALYSIS - U S G S STATPAC (02/07/82) DATE 7/20/84

Nevada data

FREQUENCY TABLE FOR VARIABLE 39 (U-INST)

LOG LIMITS LOWER - UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
N	0	0	0.00	0.00		
L	0	0	0.00	0.00		
T	0	0	0.00	0.00	0.10	0.10
-4.170E-01 - -2.503E-01	1	1	2.27	2.27	1.87	0.41
-2.503E-01 - -8.367E-02	7	8	15.91	18.18	10.79	1.33
-8.367E-02 - 8.300E-02	27	35	61.36	79.55	19.05	3.32
8.300E-02 - 2.497E-01	5	40	11.36	90.91	10.38	2.79
2.497E-01 - 4.163E-01	4	44	9.09	100.00	1.82	2.63
G	0	44	0.00	100.00	0.10	0.10
H	0	44				
B	23	67				

TOTALS LESS H AND B 44

HISTOGRAM FOR VARIABLE 39 (U-INST)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
4.638E-01 XX
6.808E-01 XXXXXXXXXXXXXXXX
9.992E-01 XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
1.467E+00 XXXXXXXXXXX
2.153E+00 XXXXXXXXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 4.50000E-01
MAXIMUM ANTILOG = 2.30000E+00
GEOMETRIC MEAN = 9.92860E-01
GEOMETRIC DEVIATION = 1.39826E+00
VARIANCE OF LOGS = 2.11958E-02

PERCENT TABLE FOR VARIABLE 39 (U-INST) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	2.363346E-01	1.723196E+00
95.00	1.000000E+35	1.000000E+35
98.00	1.000000E+35	1.000000E+35

D0036 GR. CAL ANALYSIS - U S G S STATPAC (02/07/82) DATE 8/10/84

TITLE	INPUT ID	N	M	***** OPTIONS ****
SilverPeak	-ds-5 -	67	34	1 0 0 0 2 1 0 0 0 0

NUMBER OF SELECTED VARIABLES = 27

SELECTED VARIABLE INDICES

3	4	5	6	7	8	9	11	12	13
16	17	18	19	20	21	22	23	25	26
27	28	29	30	31	32	34			

SELECTED VARIABLE IDENTIFIERS

S-FE%	S-MG%	S-CA%	S-TI%	S-MN	S-AG	S-AS	S-B	S-BA	S-BE
S-CO	S-CR	S-CU	S-LA	S-MO	S-NB	S-NI	S-PB	S-SC	S-SN
S-SR	S-V	S-W	S-Y	S-ZN	S-ZR	INST-HG			

SELECTED ROW PAIRS
1 TO 67

LOWER BOUNDARIES OF THE LOWEST CLASSES

-0.58400	-1.08400	0.08300	-0.75000	2.08300	0.08300	2.58300	1.25000	2.08300	0.25000
0.91600	1.25000	0.91600	1.58300	0.91600	1.58300	0.91600	1.25000	0.91600	1.25000
2.25000	1.25000	1.91600	1.25000	2.58300	2.41600	-0.75000			

CLASS INTERVALS

0.16667	0.16667	0.16667	0.16667	0.16667	0.16667	0.16667	0.16667	0.16667	0.16667
0.16667	0.16667	0.16667	0.16667	0.16667	0.16667	0.16667	0.16667	0.16667	0.16667
0.16667	0.16667	0.16667	0.16667	0.16667	0.16667	0.16667			

95.00	4.701688E-01	2.952356E+00
98.00	6.926692E-01	4.927983E+00

D0036 GR/ CAL ANALYSIS - U S G S STATPAC (02/07/82) DATE 8/10/84

SilverPeak

FREQUENCY TABLE FOR VARIABLE 4 (S-MG%)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
		N	0	0	0.00	0.00		
		L	0	0	0.00	0.00		
		T	0	0	0.00	0.00	1.51	1.51
-1.084E+00	-	-9.173E-01	3	3	4.48	4.48	2.83	0.01
-9.173E-01	-	-7.507E-01	6	9	8.96	13.43	5.85	0.00
-7.507E-01	-	-5.840E-01	11	20	16.42	29.85	9.55	0.22
-5.840E-01	-	-4.173E-01	13	33	19.40	49.25	12.37	0.03
-4.173E-01	-	-2.507E-01	18	51	26.87	76.12	12.68	2.23
-2.507E-01	-	-8.400E-02	7	58	10.45	86.57	10.29	1.05
-8.400E-02	-	8.267E-02	1	59	1.49	88.06	6.62	4.77
8.267E-02	-	2.493E-01	2	61	2.99	91.04	3.37	0.56
2.493E-01	-	4.160E-01	6	67	8.96	100.00	1.93	8.60
		G	0	67	0.00	100.00	1.51	1.51
		H	0	67				
		B	0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 4 (S-MG%)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
9.985E-02 XXXX
1.466E-01 XXXXXXXXX
2.151E-01 XXXXXXXXXXXXXXXX
3.157E-01 XXXXXXXXXXXXXXXXXXX
4.634E-01 XXXXXXXXXXXXXXXXXXXXXXXXXXX
6.802E-01 XXXXXXXXXX
9.985E-01 X
1.466E+00 XXX
2.151E+00 XXXXXXXXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 1.00000E-01
MAXIMUM ANTILOG = 2.00000E+00
GEOMETRIC MEAN = 3.98463E-01
GEOMETRIC DEVIATION = 2.19644E+00
VARIANCE OF LOGS = 1.16772E-01

PERCENT TABLE FOR VARIABLE 4 (S-MG%) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.910025E-01	1.552396E+00

95.0	1.000000E+35	1.000000E+35
98.0	1.000000E+35	1.000000E+35

SilverPeak

FREQUENCY TABLE FOR VARIABLE 5 (S-CA%)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
		N	0	0	0.00	0.00		
		L	0	0	0.00	0.00		
		T	0	0	0.00	0.00	0.54	0.54
8.300E-02	-	2.497E-01	1	1	1.49	1.49	1.73	0.31
2.497E-01	-	4.163E-01	4	5	5.97	7.46	4.85	0.15
4.163E-01	-	5.830E-01	12	17	17.91	25.37	9.79	0.50
5.830E-01	-	7.497E-01	23	40	34.33	59.70	14.25	5.37
7.497E-01	-	9.163E-01	8	48	11.94	71.64	14.97	3.24
9.163E-01	-	1.083E+00	5	53	7.46	79.10	11.34	3.55
1.083E+00	-	1.250E+00	10	63	14.93	94.03	6.20	2.32
1.250E+00	-	1.416E+00	4	67	5.97	100.00	3.31	0.14
		G	0	67	0.00	100.00	0.54	0.54
		H	0	67				
		B	0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 5 (S-CA%)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
1.467E+00 X
2.153E+00 XXXXXX
3.160E+00 XXXXXXXXXXXXXXXXX
4.638E+00 XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
6.808E+00 XXXXXXXXXXXX
9.992E+00 XXXXXXX
1.467E+01 XXXXXXXXXXXXXX
2.153E+01 XXXXXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

```
MINIMUM ANTILOG      =  1.50000E+00
MAXIMUM ANTILOG      =  2.00000E+01
GEOMETRIC MEAN       =  5.95310E+00
GEOMETRIC DEVIATION  =  1.93956E+00
VARIANCE OF LOGS     =  8.27731E-02
```

PERCENT TABLE FOR VARIABLE 5 (S-CA%) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.204669E+00	1.602024E+01
95.00	1.000000E+35	1.000000E+35
98.00	1.000000E+35	1.000000E+35

SilverPeak

FREQUENCY TABLE FOR VARIABLE 6 (S-TI%)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
		N	0	0	0.00	0.00		
		L	0	0	0.00	0.00		
		T	0	0	0.00	0.00	0.03	0.03
-7.500E-01	-	-5.833E-01	1	1	1.49	1.49	0.25	2.19
-5.833E-01	-	-4.167E-01	3	4	4.48	5.97	1.39	1.87
-4.167E-01	-	-2.500E-01	4	8	5.97	11.94	4.91	0.17
-2.500E-01	-	-8.333E-02	8	16	11.94	23.88	11.29	0.96
-8.333E-02	-	8.333E-02	14	30	20.90	44.78	16.87	0.49
8.333E-02	-	2.500E-01	13	43	19.40	64.18	16.37	0.69
2.500E-01	-	4.167E-01	14	57	20.90	85.07	15.88	0.22
		G	10	67	14.93	100.00	0.03	3045.33
		H	0	67				
		B	0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 6 (S-TI%)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
2.154E-01 X
3.162E-01 XXXX
4.642E-01 XXXXXX
6.813E-01 XXXXXXXXXXXX
1.000E+00 XXXXXXXXXXXXXXXXXXXXX
1.468E+00 XXXXXXXXXXXXXXXXXXX
2.154E+00 XXXXXXXXXXXXXXXXXXXXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

```
MINIMUM ANTILOG     =  2.00000E-01
MAXIMUM ANTILOG     =  2.00000E+00
GEOMETRIC MEAN      =  1.07510E+00
GEOMETRIC DEVIATION =  1.77515E+00
VARIANCE OF LOGS    =  6.21177E-02
```

PERCENT TABLE FOR VARIABLE 6 (S-TI%) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.000000E+35	1.000000E+35
95.00	1.000000E+35	1.000000E+35
98.00	1.000000E+35	1.000000E+35

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FREQUENCY TABLE FOR VARIABLE 7 (S-MN)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
		N	0	0	0.00	0.00		
		L	0	0	0.00	0.00		
		T	0	0	0.00	0.00	1.41	1.41
2.083E+00	-	2.250E+00	3	3	4.48	4.48	4.73	0.63
2.250E+00	-	2.416E+00	13	16	19.40	23.88	11.58	0.17
2.416E+00	-	2.583E+00	24	40	35.82	59.70	17.70	2.24
2.583E+00	-	2.750E+00	13	53	19.40	79.10	16.86	0.89
2.750E+00	-	2.916E+00	8	61	11.94	91.04	10.02	0.41
2.916E+00	-	3.083E+00	5	66	7.46	98.51	3.71	0.45
3.083E+00	-	3.250E+00	1	67	1.49	100.00	0.99	0.00
		G	0	67	0.00	100.00	1.41	1.41
		H	0	67				
		B	0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 7 (S-MN)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
1.467E+02 XXXX
2.153E+02 XXXXXXXXXXXXXXXXXXX
3.160E+02 XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
4.638E+02 XXXXXXXXXXXXXXXXXXX
6.808E+02 XXXXXXXXXXXX
9.992E+02 XXXXXXX
1.467E+03 X
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 1.50000E+02
MAXIMUM ANTILOG = 1.50000E+03
GEOMETRIC MEAN = 3.68054E+02
GEOMETRIC DEVIATION = 1.72815E+00
VARIANCE OF LOGS = 5.64453E-02

PERCENT TABLE FOR VARIABLE 7 (S-MN) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	2.901752E+00	7.975385E+02
95.00	3.004669E+00	1.010808E+03
98.00	3.071669E+00	1.179420E+03

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FREQUENCY TABLE FOR VARIABLE 8 (S-AG)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
		N	56	56	83.58	83.58		
		L	1	57	1.49	85.07		
		T	0	57	0.00	85.07	30.43	30.43
8.300E-02	-	2.497E-01	1	58	1.49	86.57	12.72	10.80
2.497E-01	-	4.163E-01	1	59	1.49	88.06	10.67	8.77
4.163E-01	-	5.830E-01	1	60	1.49	89.55	7.12	5.26
5.830E-01	-	7.497E-01	2	62	2.99	92.54	3.77	0.83
7.497E-01	-	9.163E-01	2	64	2.99	95.52	1.59	0.11
9.163E-01	-	1.083E+00	1	65	1.49	97.01	0.53	0.42
1.083E+00	-	1.250E+00	0	65	0.00	97.01	0.14	0.14
1.250E+00	-	1.416E+00	0	65	0.00	97.01	0.03	0.03
1.416E+00	-	1.583E+00	1	66	1.49	98.51	0.00	199.26
1.583E+00	-	1.750E+00	1	67	1.49	100.00	0.00	1356.14
		G	0	67	0.00	100.00	0.00	0.00
		H	0	67				
		B	0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 8 (S-AG)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
1.467E+00 X
2.153E+00 X
3.160E+00 X
4.638E+00 XXX
6.808E+00 XXX
9.992E+00 X
1.467E+01
2.153E+01
3.160E+01 X
4.638E+01 X
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 1.50000E+00
MAXIMUM ANTILOG = 5.00000E+01
GEOMETRIC MEAN = 6.63509E+00
GEOMETRIC DEVIATION = 3.01612E+00
VARIANCE OF LOGS = 2.29870E-01

PERCENT TABLE FOR VARIABLE 8 (S-AG) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
OF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION.
[illegible]

90.00	6.080011E-01	4.055095E+00
95.00	8.871683E-01	7.712022E+00
98.00	1.413003E+00	2.588229E+01

THE FOLLOWING

MINIMUM ANTILOG
MAXIMUM ANTILOG

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FREQUENCY TABLE FOR VARIABLE 9 (S-AS)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		63	63	94.03	94.03		
	L		2	65	2.99	97.01		
	T		0	65	0.00	97.01	0.00	0.00
2.583E+00	-	2.750E+00	1	66	1.49	98.51	66.78	64.80
2.750E+00	-	2.916E+00	1	67	1.49	100.00	0.22	2.81
	G		0	67	0.00	100.00	0.00	0.00
	H		0	67				
	B		0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 9 (S-AS)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

4.638E+02 X
6.808E+02 X

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 5.00000E+02
MAXIMUM ANTILOG = 7.00000E+02
GEOMETRIC MEAN = 5.91608E+02
GEOMETRIC DEVIATION = 1.26861E+00
VARIANCE OF LOGS = 1.06766E-02

PERCENT TABLE FOR VARIABLE 9 (S-AS) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.000000E+35	1.000000E+35
95.00	1.000000E+35	1.000000E+35
98.00	1.000000E+35	1.000000E+35

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FREQUENCY TABLE FOR VARIABLE 11 (S-B)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
		N	22	22	32.84	32.84		
		L	18	40	26.87	59.70		
		T	0	40	0.00	59.70	14.98	14.98
1.250E+00	-	1.417E+00	10	50	14.93	74.63	18.27	3.74
1.417E+00	-	1.583E+00	3	53	4.48	79.10	18.39	12.88
1.583E+00	-	1.750E+00	6	59	8.96	88.06	10.81	2.14
1.750E+00	-	1.917E+00	4	63	5.97	94.03	3.71	0.02
1.917E+00	-	2.083E+00	4	67	5.97	100.00	0.83	12.01
		G	0	67	0.00	100.00	0.00	0.00
		H	0	67				
		B	0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 11 (S-B)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
2.154E+01 XXXXXXXXXXXXXXX
3.162E+01 XXXX
4.642E+01 XXXXXXXXX
6.813E+01 XXXXXX
1.000E+02 XXXXXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 2.00000E+01
MAXIMUM ANTILOG = 1.00000E+02
GEOMETRIC MEAN = 3.91905E+01
GEOMETRIC DEVIATION = 1.85644E+00
VARIANCE OF LOGS = 7.21897E-02

PERCENT TABLE FOR VARIABLE 11 (S-B) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.804168E+00	6.370416E+01
95.00	1.000000E+35	1.000000E+35
98.00	1.000000E+35	1.000000E+35

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FREQUENCY TABLE FOR VARIABLE 12 (S-BA)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		0	0	0.00	0.00		
	L		0	0	0.00	0.00		
	T		0	0	0.00	0.00	0.92	0.92
2.083E+00	-	2.250E+00	1	1	1.49	1.49	0.94	0.00
2.250E+00	-	2.416E+00	2	3	2.99	4.48	1.62	0.09
2.416E+00	-	2.583E+00	3	6	4.48	8.96	2.58	0.07
2.583E+00	-	2.750E+00	5	11	7.46	16.42	3.79	0.38
2.750E+00	-	2.916E+00	10	21	14.93	31.34	5.13	4.64
2.916E+00	-	3.083E+00	4	25	5.97	37.31	6.37	0.88
3.083E+00	-	3.250E+00	7	32	10.45	47.76	7.30	0.01
3.250E+00	-	3.416E+00	5	37	7.46	55.22	7.69	0.94
3.416E+00	-	3.583E+00	2	39	2.99	58.21	7.46	3.99
3.583E+00	-	3.750E+00	2	41	2.99	61.19	6.66	3.26
3.750E+00	-	3.916E+00	3	44	4.48	65.67	5.47	1.12
3.916E+00	-	4.083E+00	4	48	5.97	71.64	11.07	4.52
	G		19	67	28.36	100.00	0.92	354.81
	H		0	67				
	B		0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 12 (S-BA)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
1.467E+02 X
2.153E+02 XXX
3.160E+02 XXXX
4.638E+02 XXXXXXX
6.808E+02 XXXXXXXXXXXXXXX
9.992E+02 XXXXXX
1.467E+03 XXXXXXXXXX
2.153E+03 XXXXXXX
3.160E+03 XXX
4.638E+03 XXX
6.808E+03 XXXX
9.992E+03 XXXXXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 1.50000E+02
MAXIMUM ANTILOG = 1.00000E+04
GEOMETRIC MEAN = 1.25776E+03
GEOMETRIC DEVIATION = 3.03681E+00
VARIANCE OF LOGS = 2.32726E-01

PERCENT TABLE FOR VARIABLE 12 (S-BA) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,

THE D VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.000000E+35	1.000000E+35
95.00	1.000000E+35	1.000000E+35
98.00	1.000000E+35	1.000000E+35

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FREQUENCY TABLE FOR VARIABLE 13 (S-BE)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
		N	57	57	85.07	85.07		
		L	6	63	8.96	94.03		
		T	0	63	0.00	94.03	0.42	0.42
2.500E-01	-	4.167E-01	3	66	4.48	98.51	0.00	0.00
4.167E-01	-	5.833E-01	1	67	1.49	100.00	66.58	64.59
		G	0	67	0.00	100.00	0.00	0.00
		H	0	67				
		B	0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 13 (S-BE)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
2.154E+00 XXXX
3.162E+00 X
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

```
MINIMUM ANTILOG      =  2.00000E+00
MAXIMUM ANTILOG      =  3.00000E+00
GEOMETRIC MEAN       =  2.21336E+00
GEOMETRIC DEVIATION  =  1.22474E+00
VARIANCE OF LOGS     =  7.75203E-03
```

PERCENT TABLE FOR VARIABLE 13 (S-BE) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.000000E+35	1.000000E+35
95.00	1.000000E+35	1.000000E+35
98.00	1.000000E+35	1.000000E+35

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FREQUENCY TABLE FOR VARIABLE 16 (S-CO)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
		N	29	29	43.28	43.28		
		L	24	53	35.82	79.10		
		T	0	53	0.00	79.10	15.86	15.86
9.160E-01	-	1.083E+00	11	64	16.42	95.52	26.53	9.09
1.083E+00	-	1.249E+00	0	64	0.00	95.52	19.15	19.15
1.249E+00	-	1.416E+00	1	65	1.49	97.01	4.99	3.19
1.416E+00	-	1.583E+00	1	66	1.49	98.51	0.46	0.62
1.583E+00	-	1.749E+00	0	66	0.00	98.51	0.00	0.00
1.749E+00	-	1.916E+00	0	66	0.00	98.51	0.00	0.00
1.916E+00	-	2.083E+00	0	66	0.00	98.51	0.00	0.00
2.083E+00	-	2.249E+00	1	67	1.49	100.00	0.02	63.76
		G	0	67	0.00	100.00	0.00	0.00
		H	0	67				
		B	0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 16 (S-CO)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
9.985E+00 XXXXXXXXXXXXXXXX
1.466E+01
2.151E+01 X
3.157E+01 X
4.634E+01
6.802E+01
9.985E+01
1.466E+02 X
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

```
MINIMUM ANTILOG      =  1.00000E+01
MAXIMUM ANTILOG      =  1.50000E+02
GEOMETRIC MEAN       =  1.37908E+01
GEOMETRIC DEVIATION  =  2.14540E+00
VARIANCE OF LOGS     =  1.09897E-01
```

PERCENT TABLE FOR VARIABLE 16 (S-CO) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.000000E+35	1.000000E+35
95.00	1.000000E+35	1.000000E+35
98.00	1.526001E+00	3.357386E+01

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FREQUENCY TABLE FOR VARIABLE 17 (S-CR)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
		N	4	4	5.97	5.97		
		L	6	10	8.96	14.93		
		T	0	10	0.00	14.93	7.63	7.63
1.250E+00	-	1.417E+00	14	24	20.90	35.82	10.42	1.23
1.417E+00	-	1.583E+00	9	33	13.43	49.25	14.83	2.29
1.583E+00	-	1.750E+00	15	48	22.39	71.64	15.03	0.00
1.750E+00	-	1.917E+00	16	64	23.88	95.52	10.85	2.45
1.917E+00	-	2.083E+00	1	65	1.49	97.01	5.57	3.75
2.083E+00	-	2.250E+00	0	65	0.00	97.01	2.04	2.04
2.250E+00	-	2.417E+00	1	66	1.49	98.51	0.53	0.42
2.417E+00	-	2.583E+00	0	66	0.00	98.51	0.10	0.10
2.583E+00	-	2.750E+00	1	67	1.49	100.00	0.01	68.52
		G	0	67	0.00	100.00	0.00	0.00
		H	0	67				
		B	0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 17 (S-CR)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
2.154E+01 XXXXXXXXXXXXXXXXXXXX
3.162E+01 XXXXXXXXXXXX
4.642E+01 XXXXXXXXXXXXXXXXXXXXXX
6.813E+01 XXXXXXXXXXXXXXXXXXXXXXXX
1.000E+02 X
1.468E+02
2.154E+02 X
3.162E+02
4.642E+02 X
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 2.00000E+01
MAXIMUM ANTILOG = 5.00000E+02
GEOMETRIC MEAN = 4.37127E+01
GEOMETRIC DEVIATION = 1.88724E+00
VARIANCE OF LOGS = 7.60810E-02

PERCENT TABLE FOR VARIABLE 17 (S-CR) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.878126E+00	7.553118E+01

95.00	1.913022E+00	8.185066E+01
98.00	2.303336E+00	2.010646E+02

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FREQUENCY TABLE FOR VARIABLE 18 (S-CU)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
		N	21	21	31.34	31.34		
		L	18	39	26.87	58.21		
		T	0	39	0.00	58.21	15.73	15.73
9.160E-01	-	1.083E+00	5	44	7.46	65.67	9.52	2.15
1.083E+00	-	1.249E+00	6	50	8.96	74.63	10.81	2.14
1.249E+00	-	1.416E+00	2	52	2.99	77.61	10.40	6.78
1.416E+00	-	1.583E+00	4	56	5.97	83.58	8.48	2.36
1.583E+00	-	1.749E+00	7	63	10.45	94.03	5.86	0.22
1.749E+00	-	1.916E+00	1	64	1.49	95.52	3.43	1.72
1.916E+00	-	2.083E+00	1	65	1.49	97.01	1.70	0.29
2.083E+00	-	2.249E+00	0	65	0.00	97.01	0.72	0.72
2.249E+00	-	2.416E+00	0	65	0.00	97.01	0.26	0.26
2.416E+00	-	2.583E+00	1	66	1.49	98.51	0.08	11.06
2.583E+00	-	2.749E+00	0	66	0.00	98.51	0.02	0.02
2.749E+00	-	2.916E+00	0	66	0.00	98.51	0.00	0.00
2.916E+00	-	3.083E+00	0	66	0.00	98.51	0.00	0.00
3.083E+00	-	3.249E+00	0	66	0.00	98.51	0.00	0.00
3.249E+00	-	3.416E+00	1	67	1.49	100.00	0.00	1076.76
		G	0	67	0.00	100.00	0.00	0.00
		H	0	67				
		B	0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 18 (S-CU)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
9.985E+00 XXXXXXX
1.466E+01 XXXXXXXXX
2.151E+01 XXX
3.157E+01 XXXXXX
4.634E+01 XXXXXXXXXX
6.802E+01 X
9.985E+01 X
1.466E+02
2.151E+02
3.157E+02 X
4.635E+02
6.803E+02
9.985E+02
1.466E+03
2.151E+03 X
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 1.00000E+01
MAXIMUM ANTILOG = 2.00000E+03
GEOMETRIC MEAN = 3.18397E+01

GEOMETRIC /IATION = 3.17717E+00
VARIANCE . LOGS = 2.52045E-01

PERCENT TABLE FOR VARIABLE 18 (S-CU) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.685049E+00	4.842272E+01
95.00	1.857669E+00	7.205573E+01
98.00	2.412670E+00	2.586245E+02

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FREQUENCY TABLE FOR VARIABLE 19 (S-LA)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		0	0	0.00	0.00		
	L		0	0	0.00	0.00		
	T		0	0	0.00	0.00	0.14	0.14
1.583E+00	-	1.750E+00	2	2	2.99	2.99	0.70	2.44
1.750E+00	-	1.916E+00	2	4	2.99	5.97	2.74	0.20
1.916E+00	-	2.083E+00	7	11	10.45	16.42	7.35	0.02
2.083E+00	-	2.250E+00	9	20	13.43	29.85	13.39	1.44
2.250E+00	-	2.416E+00	19	39	28.36	58.21	16.59	0.35
2.416E+00	-	2.583E+00	15	54	22.39	80.60	13.97	0.08
2.583E+00	-	2.750E+00	11	65	16.42	97.01	8.01	1.12
2.750E+00	-	2.916E+00	2	67	2.99	100.00	4.11	1.09
	G		0	67	0.00	100.00	0.14	0.14
	H		0	67				
	B		0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 19 (S-LA)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
4.638E+01 XXX
6.808E+01 XXX
9.992E+01 XXXXXXXXXX
1.467E+02 XXXXXXXXXXXXX
2.153E+02 XXXXXXXXXXXXXXXXXXXXXXXXXXX
3.160E+02 XXXXXXXXXXXXXXXXXXXXXX
4.638E+02 XXXXXXXXXXXXXXXX
6.808E+02 XXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 5.00000E+01
MAXIMUM ANTILOG = 7.00000E+02
GEOMETRIC MEAN = 2.19893E+02
GEOMETRIC DEVIATION = 1.83666E+00
VARIANCE OF LOGS = 6.97113E-02

PERCENT TABLE FOR VARIABLE 19 (S-LA) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	2.678457E+00	4.769323E+02
95.00	2.729214E+00	5.360613E+02
98.00	1.000000E+35	1.000000E+35

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FREQUENCY TABLE FOR VARIABLE 20 (S-MO)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
		N	49	49	73.13	73.13		
		L	3	52	4.48	77.61		
		T	0	52	0.00	77.61	6.52	6.52
9.160E-01	-	1.083E+00	6	58	8.96	86.57	41.39	30.26
1.083E+00	-	1.249E+00	6	64	8.96	95.52	18.59	8.52
1.249E+00	-	1.416E+00	2	66	2.99	98.51	0.00	0.00
1.416E+00	-	1.583E+00	1	67	1.49	100.00	0.50	0.50
		G	0	67	0.00	100.00	0.00	0.00
		H	0	67				
		B	0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 20 (S-MO)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
9.985E+00 XXXXXXXXX
1.466E+01 XXXXXXXXX
2.151E+01 XXX
3.157E+01 X
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 1.00000E+01
MAXIMUM ANTILOG = 3.00000E+01
GEOMETRIC MEAN = 1.38798E+01
GEOMETRIC DEVIATION = 1.39358E+00
VARIANCE OF LOGS = 2.07744E-02

PERCENT TABLE FOR VARIABLE 20 (S-MO) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.146556E+00	1.401380E+01
95.00	1.239612E+00	1.736248E+01
98.00	1.387668E+00	2.441561E+01

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FREQUENCY TABLE FOR VARIABLE 21 (S-NB)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
		N	16	16	23.88	23.88		
		L	23	39	34.33	58.21		
		T	0	39	0.00	58.21	0.57	0.57
1.583E+00	-	1.750E+00	20	59	29.85	88.06	46.77	15.32
1.750E+00	-	1.916E+00	7	66	10.45	98.51	19.64	8.14
1.916E+00	-	2.083E+00	1	67	1.49	100.00	0.02	55.47
		G	0	67	0.00	100.00	0.00	0.00
		H	0	67				
		B	0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 21 (S-NB)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
4.638E+01 XXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
6.808E+01 XXXXXXXXXX
9.992E+01 X
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 5.00000E+01
MAXIMUM ANTILOG = 1.00000E+02
GEOMETRIC MEAN = 5.57511E+01
GEOMETRIC DEVIATION = 1.20526E+00
VARIANCE OF LOGS = 6.57391E-03

PERCENT TABLE FOR VARIABLE 21 (S-NB) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.780619E+00	6.034196E+01
95.00	1.860382E+00	7.250726E+01
98.00	1.908239E+00	8.095408E+01

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FREQUENCY TABLE FOR VARIABLE 22 (S-NI)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
		N	16	16	23.88	23.88		
		L	19	35	28.36	52.24		
		T	0	35	0.00	52.24	11.71	11.71
9.160E-01	-	1.083E+00	13	48	19.40	71.64	21.13	3.13
1.083E+00	-	1.249E+00	9	57	13.43	85.07	21.58	7.33
1.249E+00	-	1.416E+00	8	65	11.94	97.01	10.15	0.46
1.416E+00	-	1.583E+00	0	65	0.00	97.01	2.19	2.19
1.583E+00	-	1.749E+00	0	65	0.00	97.01	0.22	0.22
1.749E+00	-	1.916E+00	1	66	1.49	98.51	0.00	0.00
1.916E+00	-	2.083E+00	1	67	1.49	100.00	0.01	99.00
		G	0	67	0.00	100.00	0.00	0.00
		H	0	67				
		B	0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 22 (S-NI)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
9.985E+00 XXXXXXXXXXXXXXXXXX
1.466E+01 XXXXXXXXXXXXX
2.151E+01 XXXXXXXXXXXX
3.157E+01
4.634E+01
6.802E+01 X
9.985E+01 X
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 1.00000E+01
MAXIMUM ANTILOG = 1.00000E+02
GEOMETRIC MEAN = 1.52210E+01
GEOMETRIC DEVIATION = 1.70186E+00
VARIANCE OF LOGS = 5.33254E-02

PERCENT TABLE FOR VARIABLE 22 (S-NI) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.318084E+00	2.080100E+01
95.00	1.387876E+00	2.442733E+01
98.00	1.746002E+00	5.571880E+01

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FREQUENCY TABLE FOR VARIABLE 23 (S-PB)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		0	0	0.00	0.00		
	L		2	2	2.99	2.99		
	T		0	2	0.00	2.99	7.04	7.04
1.250E+00	-	1.417E+00	8	10	11.94	14.93	4.56	2.59
1.417E+00	-	1.583E+00	14	24	20.90	35.82	6.10	10.22
1.583E+00	-	1.750E+00	7	31	10.45	46.27	7.42	0.02
1.750E+00	-	1.917E+00	9	40	13.43	59.70	8.18	0.08
1.917E+00	-	2.083E+00	4	44	5.97	65.67	8.20	2.15
2.083E+00	-	2.250E+00	5	49	7.46	73.13	7.47	0.82
2.250E+00	-	2.417E+00	4	53	5.97	79.10	6.17	0.77
2.417E+00	-	2.583E+00	7	60	10.45	89.55	4.64	1.21
2.583E+00	-	2.750E+00	2	62	2.99	92.54	3.16	0.43
2.750E+00	-	2.917E+00	1	63	1.49	94.03	1.96	0.47
2.917E+00	-	3.083E+00	1	64	1.49	95.52	1.10	0.01
3.083E+00	-	3.250E+00	2	66	2.99	98.51	0.56	3.67
3.250E+00	-	3.417E+00	0	66	0.00	98.51	0.26	0.26
3.417E+00	-	3.583E+00	1	67	1.49	100.00	0.17	3.94
	G		0	67	0.00	100.00	0.00	0.00
	H		0	67				
	B		0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 23 (S-PB)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
2.154E+01 XXXXXXXXXXXX
3.162E+01 XXXXXXXXXXXXXXXXXXXX
4.642E+01 XXXXXXXXXX
6.813E+01 XXXXXXXXXXXXX
1.000E+02 XXXXXX
1.468E+02 XXXXXXX
2.154E+02 XXXXXX
3.162E+02 XXXXXXXXXX
4.642E+02 XXX
6.813E+02 X
1.000E+03 X
1.468E+03 XXX
2.154E+03
3.162E+03 X
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

```
MINIMUM ANTILOG      =  2.00000E+01
MAXIMUM ANTILOG      =  3.00000E+03
GEOMETRIC MEAN       =  8.70451E+01
GEOMETRIC DEVIATION  =  3.40264E+00
VARIANCE OF LOGS     =  2.82828E-01
```

PERCENT TABLE FOR VARIABLE 23 (S-PB) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	2.608336E+00	4.058224E+02
95.00	3.025004E+00	1.059262E+03
98.00	3.221671E+00	1.665983E+03

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FREQUENCY TABLE FOR VARIABLE 25 (S-SC)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		2	2	2.99	2.99		
	L		9	11	13.43	16.42		
	T		0	11	0.00	16.42	6.59	6.59
9.160E-01	-	1.083E+00	14	25	20.90	37.31	10.79	0.95
1.083E+00	-	1.249E+00	10	35	14.93	52.24	16.14	2.34
1.249E+00	-	1.416E+00	17	52	25.37	77.61	16.13	0.05
1.416E+00	-	1.583E+00	5	57	7.46	85.07	10.78	3.10
1.583E+00	-	1.749E+00	7	64	10.45	95.52	4.81	1.00
1.749E+00	-	1.916E+00	3	67	4.48	100.00	1.76	0.87
	G		0	67	0.00	100.00	0.00	0.00
	H		0	67				
	U		0	67				

TOTALS LESS - FNI = 57

HISTOGRAM FOR VARIABLE 25 (S-SC)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
9.985E+00 XXXXXXXXXXXXXXXXXXXX
1.466E+01 XXXXXXXXXXXXXX
2.151E+01 XXXXXXXXXXXXXXXXXXXXXXXX
3.157E+01 XXXXXXX
4.634E+01 XXXXXXXXXX
6.802E+01 XXXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

```
MINIMUM ANTILOG      =  1.00000E+01
MAXIMUM ANTILOG      =  7.00000E+01
GEOMETRIC MEAN       =  1.98643E+01
GEOMETRIC DEVIATION  =  1.79879E+00
VARIANCE OF LOGS     =  6.50153E-02
```

PERCENT TABLE FOR VARIABLE 25 (S-SC) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.661240E+00	4.583947E+01
95.00	1.741002E+00	5.508098E+01
98.00	1.000000E+35	1.000000E+35

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FREQUENCY TABLE FOR VARIABLE 26 (S-SN)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		60	60	89.55	89.55		
	L		2	62	2.99	92.54		
	T		0	62	0.00	92.54	24.04	24.04
1.250E+00	-	1.417E+00	2	64	2.99	95.52	13.86	10.15
1.417E+00	-	1.583E+00	0	64	0.00	95.52	12.73	12.73
1.583E+00	-	1.750E+00	0	64	0.00	95.52	8.91	8.91
1.750E+00	-	1.917E+00	0	64	0.00	95.52	4.76	4.76
1.917E+00	-	2.083E+00	1	65	1.49	97.01	1.94	0.45
2.083E+00	-	2.250E+00	0	65	0.00	97.01	0.60	0.60
2.250E+00	-	2.417E+00	0	65	0.00	97.01	0.14	0.14
2.417E+00	-	2.583E+00	0	65	0.00	97.01	0.03	0.03
2.583E+00	-	2.750E+00	0	65	0.00	97.01	0.00	0.00
2.750E+00	-	2.917E+00	1	66	1.49	98.51	0.00	0.00
2.917E+00	-	3.083E+00	0	66	0.00	98.51	0.00	0.00
3.083E+00	-	3.250E+00	0	66	0.00	98.51	0.00	0.00
3.250E+00	-	3.417E+00	1	67	1.49	100.00	0.00	254.34
	G		0	67	0.00	100.00	0.00	0.00
	H		0	67				
	B		0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 26 (S-SN)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
2.154E+01 XXX
3.162E+01
4.642E+01
6.813E+01
1.000E+02 X
1.468E+02
2.154E+02
3.162E+02
4.642E+02
6.813E+02 X
1.000E+03
1.468E+03
2.154E+03 X
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 2.00000E+01
MAXIMUM ANTILOG = 2.00000E+03
GEOMETRIC MEAN = 1.41136E+02
GEOMETRIC DEVIATION = 8.02487E+00
VARIANCE OF LOGS = 8.18008E-01

PERCENT T E FOR VARIABLE 26 (S-SN) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECT PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.000000E+35	1.000000E+35
95.00	1.000000E+35	1.000000E+35
98.00	2.633336E+00	4.298691E+02

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FREQUENCY TABLE FOR VARIABLE 27 (S-SR)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		2	2	2.99	2.99		
	L		5	7	7.46	10.45		
	T		0	7	0.00	10.45	7.45	7.45
2.250E+00	-	2.417E+00	11	18	16.42	26.87	6.47	3.17
2.417E+00	-	2.583E+00	10	28	14.93	41.79	8.97	0.12
2.583E+00	-	2.750E+00	10	38	14.93	56.72	10.56	0.03
2.750E+00	-	2.917E+00	7	45	10.45	67.16	10.56	1.20
2.917E+00	-	3.083E+00	8	53	11.94	79.10	8.99	0.11
3.083E+00	-	3.250E+00	7	60	10.45	89.55	6.50	0.04
3.250E+00	-	3.417E+00	1	61	1.49	91.04	3.99	2.24
3.417E+00	-	3.583E+00	3	64	4.48	95.52	2.09	0.40
3.583E+00	-	3.750E+00	2	66	2.99	98.51	0.93	1.25
3.750E+00	-	3.917E+00	1	67	1.49	100.00	0.50	0.50
	G		0	67	0.00	100.00	0.00	0.00
	H		0	67				
	B		0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 27 (S-SR)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
2.154E+02 XXXXXXXXXXXXXXXX
3.162E+02 XXXXXXXXXXXXXXX
4.642E+02 XXXXXXXXXXXXXXX
6.813E+02 XXXXXXXXXX
1.000E+03 XXXXXXXXXXXX
1.468E+03 XXXXXXXXXX
2.154E+03 X
3.162E+03 XXXX
4.642E+03 XXX
6.813E+03 X
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

```
MINIMUM ANTILOG      =  2.00000E+02
MAXIMUM ANTILOG      =  7.00000E+03
GEOMETRIC MEAN       =  6.35721E+02
GEOMETRIC DEVIATION  =  2.52438E+00
VARIANCE OF LOGS     =  1.61729E-01
```

PERCENT TABLE FOR VARIABLE 27 (S-SR) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE

90.00	3.300002E+00	1.995272E+03
95.00	3.563892E+00	3.663460E+03
98.00	3.721670E+00	5.268289E+03

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FREQUENCY TABLE FOR VARIABLE 28 (S-V)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
		N	0	0	0.00	0.00		
		L	0	0	0.00	0.00		
		T	0	0	0.00	0.00	0.43	0.43
1.250E+00	-	1.417E+00	4	4	5.97	5.97	2.01	1.97
1.417E+00	-	1.583E+00	4	8	5.97	11.94	6.64	1.05
1.583E+00	-	1.750E+00	14	22	20.90	32.84	13.83	0.00
1.750E+00	-	1.917E+00	22	44	32.84	65.67	18.14	0.82
1.917E+00	-	2.083E+00	12	56	17.91	83.58	14.99	0.60
2.083E+00	-	2.250E+00	8	64	11.94	95.52	7.80	0.01
2.250E+00	-	2.417E+00	3	67	4.48	100.00	3.16	0.01
		G	0	67	0.00	100.00	0.43	0.43
		H	0	67				
		B	0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 28 (S-V)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
2.154E+01 XXXXXX
3.162E+01 XXXXXX
4.642E+01 XXXXXXXXXXXXXXXXXXXX
6.813E+01 XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
1.000E+02 XXXXXXXXXXXXXXXXXX
1.468E+02 XXXXXXXXXXXX
2.154E+02 XXXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 2.00000E+01
MAXIMUM ANTILOG = 2.00000E+02
GEOMETRIC MEAN = 7.04358E+01
GEOMETRIC DEVIATION = 1.73913E+00
VARIANCE OF LOGS = 5.77593E-02

PERCENT TABLE FOR VARIABLE 28 (S-V) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	2.172919E+00	1.489082E+02
95.00	2.242710E+00	1.748680E+02
98.00	1.000000E+35	1.000000E+35

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FREQUENCY TABLE FOR VARIABLE 29 (S-W)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
		N	55	55	82.09	82.09		
		L	5	60	7.46	89.55		
		T	0	60	0.00	89.55	20.40	20.40
1.916E+00	-	2.083E+00	1	61	1.49	91.04	12.41	10.49
2.083E+00	-	2.249E+00	1	62	1.49	92.54	12.56	10.64
2.249E+00	-	2.416E+00	0	62	0.00	92.54	10.09	10.09
2.416E+00	-	2.583E+00	1	63	1.49	94.03	6.43	4.59
2.583E+00	-	2.749E+00	0	63	0.00	94.03	3.25	3.25
2.749E+00	-	2.916E+00	0	63	0.00	94.03	1.31	1.31
2.916E+00	-	3.083E+00	1	64	1.49	95.52	0.42	0.82
3.083E+00	-	3.249E+00	1	65	1.49	97.01	0.11	7.63
3.249E+00	-	3.416E+00	1	66	1.49	98.51	0.02	45.55
3.416E+00	-	3.583E+00	0	66	0.00	98.51	0.00	0.00
3.583E+00	-	3.749E+00	0	66	0.00	98.51	0.00	0.00
3.749E+00	-	3.916E+00	0	66	0.00	98.51	0.00	0.00
3.916E+00	-	4.083E+00	1	67	1.49	100.00	0.00	260.48
		G	0	67	0.00	100.00	0.00	0.00
		H	0	67				
		B	0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 29 (S-W)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
9.985E+01 X
1.466E+02 X
2.151E+02
3.157E+02 X
4.634E+02
6.802E+02
9.985E+02 X
1.466E+03 X
2.151E+03 X
3.157E+03
4.635E+03
6.803E+03
9.985E+03 X
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

```
MINIMUM ANTILOG      =  1.00000E+02
MAXIMUM ANTILOG      =  1.00000E+04
GEOMETRIC MEAN       =  7.51211E+02
GEOMETRIC DEVIATION  =  5.04738E+00
VARIANCE OF LOGS     =  4.94301E-01
```

PERCENT T FOR VARIABLE 29 (S-W) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTL PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.000000E+35	1.000000E+35
95.00	2.907669E+00	8.084786E+02
98.00	3.359336E+00	2.287369E+03

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FREQUENCY TABLE FOR VARIABLE 30 (S-Y)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
		N	0	0	0.00	0.00		
		L	0	0	0.00	0.00		
		T	0	0	0.00	0.00	0.10	0.10
1.250E+00	-	1.417E+00	1	1	1.49	1.49	0.36	1.13
1.417E+00	-	1.583E+00	5	6	7.46	8.96	1.25	11.27
1.583E+00	-	1.750E+00	1	7	1.49	10.45	3.33	1.63
1.750E+00	-	1.917E+00	1	8	1.49	11.94	6.87	5.02
1.917E+00	-	2.083E+00	8	16	11.94	23.88	10.94	0.79
2.083E+00	-	2.250E+00	13	29	19.40	43.28	13.44	0.01
2.250E+00	-	2.417E+00	22	51	32.84	76.12	12.75	6.71
2.417E+00	-	2.583E+00	9	60	13.43	89.55	9.34	0.01
2.583E+00	-	2.750E+00	6	66	8.96	98.51	5.28	0.10
2.750E+00	-	2.917E+00	1	67	1.49	100.00	3.33	1.63
		G	0	67	0.00	100.00	0.10	0.10
		H	0	67				
		B	0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 30 (S-Y)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
2.154E+01 X
3.162E+01 XXXXXXX
4.642E+01 X
6.813E+01 X
1.000E+02 XXXXXXXXXXXX
1.468E+02 XXXXXXXXXXXXXXXXXX
2.154E+02 XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
3.162E+02 XXXXXXXXXXXXX
4.642E+02 XXXXXXXXX
6.813E+02 X
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 2.00000E+01
MAXIMUM ANTILOG = 7.00000E+02
GEOMETRIC MEAN = 1.64457E+02
GEOMETRIC DEVIATION = 2.10923E+00
VARIANCE OF LOGS = 1.05057E-01

PERCENT TABLE FOR VARIABLE 30 (S-Y) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE

90.00	2.591669E+00	3.905434E+02
95.00	2.684725E+00	4.638660E+02
98.00	2.740559E+00	5.502481E+02

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FREQUENCY TABLE FOR VARIABLE 31 (S-ZN)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		60	60	89.55	89.55		
	L		2	62	2.99	92.54		
	T		0	62	0.00	92.54	9.38	9.38
2.583E+00	-	2.750E+00	3	65	4.48	97.01	31.32	25.60
2.750E+00	-	2.916E+00	1	66	1.49	98.51	22.82	20.86
2.916E+00	-	3.083E+00	0	66	0.00	98.51	3.39	3.39
3.083E+00	-	3.250E+00	0	66	0.00	98.51	0.00	0.00
3.250E+00	-	3.416E+00	0	66	0.00	98.51	0.00	0.00
3.416E+00	-	3.583E+00	0	66	0.00	98.51	0.00	0.00
3.583E+00	-	3.750E+00	1	67	1.49	100.00	0.10	8.40
	G		0	67	0.00	100.00	0.00	0.00
	H		0	67				
	B		0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 31 (S-ZN)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
4.638E+02 XXXX
6.808E+02 X
9.992E+02
1.467E+03
2.153E+03
3.160E+03
4.638E+03 X
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 5.00000E+02
MAXIMUM ANTILOG = 5.00000E+03
GEOMETRIC MEAN = 8.47609E+02
GEOMETRIC DEVIATION = 2.72582E+00
VARIANCE OF LOGS = 1.89658E-01

PERCENT TABLE FOR VARIABLE 31 (S-ZN) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.000000E+35	1.000000E+35
95.00	1.000000E+35	1.000000E+35
98.00	2.859667E+00	7.238811E+02

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FREQUENCY TABLE FOR VARIABLE 32 (S-ZR)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		0	0	0.00	0.00		
	L		0	0	0.00	0.00		
	T		0	0	0.00	0.00	0.00	0.00
2.416E+00	-	2.583E+00	1	1	1.49	1.49	0.00	0.00
2.583E+00	-	2.749E+00	2	3	2.99	4.48	0.01	353.49
2.749E+00	-	2.916E+00	0	3	0.00	4.48	0.50	0.50
2.916E+00	-	3.083E+00	0	3	0.00	4.48	6.34	6.34
3.083E+00	-	3.249E+00	3	6	4.48	8.96	23.72	18.10
3.249E+00	-	3.416E+00	4	10	5.97	14.93	36.44	28.88
	G		57	67	85.07	100.00	0.00	0.00
	H		0	67				
	B		0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 32 (S-ZR)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
3.157E+02 X
4.634E+02 XXX
6.802E+02
9.985E+02
1.466E+03 XXXX
2.151E+03 XXXXXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

```
MINIMUM ANTILOG      =  3.00000E+02
MAXIMUM ANTILOG      =  2.00000E+03
GEOMETRIC MEAN       =  1.15013E+03
GEOMETRIC DEVIATION  =  2.04876E+00
VARIANCE OF LOGS     =  9.70266E-02
```

PERCENT TABLE FOR VARIABLE 32 (S-ZR) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.000000E+35	1.000000E+35
95.00	1.000000E+35	1.000000E+35
98.00	1.000000E+35	1.000000E+35

D0036 GR ICAL ANALYSIS - U S G S STATPAC (02/07/82) DATE 8/10/84

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FREQUENCY TABLE FOR VARIABLE 34 (INST-HG)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
		N	0	0	0.00	0.00		
		L	28	28	41.79	41.79		
		T	0	28	0.00	41.79	13.56	13.56
-7.500E-01	-	-5.833E-01	8	36	11.94	53.73	5.59	1.04
-5.833E-01	-	-4.167E-01	2	38	2.99	56.72	6.50	3.12
-4.167E-01	-	-2.500E-01	7	45	10.45	67.16	7.04	0.00
-2.500E-01	-	-8.333E-02	3	48	4.48	71.64	7.09	2.36
-8.333E-02	-	8.333E-02	0	48	0.00	71.64	6.66	6.66
8.333E-02	-	2.500E-01	1	49	1.49	73.13	5.82	4.00
2.500E-01	-	4.167E-01	5	54	7.46	80.60	4.74	0.01
4.167E-01	-	5.833E-01	2	56	2.99	83.58	3.60	0.71
5.833E-01	-	7.500E-01	2	58	2.99	86.57	6.40	3.02
		G	9	67	13.43	100.00	0.00	0.00
		H	0	67				
		B	0	67				

TOTALS LESS H AND B 67

HISTOGRAM FOR VARIABLE 34 (INST-HG)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
2.154E-01 XXXXXXXXXXXX
3.162E-01 XXX
4.642E-01 XXXXXXXXXX
6.813E-01 XXXX
1.000E+00
1.468E+00 X
2.154E+00 XXXXXXX
3.162E+00 XXX
4.642E+00 XXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

```
MINIMUM ANTILOG      =  2.00000E-01
MAXIMUM ANTILOG      =  4.40000E+00
GEOMETRIC MEAN       =  6.86090E-01
GEOMETRIC DEVIATION  =  2.77284E+00
VARIANCE OF LOGS     =  1.96182E-01
```

PERCENT TABLE FOR VARIABLE 34 (INST-HG) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.000000E+35	1.000000E+35

95.00	1.000000E+35	1.000000E+35
98.00	1.000000E+35	1.000000E+35

Silver Peak rocks -

D0036 GRAPHICAL ANALYSIS - U S G S STATPAC (02/07/82) DATE 7/20/84

TITLE	INPUT ID	N	M	***** OPTIONS ****
Nevada data	-ds-6 -	29	38	1 0 0 0 2 1 0 0 0 0

VARIABLE NO. 10 CONTAINS NO VALID DATA POINTS. THEREFORE THIS VARIABLE WILL BE SKIPPED.

VARIABLE NO. 14 CONTAINS NO VALID DATA POINTS. THEREFORE THIS VARIABLE WILL BE SKIPPED.

VARIABLE NO. 21 CONTAINS NO VALID DATA POINTS. THEREFORE THIS VARIABLE WILL BE SKIPPED.

VARIABLE NO. 26 CONTAINS NO VALID DATA POINTS. THEREFORE THIS VARIABLE WILL BE SKIPPED.

THE MAX AND MIN 0.20000E+01 FOR VARIABLE NO. 29 ARE THE SAME. THEREFORE THIS VARIABLE WILL BE SKIPPED.

VARIABLE NO. 33 CONTAINS NO VALID DATA POINTS. THEREFORE THIS VARIABLE WILL BE SKIPPED.

D0036 GRAPHICAL ANALYSIS - U S G S STATPAC (02/07/82) DATE 7/20/84

TITLE	INPUT ID		N	M	***** OPTIONS ****
Nevada data	-ds-6	-	29	38	1 0 0 0 2 1 0 0 0 0

NUMBER OF SELECTED VARIABLES = 30

SELECTED VARIABLE INDICES

3	4	5	6	7	8	9	11	12	13
15	16	17	18	19	20	22	23	24	25
27	28	30	31	32	34	35	36	37	38

SELECTED VARIABLE IDENTIFIERS

S-FE%	S-MG%	S-CA%	S-TI%	S-MN	S-AG	S-AS	S-B	S-BA	S-BE
S-CD	S-CO	S-CR	S-CU	S-LA	S-MO	S-NI	S-PB	S-SB	S-SC
S-SR	S-V	S-Y	S-ZN	S-ZR	AA-AU-P	INST-HG	AA-AS-P	AA-ZN-P	AA-SB-P

SELECTED ROW PAIRS
1 TO 29

LOWER BOUNDARIES OF THE LOWEST CLASSES

-0.91700	-1.75000	-1.41700	-2.75000	1.08300	-0.41700	2.25000	0.91600	1.41600	-0.08400
1.25000	0.58300	0.91600	0.58300	1.25000	0.58300	0.58300	1.08300	1.91600	0.58300
1.91600	0.91600	0.91600	2.25000	0.91600	-1.08400	-1.75000	0.58300	0.91600	0.25000

CLASS INTERVALS

0.16667	0.16667	0.16667	0.16667	0.16667	0.16667	0.16667	0.16667	0.16667	0.16667
0.16667	0.16667	0.16667	0.16667	0.16667	0.16667	0.16667	0.16667	0.16667	0.16667
0.16667	0.16667	0.16667	0.16667	0.16667	0.16667	0.16667	0.16667	0.16667	0.16667

D0036 GRAPHICAL ANALYSIS - U S G S STATPAC (02/07/82) DATE 7/20/84

Nevada data

FREQUENCY TABLE FOR VARIABLE 3 (S-FE%)

LOG LIMITS LOWER	- UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N	0	0	0.00	0.00		
	L	0	0	0.00	0.00		
	T	0	0	0.00	0.00	1.81	1.81
-9.170E-01	- -7.503E-01	1	1	3.45	3.45	1.44	0.13
-7.503E-01	- -5.837E-01	4	5	13.79	17.24	2.11	1.69
-5.837E-01	- -4.170E-01	6	11	20.69	37.93	2.80	3.64
-4.170E-01	- -2.503E-01	1	12	3.45	41.38	3.37	1.66
-2.503E-01	- -8.367E-02	7	19	24.14	65.52	3.66	3.06
-8.367E-02	- 8.300E-02	2	21	6.90	72.41	3.59	0.70
8.300E-02	- 2.497E-01	1	22	3.45	75.86	3.18	1.50
2.497E-01	- 4.163E-01	1	23	3.45	79.31	2.55	0.95
4.163E-01	- 5.830E-01	2	25	6.90	86.21	1.85	0.01
5.830E-01	- 7.497E-01	1	26	3.45	89.66	1.21	0.04
7.497E-01	- 9.163E-01	2	28	6.90	96.55	0.72	2.28
9.163E-01	- 1.083E+00	1	29	3.45	100.00	0.70	0.12
	G	0	29	0.00	100.00	1.81	1.81
	H	0	29				
	B	0	29				

TOTALS LESS H AND B 29

HISTOGRAM FOR VARIABLE 3 (S-FE%)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
1.467E-01 XXX
2.153E-01 XXXXXXXXXXXXXX
3.160E-01 XXXXXXXXXXXXXXXXXXXXX
4.638E-01 XXX
6.803E-01 XXXXXXXXXXXXXXXXXXXXXXXXX
9.992E-01 XXXXXXX
1.467E+00 XXX
2.153E+00 XXX
3.160E+00 XXXXXXX
4.638E+00 XXX
6.808E+00 XXXXXXX
9.992E+00 XXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

```
MINIMUM ANTILOG      =  1.50000E-01
MAXIMUM ANTILOG      =  1.00000E+01
GEOMETRIC MEAN       =  7.68162E-01
GEOMETRIC DEVIATION  =  3.33075E+00
VARIANCE OF LOGS     =  2.73050E-01
```

PERCENT TABLE FOR VARIABLE 3 (S-FE%) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,

THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	7.580033E-01	5.723004E+00
95.00	8.783369E-01	7.565487E+00
98.00	1.000000E+35	1.000000E+35

D0036 GRAPHICAL ANALYSIS - U S G S STATPAC (02/07/82) DATE 7/20/84

Nevada data

FREQUENCY TABLE FOR VARIABLE 4 (S-MG%)

LOG LIMITS LOWER - UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
N	0	0	0.00	0.00		
L	8	8	27.59	27.59		
T	0	8	0.00	27.59	5.89	5.89
-1.750E+00 - -1.583E+00	5	13	17.24	44.83	3.14	1.11
-1.583E+00 - -1.417E+00	4	17	13.79	58.62	3.70	0.02
-1.417E+00 - -1.250E+00	4	21	13.79	72.41	3.89	0.00
-1.250E+00 - -1.083E+00	1	22	3.45	75.86	3.66	1.93
-1.083E+00 - -9.167E-01	2	24	6.90	82.76	3.07	0.37
-9.167E-01 - -7.500E-01	2	26	6.90	89.66	2.30	0.04
-7.500E-01 - -5.833E-01	1	27	3.45	93.10	1.54	0.19
-5.833E-01 - -4.167E-01	0	27	0.00	93.10	0.92	0.92
-4.167E-01 - -2.500E-01	1	28	3.45	96.55	0.49	0.53
-2.500E-01 - -8.333E-02	0	28	0.00	96.55	0.23	0.23
-8.333E-02 - 8.334E-02	0	28	0.00	96.55	0.10	0.10
8.334E-02 - 2.500E-01	0	28	0.00	96.55	0.04	0.04
2.500E-01 - 4.167E-01	1	29	3.45	100.00	0.02	53.52
G	0	29	0.00	100.00	0.00	0.00
H	0	29				
B	0	29				

TOTALS LESS H AND B 29

HISTOGRAM FOR VARIABLE 4 (S-MG%)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
2.154E-02 XXXXXXXXXXXXXXXXX
3.162E-02 XXXXXXXXXXXXXX
4.642E-02 XXXXXXXXXXXXXX
6.813E-02 XXX
1.000E-01 XXXXXXX
1.463E-01 XXXXXXX
2.154E-01 XXX
3.162E-01
4.642E-01 XXX
6.813E-01
1.000E+00
1.463E+00
2.154E+00 XXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 2.00000E-02
MAXIMUM ANTILOG = 2.00000E+00
GEOMETRIC MEAN = 6.24613E-02
GEOMETRIC DEVIATION = 3.30086E+00
VARIANCE OF LOGS = 2.68974E-01

PERCENT TABLE FOR VARIABLE 4 (S-MG%) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	-7.333313E-01	1.847858E-01
95.00	-3.999973E-01	3.981096E-01
98.00	1.000000E+35	1.000000E+35

D0036 GRAPHICAL ANALYSIS - U S G S STATPAC (02/07/82) DATE 7/20/84

Nevada data

FREQUENCY TABLE FOR VARIABLE 5 (S-CA%)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
		N	0	0	0.00	0.00		
		L	1	1	3.45	3.45		
		T	0	1	0.00	3.45	1.32	1.32
-1.417E+00	-	-1.250E+00	2	3	6.90	10.34	0.67	2.63
-1.250E+00	-	-1.084E+00	1	4	3.45	13.79	0.91	0.01
-1.084E+00	-	-9.170E-01	1	5	3.45	17.24	1.18	0.03
-9.170E-01	-	-7.503E-01	2	7	6.90	24.14	1.47	0.19
-7.503E-01	-	-5.837E-01	2	9	6.90	31.03	1.75	0.04
-5.837E-01	-	-4.170E-01	2	11	6.90	37.93	2.01	0.00
-4.170E-01	-	-2.503E-01	0	11	0.00	37.93	2.21	2.21
-2.503E-01	-	-8.366E-02	3	14	10.34	48.28	2.33	0.20
-8.366E-02	-	8.300E-02	3	17	10.34	58.62	2.35	0.18
8.300E-02	-	2.497E-01	0	17	0.00	58.62	2.28	2.28
2.497E-01	-	4.163E-01	0	17	0.00	58.62	2.13	2.13
4.163E-01	-	5.830E-01	3	20	10.34	68.97	1.90	0.64
5.830E-01	-	7.497E-01	3	23	10.34	79.31	1.63	1.16
7.497E-01	-	9.163E-01	3	26	10.34	89.66	1.34	2.06
9.163E-01	-	1.083E+00	1	27	3.45	93.10	1.06	0.00
1.083E+00	-	1.250E+00	1	28	3.45	96.55	0.80	0.05
1.250E+00	-	1.416E+00	1	29	3.45	100.00	1.67	0.27
		G	0	29	0.00	100.00	0.00	0.00
		H	0	29				
		B	0	29				

TOTALS LESS H AND B 29

HISTOGRAM FOR VARIABLE 5 (S-CA%)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
4.633E-02 XXXXXXX
6.808E-02 XXX
9.992E-02 XXX
1.467E-01 XXXXXXX
2.153E-01 XXXXXXX
3.160E-01 XXXXXXX
4.633E-01
6.808E-01 XXXXXXXXXX
9.992E-01 XXXXXXXXXX
1.467E+00
2.153E+00
3.160E+00 XXXXXXXXXX
4.633E+00 XXXXXXXXXX
6.808E+00 XXXXXXXXXX
9.992E+00 XXX
1.467E+01 XXX
2.153E+01 XXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

```
MINIMUM ANTILOG      =  5.00000E-02
MAXIMUM ANTILOG      =  2.00000E+01
GEOMETRIC MEAN       =  1.01889E+00
GEOMETRIC DEVIATION  =  6.22840E+00
VARIANCE OF LOGS     =  6.31034E-01
```

PERCENT TABLE FOR VARIABLE 5 (S-CA%) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	9.330047E-01	8.570471E+00
95.00	1.174672E+00	1.495106E+01
98.00	1.000000E+35	1.000000E+35

D0036 GRAPHICAL ANALYSIS - U S G S STATPAC (02/07/82) DATE 7/20/84

Nevada data

FREQUENCY TABLE FOR VARIABLE 6 (S-TIX)

LOG LIMITS LOWER - UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
N	8	8	27.59	27.59		
L	3	11	10.34	37.93		
T	0	11	0.00	37.93	4.27	4.27
-2.750E+00 - -2.583E+00	1	12	3.45	41.38	1.67	0.27
-2.583E+00 - -2.417E+00	0	12	0.00	41.38	2.01	2.01
-2.417E+00 - -2.250E+00	2	14	6.90	48.28	2.30	0.04
-2.250E+00 - -2.083E+00	1	15	3.45	51.72	2.50	0.90
-2.083E+00 - -1.917E+00	1	16	3.45	55.17	2.58	0.97
-1.917E+00 - -1.750E+00	1	17	3.45	58.62	2.54	0.94
-1.750E+00 - -1.583E+00	2	19	6.90	65.52	2.38	0.06
-1.583E+00 - -1.417E+00	1	20	3.45	68.97	2.12	0.59
-1.417E+00 - -1.250E+00	3	23	10.34	79.31	1.80	0.81
-1.250E+00 - -1.083E+00	1	24	3.45	82.76	1.45	0.14
-1.083E+00 - -9.167E-01	1	25	3.45	86.21	1.11	0.01
-9.167E-01 - -7.500E-01	3	28	10.34	96.55	0.81	5.92
-7.500E-01 - -5.833E-01	1	29	3.45	100.00	1.47	0.15
G	0	29	0.00	100.00	0.00	0.00
H	0	29				
B	0	29				

TOTALS LESS H AND B 29

HISTOGRAM FOR VARIABLE 6 (S-TIX)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
2.154E-03 XXX
3.162E-03
4.642E-03 XXXXXXX
6.813E-03 XXX
1.000E-02 XXX
1.468E-02 XXX
2.154E-02 XXXXXXX
3.162E-02 XXX
4.642E-02 XXXXXXXXXX
6.813E-02 XXX
1.000E-01 XXX
1.468E-01 XXXXXXXXXX
2.154E-01 XXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

```
MINIMUM ANTILOG      =  2.00000E-03
MAXIMUM ANTILOG      =  2.00000E-01
GEOMETRIC MEAN       =  2.99328E-02
GEOMETRIC DEVIATION  =  3.96082E+00
VARIANCE OF LOGS     =  3.57348E-01
```

PERCENT TABLE FOR VARIABLE 6 (S-TI%) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	-8.555518E-01	1.394595E-01
95.00	-7.749961E-01	1.678819E-01
98.00	1.000000E+35	1.000000E+35

D0036 GRAPHICAL ANALYSIS - U S G S STATPAC (02/07/82) DATE 7/20/84

Nevada data

FREQUENCY TABLE FOR VARIABLE 7 (S-MN)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		0	0	0.00	0.00		
	L		0	0	0.00	0.00		
	T		0	0	0.00	0.00	0.15	0.15
1.083E+00	-	1.250E+00	1	1	3.45	3.45	0.13	5.93
1.250E+00	-	1.416E+00	0	1	0.00	3.45	0.22	0.22
1.416E+00	-	1.583E+00	0	1	0.00	3.45	0.35	0.35
1.583E+00	-	1.750E+00	0	1	0.00	3.45	0.54	0.54
1.750E+00	-	1.916E+00	0	1	0.00	3.45	0.78	0.78
1.916E+00	-	2.083E+00	3	4	10.34	13.79	1.09	3.38
2.083E+00	-	2.250E+00	2	6	6.90	20.69	1.43	0.23
2.250E+00	-	2.416E+00	3	9	10.34	31.03	1.78	0.83
2.416E+00	-	2.583E+00	0	9	0.00	31.03	2.12	2.12
2.583E+00	-	2.750E+00	3	12	10.34	41.38	2.39	0.15
2.750E+00	-	2.916E+00	0	12	0.00	41.38	2.57	2.57
2.916E+00	-	3.083E+00	2	14	6.90	48.28	2.61	0.14
3.083E+00	-	3.250E+00	2	16	6.90	55.17	2.53	0.11
3.250E+00	-	3.416E+00	1	17	3.45	58.62	2.33	0.76
3.416E+00	-	3.583E+00	1	18	3.45	62.07	2.03	0.53
3.583E+00	-	3.750E+00	3	21	10.34	72.41	5.95	1.47
	G		8	29	27.59	100.00	0.15	423.88
	H		0	29				
	B		0	29				

TOTALS LESS H AND B 29

HISTOGRAM FOR VARIABLE 7 (S-MN)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
1.467E+01 XXX
2.153E+01
3.160E+01
4.638E+01
6.808E+01
9.992E+01 XXXXXXXXXX
1.467E+02 XXXXXXX
2.153E+02 XXXXXXXXXX
3.160E+02
4.638E+02 XXXXXXXXXX
6.808E+02
9.992E+02 XXXXXXX
1.467E+03 XXXXXXX
2.153E+03 XXX
3.160E+03 XXX
4.638E+03 XXXXXXXXXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 1.50000E+01

```
MAXIMUM ANTILOG      =  5.00000E+03
GEOMETRIC MEAN       =  5.04247E+02
GEOMETRIC DEVIATION  =  4.85249E+00
VARIANCE OF LOGS     =  4.70548E-01
```

PERCENT TABLE FOR VARIABLE 7 (S-MN) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.000000E+35	1.000000E+35
95.00	1.000000E+35	1.000000E+35
98.00	1.000000E+35	1.000000E+35

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Nevada data

FREQUENCY TABLE FOR VARIABLE 8 (S-AG)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
		N	2	2	6.90	6.90		
		L	1	3	3.45	10.34		
		T	0	3	0.00	10.34	1.38	1.38
-4.170E-01	-	-2.503E-01	1	4	3.45	13.79	0.47	0.59
-2.503E-01	-	-8.367E-02	0	4	0.00	13.79	0.59	0.59
-8.367E-02	-	8.300E-02	0	4	0.00	13.79	0.72	0.72
8.300E-02	-	2.497E-01	1	5	3.45	17.24	0.86	0.02
2.497E-01	-	4.163E-01	2	7	6.90	24.14	1.01	0.97
4.163E-01	-	5.830E-01	1	8	3.45	27.59	1.16	0.02
5.830E-01	-	7.497E-01	0	8	0.00	27.59	1.30	1.30
7.497E-01	-	9.163E-01	3	11	10.34	37.93	1.43	1.73
9.163E-01	-	1.083E+00	1	12	3.45	41.38	1.54	0.19
1.083E+00	-	1.250E+00	1	13	3.45	44.83	1.62	0.24
1.250E+00	-	1.416E+00	0	13	0.00	44.83	1.67	1.67
1.416E+00	-	1.583E+00	0	13	0.00	44.83	1.68	1.68
1.583E+00	-	1.750E+00	1	14	3.45	48.28	1.67	0.27
1.750E+00	-	1.916E+00	2	16	6.90	55.17	1.61	0.09
1.916E+00	-	2.083E+00	1	17	3.45	58.62	1.53	0.18
2.083E+00	-	2.250E+00	2	19	6.90	65.52	1.42	0.24
2.250E+00	-	2.416E+00	2	21	6.90	72.41	1.29	0.40
2.416E+00	-	2.583E+00	3	24	10.34	82.76	1.14	3.02
2.583E+00	-	2.750E+00	2	26	6.90	89.66	0.99	1.02
2.750E+00	-	2.916E+00	1	27	3.45	93.10	0.85	0.03
2.916E+00	-	3.083E+00	0	27	0.00	93.10	0.71	0.71
3.083E+00	-	3.250E+00	1	28	3.45	96.55	0.58	0.31
3.250E+00	-	3.416E+00	1	29	3.45	100.00	1.80	0.36
		G	0	29	0.00	100.00	0.00	0.00
		H	0	29				
		B	0	29				

TOTALS LESS H AND B 29

HISTOGRAM FOR VARIABLE 8 (S-AG)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
4.638E-01 XXX
6.808E-01
9.992E-01
1.467E+00 XXX
2.153E+00 XXXXXXX
3.160E+00 XXX
4.638E+00
6.808E+00 XXXXXXXXXX
9.992E+00 XXX
1.467E+01 XXX
2.153E+01
3.160E+01
4.638E+01 XXX
6.808E+01 XXXXXXX
9.992E+01 XXX
```

```
1.467E+02 XXXXXXX
2.153E+02 XXXXXXX
3.160E+02 XXXXXXXXXX
4.638E+02 XXXXXXX
6.808E+02 XXX
9.992E+02
1.467E+03 XXX
2.153E+03 XXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

```
MINIMUM ANTILOG      =  5.00000E-01
MAXIMUM ANTILOG      =  2.00000E+03
GEOMETRIC MEAN       =  4.99440E+01
GEOMETRIC DEVIATION  =  1.04015E+01
VARIANCE OF LOGS     =  1.03448E+00
```

PERCENT TABLE FOR VARIABLE 8 (S-AG) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	2.766340E+00	5.839016E+02
95.00	3.099674E+00	1.257980E+03
98.00	1.000000E+35	1.000000E+35

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Nevada data

FREQUENCY TABLE FOR VARIABLE 9 (S-AS)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		17	17	58.62	58.62		
	L		2	19	6.90	65.52		
	T		0	19	0.00	65.52	7.89	7.89
2.250E+00	-	2.417E+00	3	22	10.34	75.86	6.13	1.59
2.417E+00	-	2.583E+00	1	23	3.45	79.31	6.27	4.43
2.583E+00	-	2.750E+00	4	27	13.79	93.10	4.70	0.10
2.750E+00	-	2.917E+00	1	28	3.45	96.55	2.59	0.97
2.917E+00	-	3.083E+00	0	28	0.00	96.55	1.04	1.04
3.083E+00	-	3.250E+00	0	28	0.00	96.55	0.31	0.31
3.250E+00	-	3.417E+00	0	28	0.00	96.55	0.07	0.07
3.417E+00	-	3.583E+00	0	28	0.00	96.55	0.01	0.01
3.583E+00	-	3.750E+00	1	29	3.45	100.00	0.00	746.30
	G		0	29	0.00	100.00	0.00	0.00
	H		0	29				
	B		0	29				

TOTALS LESS H AND B 29

HISTOGRAM FOR VARIABLE 9 (S-AS)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
2.154E+02 XXXXXXXXXX
3.162E+02 XXX
4.642E+02 XXXXXXXXXXXXXX
6.813E+02 XXX
1.000E+03
1.468E+03
2.154E+03
3.162E+03
4.642E+03 XXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

```
MINIMUM ANTILOG      =  2.00000E+02
MAXIMUM ANTILOG      =  5.00000E+03
GEOMETRIC MEAN       =  4.69911E+02
GEOMETRIC DEVIATION  =  2.59082E+00
VARIANCE OF LOGS     =  1.70930E-01
```

PERCENT TABLE FOR VARIABLE 9 (S-AS) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	2.712501E+00	5.158233E+02

95.00	2.841568E+00	6.944930E+02
98.00	1.000000E+35	1.000000E+35

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Nevada data

FREQUENCY TABLE FOR VARIABLE 11 (S-B)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		0	0	0.00	0.00		
	L		1	1	3.45	3.45		
	T		0	1	0.00	3.45	1.38	1.38
9.160E-01	-	1.083E+00	4	5	13.79	17.24	2.09	1.75
1.083E+00	-	1.249E+00	2	7	6.90	24.14	3.69	0.77
1.249E+00	-	1.416E+00	4	11	13.79	37.93	5.13	0.25
1.416E+00	-	1.583E+00	9	20	31.03	68.97	5.63	2.01
1.583E+00	-	1.749E+00	1	21	3.45	72.41	4.87	3.08
1.749E+00	-	1.916E+00	5	26	17.24	89.66	3.32	0.85
1.916E+00	-	2.083E+00	2	28	6.90	96.55	1.79	0.03
2.083E+00	-	2.249E+00	1	29	3.45	100.00	1.09	0.01
	G		0	29	0.00	100.00	0.00	0.00
	H		0	29				
	B		0	29				

TOTALS LESS H AND B 29

HISTOGRAM FOR VARIABLE 11 (S-B)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
9.985E+00 XXXXXXXXXXXXXX
1.466E+01 XXXXXXX
2.151E+01 XXXXXXXXXXXXXX
3.157E+01 XXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
4.634E+01 XXX
6.802E+01 XXXXXXXXXXXXXXXXX
9.985E+01 XXXXXXX
1.466E+02 XXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 1.00000E+01
MAXIMUM ANTILOG = 1.50000E+02
GEOMETRIC MEAN = 3.14955E+01
GEOMETRIC DEVIATION = 2.14477E+00
VARIANCE OF LOGS = 1.09814E-01

PERCENT TABLE FOR VARIABLE 11 (S-B) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.924335E+00	8.401085E+01
95.00	2.045169E+00	1.109606E+02
98.00	1.000000E+35	1.000000E+35

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Nevada data

FREQUENCY TABLE FOR VARIABLE 12 (S-BA)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		0	0	0.00	0.00		
	L		0	0	0.00	0.00		
	T		0	0	0.00	0.00	0.21	0.21
1.416E+00	-	1.583E+00	1	1	3.45	3.45	0.19	3.33
1.583E+00	-	1.749E+00	1	2	3.45	6.90	0.33	1.32
1.749E+00	-	1.916E+00	0	2	0.00	6.90	0.54	0.54
1.916E+00	-	2.083E+00	0	2	0.00	6.90	0.82	0.82
2.083E+00	-	2.249E+00	1	3	3.45	10.34	1.18	0.03
2.249E+00	-	2.416E+00	2	5	6.90	17.24	1.59	0.11
2.416E+00	-	2.583E+00	3	8	10.34	27.59	2.01	0.49
2.583E+00	-	2.749E+00	3	11	10.34	37.93	2.40	0.15
2.749E+00	-	2.916E+00	0	11	0.00	37.93	2.69	2.69
2.916E+00	-	3.083E+00	1	12	3.45	41.38	2.84	1.19
3.083E+00	-	3.249E+00	4	16	13.79	55.17	2.82	0.49
3.249E+00	-	3.416E+00	1	17	3.45	58.62	2.64	1.02
3.416E+00	-	3.583E+00	0	17	0.00	58.62	2.32	2.32
3.583E+00	-	3.749E+00	1	18	3.45	62.07	6.41	4.57
	G		11	29	37.93	100.00	0.21	556.66
	H		0	29				
	B		0	29				

TOTALS LESS H AND B 29

HISTOGRAM FOR VARIABLE 12 (S-BA)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
3.157E+01 XXX
4.634E+01 XXX
6.802E+01
9.985E+01
1.466E+02 XXX
2.151E+02 XXXXXXX
3.157E+02 XXXXXXXXXX
4.634E+02 XXXXXXXXXX
6.803E+02
9.985E+02 XXX
1.466E+03 XXXXXXXXXXXXXX
2.151E+03 XXX
3.157E+03
4.635E+03 XXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 3.00000E+01
MAXIMUM ANTILOG = 5.00000E+03
GEOMETRIC MEAN = 4.75389E+02
GEOMETRIC DEVIATION = 3.74292E+00
VARIANCE OF LOGS = 3.28571E-01

PERCENT TABLE FOR VARIABLE 12 (S-BA) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.000000E+35	1.000000E+35
95.00	1.000000E+35	1.000000E+35
98.00	1.000000E+35	1.000000E+35

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Nevada data

FREQUENCY TABLE FOR VARIABLE 13 (S-BE)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		0	0	0.00	0.00		
	L		2	2	6.90	6.90		
	T		0	2	0.00	6.90	1.74	1.74
-8.400E-02	-	8.267E-02	3	5	10.34	17.24	0.87	5.20
8.267E-02	-	2.493E-01	1	6	3.45	20.69	1.16	0.02
2.493E-01	-	4.160E-01	3	9	10.34	31.03	1.48	1.57
4.160E-01	-	5.827E-01	0	9	0.00	31.03	1.79	1.79
5.827E-01	-	7.493E-01	0	9	0.00	31.03	2.08	2.08
7.493E-01	-	9.160E-01	3	12	10.34	41.38	2.31	0.21
9.160E-01	-	1.083E+00	1	13	3.45	44.83	2.44	0.85
1.083E+00	-	1.249E+00	0	13	0.00	44.83	2.47	2.47
1.249E+00	-	1.416E+00	2	15	6.90	51.72	2.39	0.06
1.416E+00	-	1.583E+00	3	18	10.34	62.07	2.21	0.29
1.583E+00	-	1.749E+00	3	21	10.34	72.41	1.94	0.57
1.749E+00	-	1.916E+00	2	23	6.90	79.31	1.64	0.08
1.916E+00	-	2.083E+00	5	28	17.24	96.55	1.32	10.29
2.083E+00	-	2.249E+00	1	29	3.45	100.00	3.15	1.47
	G		0	29	0.00	100.00	0.00	0.00
	H		0	29				
	B		0	29				

TOTALS LESS H AND B 29

HISTOGRAM FOR VARIABLE 13 (S-BE)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
9.985E-01 XXXXXXXXXX
1.466E+00 XXX
2.151E+00 XXXXXXXXXX
3.157E+00
4.634E+00
6.802E+00 XXXXXXXXXX
9.985E+00 XXX
1.466E+01
2.151E+01 XXXXXXX
3.157E+01 XXXXXXXXXX
4.635E+01 XXXXXXXXXX
6.803E+01 XXXXXXX
9.985E+01 XXXXXXXXXXXXXXXXX
1.466E+02 XXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 1.00000E+00
MAXIMUM ANTILOG = 1.50000E+02
GEOMETRIC MEAN = 1.61368E+01
GEOMETRIC DEVIATION = 5.48036E+00
VARIANCE OF LOGS = 5.45839E-01

PERCENT TABLE FOR VARIABLE 13 (S-BE) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	2.019338E+00	1.045532E+02
95.00	2.067671E+00	1.168614E+02
98.00	1.000000E+35	1.000000E+35

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Nevada data

FREQUENCY TABLE FOR VARIABLE 15 (S-CD)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		23	23	79.31	79.31		
	L		0	23	0.00	79.31		
	T		0	23	0.00	79.31	9.26	9.26
1.250E+00	-	1.417E+00	3	26	10.34	89.66	8.50	3.56
1.417E+00	-	1.583E+00	2	28	6.90	96.55	6.92	3.50
1.583E+00	-	1.750E+00	0	28	0.00	96.55	3.27	3.27
1.750E+00	-	1.917E+00	0	28	0.00	96.55	0.90	0.90
1.917E+00	-	2.083E+00	0	28	0.00	96.55	0.14	0.14
2.083E+00	-	2.250E+00	0	28	0.00	96.55	0.01	0.01
2.250E+00	-	2.417E+00	0	28	0.00	96.55	0.00	0.00
2.417E+00	-	2.583E+00	1	29	3.45	100.00	0.00	1401.34
	G		0	29	0.00	100.00	0.00	0.00
	H		0	29				
	B		0	29				

TOTALS LESS H AND B 29

HISTOGRAM FOR VARIABLE 15 (S-CD)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
2.154E+01 XXXXXXXXXX
3.162E+01 XXXXXXX
4.642E+01
6.313E+01
1.000E+02
1.468E+02
2.154E+02
3.162E+02 XXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 2.00000E+01
MAXIMUM ANTILOG = 3.00000E+02
GEOMETRIC MEAN = 3.59536E+01
GEOMETRIC DEVIATION = 2.83105E+00
VARIANCE OF LOGS = 2.11187E-01

PERCENT TABLE FOR VARIABLE 15 (S-CD) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.423000E+00	2.660727E+01
95.00	1.545834E+00	3.514260E+01
98.00	1.000000E+35	1.000000E+35

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Nevada data

FREQUENCY TABLE FOR VARIABLE 16 (S-CO)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		18	18	62.07	62.07		
	L		4	22	13.79	75.86		
	T		0	22	0.00	75.86	5.31	5.31
5.830E-01	-	7.497E-01	1	23	3.45	79.31	7.60	5.73
7.497E-01	-	9.163E-01	3	26	10.34	89.66	8.40	3.47
9.163E-01	-	1.083E+00	1	27	3.45	93.10	5.32	3.51
1.083E+00	-	1.250E+00	0	27	0.00	93.10	1.93	1.93
1.250E+00	-	1.416E+00	1	28	3.45	96.55	0.40	0.91
1.416E+00	-	1.583E+00	0	28	0.00	96.55	0.05	0.05
1.583E+00	-	1.750E+00	1	29	3.45	100.00	0.00	303.52
	G		0	29	0.00	100.00	0.00	0.00
	H		0	29				
	B		0	29				

TOTALS LESS H AND B 29

HISTOGRAM FOR VARIABLE 16 (S-CO)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
4.638E+00 XXX
6.308E+00 XXXXXXXXXX
9.992E+00 XXX
1.467E+01
2.153E+01 XXX
3.160E+01
4.633E+01 XXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

```
MINIMUM ANTILOG      =  5.00000E+00
MAXIMUM ANTILOG      =  5.00000E+01
GEOMETRIC MEAN       =  1.08011E+01
GEOMETRIC DEVIATION  =  2.23742E+00
VARIANCE OF LOGS     =  1.22324E-01
```

PERCENT TABLE FOR VARIABLE 16 (S-CO) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	9.330007E-01	8.570392E+00
95.00	1.266335E+00	1.846438E+01
98.00	1.000000E+35	1.000000E+35

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Nevada data

FREQUENCY TABLE FOR VARIABLE 17 (S-CR)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		18	18	62.07	62.07		
	L		4	22	13.79	75.86		
	T		0	22	0.00	75.86	7.09	7.09
9.160E-01	-	1.083E+00	4	26	13.79	89.66	8.86	2.66
1.083E+00	-	1.249E+00	1	27	3.45	93.10	8.04	6.16
1.249E+00	-	1.416E+00	0	27	0.00	93.10	3.88	3.88
1.416E+00	-	1.583E+00	1	28	3.45	96.55	0.99	0.00
1.583E+00	-	1.749E+00	0	28	0.00	96.55	0.13	0.13
1.749E+00	-	1.916E+00	0	28	0.00	96.55	0.01	0.01
1.916E+00	-	2.083E+00	1	29	3.45	100.00	0.00	2723.68
	G		0	29	0.00	100.00	0.00	0.00
	H		0	29				
	B		0	29				

TOTALS LESS H AND B 29

HISTOGRAM FOR VARIABLE 17 (S-CR)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
9.985E+00 XXXXXXXXXXXXXX
1.466E+01 XXX
2.151E+01
3.157E+01 XXX
4.634E+01
6.802E+01
9.985E+01 XXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 1.00000E+01
MAXIMUM ANTILOG = 1.00000E+02
GEOMETRIC MEAN = 1.72256E+01
GEOMETRIC DEVIATION = 2.40102E+00
VARIANCE OF LOGS = 1.44701E-01

PERCENT TABLE FOR VARIABLE 17 (S-CR) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.099334E+00	1.256995E+01
95.00	1.432568E+00	2.703119E+01
98.00	1.000000E+35	1.000000E+35

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Nevada data

FREQUENCY TABLE FOR VARIABLE 18 (S-CU)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		0	0	0.00	0.00		
	L		4	4	13.79	13.79		
	T		0	4	0.00	13.79	2.75	2.75
5.830E-01	-	7.497E-01	1	5	3.45	17.24	1.04	0.00
7.497E-01	-	9.163E-01	3	8	10.34	27.59	1.28	2.29
9.163E-01	-	1.083E+00	2	10	6.90	34.48	1.53	0.14
1.083E+00	-	1.250E+00	1	11	3.45	37.93	1.76	0.33
1.250E+00	-	1.416E+00	1	12	3.45	41.38	1.95	0.47
1.416E+00	-	1.583E+00	3	15	10.34	51.72	2.09	0.39
1.583E+00	-	1.750E+00	1	16	3.45	55.17	2.17	0.63
1.750E+00	-	1.916E+00	1	17	3.45	58.62	2.16	0.63
1.916E+00	-	2.083E+00	0	17	0.00	58.62	2.09	2.09
2.083E+00	-	2.250E+00	3	20	10.34	68.97	1.94	0.58
2.250E+00	-	2.416E+00	0	20	0.00	68.97	1.74	1.74
2.416E+00	-	2.583E+00	2	22	6.90	75.86	1.51	0.16
2.583E+00	-	2.750E+00	3	25	10.34	86.21	1.27	2.38
2.750E+00	-	2.916E+00	1	26	3.45	89.66	1.02	0.00
2.916E+00	-	3.083E+00	1	27	3.45	93.10	0.80	0.05
3.083E+00	-	3.250E+00	1	28	3.45	96.55	0.60	0.27
3.250E+00	-	3.416E+00	0	28	0.00	96.55	0.44	0.44
3.416E+00	-	3.583E+00	1	29	3.45	100.00	0.85	0.03
	G		0	29	0.00	100.00	0.00	0.00
	H		0	29				
	B		0	29				

TOTALS LESS H AND B 29

HISTOGRAM FOR VARIABLE 18 (S-CU)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
4.638E+00 XXX
6.808E+00 XXXXXXXXXX
9.992E+00 XXXXXXX
1.467E+01 XXX
2.153E+01 XXX
3.160E+01 XXXXXXXXXX
4.638E+01 XXX
6.808E+01 XXX
9.992E+01
1.467E+02 XXXXXXXXXX
2.153E+02
3.160E+02 XXXXXXX
4.638E+02 XXXXXXXXXX
6.808E+02 XXX
9.992E+02 XXX
1.467E+03 XXX
2.153E+03
3.160E+03 XXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 5.00000E+00
MAXIMUM ANTILOG = 3.00000E+03
GEOMETRIC MEAN = 8.13921E+01
GEOMETRIC DEVIATION = 6.90064E+00
VARIANCE OF LOGS = 7.03735E-01

PERCENT TABLE FOR VARIABLE 18 (S-CU) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	2.933005E+00	8.570471E+02
95.00	3.174672E+00	1.495105E+03
98.00	1.000000E+35	1.000000E+35

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FREQUENCY TABLE FOR VARIABLE 19 (S-LA)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		4	4	13.79	13.79		
	L		13	17	44.83	58.62		
	T		0	17	0.00	58.62	5.89	5.89
1.250E+00	-	1.417E+00	8	25	27.59	86.21	16.07	4.05
1.417E+00	-	1.583E+00	2	27	6.90	93.10	6.67	3.27
1.583E+00	-	1.750E+00	2	29	6.90	100.00	0.38	6.95
	G		0	29	0.00	100.00	0.00	0.00
	H		0	29				
	B		0	29				

TOTALS LESS H AND B 29

HISTOGRAM FOR VARIABLE 19 (S-LA)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
2.154E+01 XXXXXXXXXXXXXXXXXXXXXXXXXXX
3.162E+01 XXXXXXX
4.642E+01 XXXXXXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 2.00000E+01
MAXIMUM ANTILOG = 5.00000E+01
GEOMETRIC MEAN = 2.49238E+01
GEOMETRIC DEVIATION = 1.43334E+00
VARIANCE OF LOGS = 2.44447E-02

PERCENT TABLE FOR VARIABLE 19 (S-LA) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.508334E+00	3.223546E+01
95.00	1.000000E+35	1.000000E+35
98.00	1.000000E+35	1.000000E+35

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Nevada data

FREQUENCY TABLE FOR VARIABLE 20 (S-MO)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		17	17	58.62	58.62		
	L		0	17	0.00	58.62		
	T		0	17	0.00	58.62	6.64	6.64
5.830E-01	-	7.497E-01	3	20	10.34	68.97	3.62	0.11
7.497E-01	-	9.163E-01	1	21	3.45	72.41	4.15	2.39
9.163E-01	-	1.083E+00	2	23	6.90	79.31	4.16	1.12
1.083E+00	-	1.250E+00	2	25	6.90	86.21	3.65	0.75
1.250E+00	-	1.416E+00	0	25	0.00	86.21	2.80	2.80
1.416E+00	-	1.583E+00	2	27	6.90	93.10	1.89	0.01
1.583E+00	-	1.750E+00	0	27	0.00	93.10	1.11	1.11
1.750E+00	-	1.916E+00	1	28	3.45	96.55	0.57	0.32
1.916E+00	-	2.083E+00	0	28	0.00	96.55	0.26	0.26
2.083E+00	-	2.250E+00	0	28	0.00	96.55	0.10	0.10
2.250E+00	-	2.416E+00	0	28	0.00	96.55	0.03	0.03
2.416E+00	-	2.583E+00	0	28	0.00	96.55	0.01	0.01
2.583E+00	-	2.750E+00	1	29	3.45	100.00	0.00	276.14
	G		0	29	0.00	100.00	0.00	0.00
	H		0	29				
	B		0	29				

TOTALS LESS H AND B 29

HISTOGRAM FOR VARIABLE 20 (S-MO)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
4.638E+00 XXXXXXXXXX
6.808E+00 XXX
9.992E+00 XXXXXXX
1.467E+01 XXXXXXX
2.153E+01
3.160E+01 XXXXXXX
4.638E+01
6.808E+01 XXX
9.992E+01
1.467E+02
2.153E+02
3.160E+02
4.638E+02 XXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

```
MINIMUM ANTILOG      =  5.00000E+00
MAXIMUM ANTILOG      =  5.00000E+02
GEOMETRIC MEAN       =  1.70887E+01
GEOMETRIC DEVIATION  =  3.84560E+00
VARIANCE OF LOGS     =  3.42183E-01
```

PERCENT TABLE FOR VARIABLE 20 (S-MO) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.433002E+00	2.710202E+01
95.00	1.766336E+00	5.838963E+01
98.00	1.000000E+35	1.000000E+35

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Nevada data

FREQUENCY TABLE FOR VARIABLE 22 (S-NI)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		14	14	48.28	48.28		
	L		3	17	10.34	58.62		
	T		0	17	0.00	58.62	7.06	7.06
5.830E-01	-	7.497E-01	3	20	10.34	68.97	4.11	0.30
7.497E-01	-	9.163E-01	2	22	6.90	75.86	4.62	1.48
9.163E-01	-	1.083E+00	4	26	13.79	89.66	4.42	0.04
1.083E+00	-	1.250E+00	1	27	3.45	93.10	3.60	1.88
1.250E+00	-	1.416E+00	0	27	0.00	93.10	2.50	2.50
1.416E+00	-	1.583E+00	0	27	0.00	93.10	1.48	1.48
1.583E+00	-	1.750E+00	1	28	3.45	96.55	0.74	0.09
1.750E+00	-	1.916E+00	0	28	0.00	96.55	0.32	0.32
1.916E+00	-	2.083E+00	0	28	0.00	96.55	0.12	0.12
2.083E+00	-	2.250E+00	0	28	0.00	96.55	0.04	0.04
2.250E+00	-	2.416E+00	0	28	0.00	96.55	0.01	0.01
2.416E+00	-	2.583E+00	0	28	0.00	96.55	0.00	0.00
2.583E+00	-	2.750E+00	1	29	3.45	100.00	0.00	2025.24
	G		0	29	0.00	100.00	0.00	0.00
	H		0	29				
	B		0	29				

TOTALS LESS H AND B 29

HISTOGRAM FOR VARIABLE 22 (S-NI)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
4.633E+00 XXXXXXXXXX
6.803E+00 XXXXXXX
9.992E+00 XXXXXXXXXXXXXX
1.467E+01 XXX
2.153E+01
3.160E+01
4.633E+01 XXX
6.803E+01
9.992E+01
1.467E+02
2.153E+02
3.160E+02
4.638E+02 XXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

```
MINIMUM ANTILOG      =  5.00000E+00
MAXIMUM ANTILOG      =  5.00000E+02
GEOMETRIC MEAN       =  1.29846E+01
GEOMETRIC DEVIATION  =  3.71373E+00
VARIANCE OF LOGS     =  3.24684E-01
```

PERCENT TABLE FOR VARIABLE 22 (S-NI) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.099668E+00	1.257963E+01
95.00	1.524669E+00	3.347099E+01
98.00	1.000000E+35	1.000000E+35

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Nevada data

FREQUENCY TABLE FOR VARIABLE 23 (S-PB)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		0	0	0.00	0.00		
	L		0	0	0.00	0.00		
	T		0	0	0.00	0.00	2.43	2.43
1.083E+00	-	1.250E+00	3	3	10.34	10.34	0.92	4.68
1.250E+00	-	1.416E+00	3	6	10.34	20.69	1.15	2.99
1.416E+00	-	1.583E+00	2	8	6.90	27.59	1.38	0.28
1.583E+00	-	1.750E+00	1	9	3.45	31.03	1.61	0.23
1.750E+00	-	1.916E+00	2	11	6.90	37.93	1.81	0.02
1.916E+00	-	2.083E+00	3	14	10.34	48.28	1.97	0.54
2.083E+00	-	2.250E+00	0	14	0.00	48.28	2.07	2.07
2.250E+00	-	2.416E+00	1	15	3.45	51.72	2.11	0.58
2.416E+00	-	2.583E+00	3	18	10.34	62.07	2.08	0.41
2.583E+00	-	2.750E+00	2	20	6.90	68.97	1.98	0.00
2.750E+00	-	2.916E+00	2	22	6.90	75.86	1.83	0.02
2.916E+00	-	3.083E+00	1	23	3.45	79.31	1.63	0.24
3.083E+00	-	3.250E+00	0	23	0.00	79.31	1.40	1.40
3.250E+00	-	3.416E+00	1	24	3.45	82.76	1.17	0.03
3.416E+00	-	3.583E+00	1	25	3.45	86.21	0.95	0.00
3.583E+00	-	3.750E+00	2	27	6.90	93.10	0.74	2.16
3.750E+00	-	3.916E+00	1	28	3.45	96.55	1.78	0.34
	G		1	29	3.45	100.00	2.43	0.84
	H		0	29				
	B		0	29				

TOTALS LESS H AND B 29

HISTOGRAM FOR VARIABLE 23 (S-PB)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
1.467E+01 XXXXXXXXXX
2.153E+01 XXXXXXXXXX
3.160E+01 XXXXXXX
4.638E+01 XXX
6.808E+01 XXXXXXX
9.992E+01 XXXXXXXXXX
1.467E+02
2.153E+02 XXX
3.160E+02 XXXXXXXXXX
4.638E+02 XXXXXXX
6.808E+02 XXXXXXX
9.992E+02 XXX
1.467E+03
2.153E+03 XXX
3.160E+03 XXX
4.638E+03 XXXXXXX
6.808E+03 XXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

```
MINIMUM ANTILOG      =  1.50000E+01
MAXIMUM ANTILOG      =  7.00000E+03
GEOMETRIC MEAN       =  1.87076E+02
GEOMETRIC DEVIATION  =  7.02248E+00
VARIANCE OF LOGS     =  7.16546E-01
```

PERCENT TABLE FOR VARIABLE 23 (S-PB) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	3.674672E+00	4.727939E+03
95.00	3.841339E+00	6.939670E+03
98.00	1.000000E+35	1.000000E+35

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Nevada data

FREQUENCY TABLE FOR VARIABLE 24 (S-SB)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		8	8	27.59	27.59		
	L		5	13	17.24	44.83		
	T		0	13	0.00	44.83	4.37	4.37
1.916E+00	-	2.083E+00	8	21	27.59	72.41	9.47	0.23
2.083E+00	-	2.249E+00	1	22	3.45	75.86	9.97	8.07
2.249E+00	-	2.416E+00	6	28	20.69	96.55	4.35	0.63
2.416E+00	-	2.583E+00	0	28	0.00	96.55	0.78	0.78
2.583E+00	-	2.749E+00	1	29	3.45	100.00	0.06	15.00
	G		0	29	0.00	100.00	0.00	0.00
	H		0	29				
	B		0	29				

TOTALS LESS G AND B 29

HISTOGRAM FOR VARIABLE 24 (S-SB)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
9.985E+01 XXXXXXXXXXXXXXXXXXXXXXXXXXXX
1.466E+02 XXX
2.151E+02 XXXXXXXXXXXXXXXXXXXXX
3.157E+02
4.634E+02 XXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 1.00000E+02
MAXIMUM ANTILOG = 5.00000E+02
GEOMETRIC MEAN = 1.47088E+02
GEOMETRIC DEVIATION = 1.59336E+00
VARIANCE OF LOGS = 4.09312E-02

PERCENT TABLE FOR VARIABLE 24 (S-SB) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.999999E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	2.363223E+00	2.307933E+02
95.00	2.403501E+00	2.532217E+02
98.00	1.000000E+35	1.000000E+35

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Nevada data

FREQUENCY TABLE FOR VARIABLE 25 (S-SC)

LOG LIMITS LOWER - UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
N	23	23	79.31	79.31		
L	4	27	13.79	93.10		
T	0	27	0.00	93.10	0.00	0.00
5.830E-01 - 7.497E-01	1	28	3.45	96.55	27.66	25.70
7.497E-01 - 9.163E-01	1	29	3.45	100.00	1.34	0.09
G	0	29	0.00	100.00	0.00	0.00
H	0	29				
B	0	29				

TOTALS LESS H AND B 29

HISTOGRAM FOR VARIABLE 25 (S-SC)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
4.638E+00 XXX
6.808E+00 XXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

```
MINIMUM ANTILOG      =  5.00000E+00
MAXIMUM ANTILOG      =  7.00000E+00
GEOMETRIC MEAN       =  5.91608E+00
GEOMETRIC DEVIATION  =  1.26861E+00
VARIANCE OF LOGS     =  1.06767E-02
```

PERCENT TABLE FOR VARIABLE 25 (S-SC) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999901E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.000000E+35	1.000000E+35
95.00	1.000000E+35	1.000000E+35
98.00	1.000000E+35	1.000000E+35

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Nevada data

FREQUENCY TABLE FOR VARIABLE 27 (S-SR)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		3	3	10.34	10.34		
	L		6	9	20.69	31.03		
	T		0	9	0.00	31.03	4.95	4.95
1.916E+00	-	2.083E+00	4	13	13.79	44.83	1.87	2.42
2.083E+00	-	2.249E+00	0	13	0.00	44.83	2.21	2.21
2.249E+00	-	2.416E+00	4	17	13.79	58.62	2.47	0.95
2.416E+00	-	2.583E+00	0	17	0.00	58.62	2.62	2.62
2.583E+00	-	2.749E+00	4	21	13.79	72.41	2.64	0.70
2.749E+00	-	2.916E+00	0	21	0.00	72.41	2.53	2.53
2.916E+00	-	3.083E+00	0	21	0.00	72.41	2.29	2.29
3.083E+00	-	3.249E+00	0	21	0.00	72.41	1.97	1.97
3.249E+00	-	3.416E+00	0	21	0.00	72.41	1.61	1.61
3.416E+00	-	3.583E+00	0	21	0.00	72.41	1.25	1.25
3.583E+00	-	3.749E+00	4	25	13.79	86.21	2.59	0.77
	G		4	29	13.79	100.00	0.00	0.00
	H		0	29				
	B		0	29				

TOTALS LESS H AND B 29

HISTOGRAM FOR VARIABLE 27 (S-SR)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
9.985E+01 XXXXXXXXXXXXXX
1.466E+02
2.151E+02 XXXXXXXXXXXXXX
3.157E+02
4.634E+02 XXXXXXXXXXXXXX
6.802E+02
9.985E+02
1.466E+03
2.151E+03
3.157E+03
4.635E+03 XXXXXXXXXXXXXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 1.00000E+02
MAXIMUM ANTILOG = 5.00000E+03
GEOMETRIC MEAN = 4.72871E+02
GEOMETRIC DEVIATION = 4.59443E+00
VARIANCE OF LOGS = 4.38551E-01

PERCENT TABLE FOR VARIABLE 27 (S-SR) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.000000E+35	1.000000E+35
95.00	1.000000E+35	1.000000E+35
98.00	1.000000E+35	1.000000E+35

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Nevada data

FREQUENCY TABLE FOR VARIABLE 28 (S-V)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		0	0	0.00	0.00		
	L		7	7	24.14	24.14		
	T		0	7	0.00	24.14	6.42	6.42
9.160E-01	-	1.083E+00	6	13	20.69	44.83	3.32	2.17
1.083E+00	-	1.249E+00	6	19	20.69	65.52	3.83	1.22
1.249E+00	-	1.416E+00	3	22	10.34	75.86	3.94	0.22
1.416E+00	-	1.583E+00	4	26	13.79	89.66	3.60	0.04
1.583E+00	-	1.749E+00	0	26	0.00	89.66	2.93	2.93
1.749E+00	-	1.916E+00	1	27	3.45	93.10	2.12	0.59
1.916E+00	-	2.083E+00	0	27	0.00	93.10	1.37	1.37
2.083E+00	-	2.249E+00	0	27	0.00	93.10	0.78	0.78
2.249E+00	-	2.416E+00	0	27	0.00	93.10	0.40	0.40
2.416E+00	-	2.583E+00	1	28	3.45	96.55	0.18	3.71
2.583E+00	-	2.749E+00	0	28	0.00	96.55	0.07	0.07
2.749E+00	-	2.916E+00	0	28	0.00	96.55	0.03	0.03
2.916E+00	-	3.083E+00	0	28	0.00	96.55	0.01	0.01
3.083E+00	-	3.249E+00	1	29	3.45	100.00	0.00	316.97
	G		0	29	0.00	100.00	0.00	0.00
	H		0	29				
	B		0	29				

TOTALS LESS H AND B 29

HISTOGRAM FOR VARIABLE 28 (S-V)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
9.985E+00 XXXXXXXXXXXXXXXXXXXXX
1.466E+01 XXXXXXXXXXXXXXXXXXXXX
2.151E+01 XXXXXXXXXX
3.157E+01 XXXXXXXXXXXXXX
4.634E+01
6.802E+01 XXX
9.985E+01
1.466E+02
2.151E+02
3.157E+02 XXX
4.635E+02
6.803E+02
9.985E+02
1.466E+03 XXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 1.00000E+01
MAXIMUM ANTILOG = 1.50000E+03
GEOMETRIC MEAN = 2.40045E+01
GEOMETRIC DEVIATION = 3.36019E+00
VARIANCE OF LOGS = 2.77059E-01

PERCENT TABLE FOR VARIABLE 28 (S-V) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.616001E+00	4.130488E+01
95.00	2.282669E+00	1.917209E+02
98.00	1.000000E+35	1.000000E+35

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Nevada data

FREQUENCY TABLE FOR VARIABLE 30 (S-Y)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		15	15	51.72	51.72		
	L		5	20	17.24	68.97		
	T		0	20	0.00	68.97	5.03	5.03
9.160E-01	-	1.083E+00	4	24	13.79	82.76	11.84	5.19
1.083E+00	-	1.249E+00	3	27	10.34	93.10	9.58	4.52
1.249E+00	-	1.416E+00	1	28	3.45	96.55	2.37	0.80
1.416E+00	-	1.583E+00	0	28	0.00	96.55	0.18	0.18
1.583E+00	-	1.749E+00	1	29	3.45	100.00	0.00	256.65
	G		0	29	0.00	100.00	0.00	0.00
	H		0	29				
	B		0	29				

TOTALS LESS H AND B 29

HISTOGRAM FOR VARIABLE 30 (S-Y)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
9.985E+00 XXXXXXXXXXXXXX
1.466E+01 XXXXXXXXXX
2.151E+01 XXX
3.157E+01
4.634E+01 XXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 1.00000E+01
MAXIMUM ANTILOG = 5.00000E+01
GEOMETRIC MEAN = 1.47846E+01
GEOMETRIC DEVIATION = 1.68704E+00
VARIANCE OF LOGS = 5.15861E-02

PERCENT TABLE FOR VARIABLE 30 (S-Y) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.199334E+00	1.582464E+01
95.00	1.341001E+00	2.192809E+01
98.00	1.000000E+35	1.000000E+35

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Nevada data

FREQUENCY TABLE FOR VARIABLE 31 (S-ZN)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		10	10	34.48	34.48		
	L		0	10	0.00	34.48		
	T		0	10	0.00	34.48	4.68	4.68
2.250E+00	-	2.417E+00	2	12	6.90	41.38	3.56	0.68
2.417E+00	-	2.583E+00	4	16	13.79	55.17	4.50	0.06
2.583E+00	-	2.750E+00	4	20	13.79	68.97	4.79	0.13
2.750E+00	-	2.917E+00	1	21	3.45	72.41	4.30	2.53
2.917E+00	-	3.083E+00	4	25	13.79	86.21	3.24	0.18
3.083E+00	-	3.250E+00	2	27	6.90	93.10	2.06	0.00
3.250E+00	-	3.417E+00	0	27	0.00	93.10	1.10	1.10
3.417E+00	-	3.583E+00	1	28	3.45	96.55	0.50	0.51
3.583E+00	-	3.750E+00	1	29	3.45	100.00	0.27	1.98
	G		0	29	0.00	100.00	0.00	0.00
	H		0	29				
	B		0	29				

TOTALS LESS H AND B 29

HISTOGRAM FOR VARIABLE 31 (S-ZN)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
2.154E+02 XXXXXXX
3.162E+02 XXXXXXXXXXXXXX
4.642E+02 XXXXXXXXXXXXXX
6.813E+02 XXX
1.000E+03 XXXXXXXXXXXXXX
1.468E+03 XXXXXXX
2.154E+03
3.162E+03 XXX
4.642E+03 XXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

```
MINIMUM ANTILOG      =  2.00000E+02
MAXIMUM ANTILOG      =  5.00000E+03
GEOMETRIC MEAN       =  6.68733E+02
GEOMETRIC DEVIATION  =  2.42144E+00
VARIANCE OF LOGS     =  1.47512E-01
```

PERCENT TABLE FOR VARIABLE 31 (S-ZN) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	3.175002E+00	1.496242E+03

95.00	3.433336E+00	2.712287E+03
98.00	1.000000E+35	1.000000E+35

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FREQUENCY TABLE FOR VARIABLE 32 (S-ZR)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		14	14	48.28	48.28		
	L		5	19	17.24	65.52		
	T		0	19	0.00	65.52	6.17	6.17
9.160E-01	-	1.083E+00	2	21	6.90	72.41	4.49	1.38
1.083E+00	-	1.249E+00	1	22	3.45	75.86	5.23	3.42
1.249E+00	-	1.416E+00	0	22	0.00	75.86	4.95	4.95
1.416E+00	-	1.583E+00	0	22	0.00	75.86	3.82	3.82
1.583E+00	-	1.749E+00	3	25	10.34	86.21	2.39	0.16
1.749E+00	-	1.916E+00	2	27	6.90	93.10	1.22	0.50
1.916E+00	-	2.083E+00	2	29	6.90	100.00	0.73	2.18
	G		0	29	0.00	100.00	0.00	0.00
	H		0	29				
	B		0	29				

TOTALS LESS H AND B 29

HISTOGRAM FOR VARIABLE 32 (S-ZR)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
9.985E+00 XXXXXXX
1.466E+01 XXX
2.151E+01
3.157E+01
4.634E+01 XXXXXXXXXX
6.802E+01 XXXXXXX
9.985E+01 XXXXXXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 1.00000E+01
MAXIMUM ANTILOG = 1.00000E+02
GEOMETRIC MEAN = 3.94748E+01
GEOMETRIC DEVIATION = 2.45437E+00
VARIANCE OF LOGS = 1.52122E-01

PERCENT TABLE FOR VARIABLE 32 (S-ZR) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	1.841002E+00	6.934288E+01
95.00	1.000000E+35	1.000000E+35
98.00	1.000000E+35	1.000000E+35

D0036 GRAPHICAL ANALYSIS - U S G S STATPAC (02/07/82) DATE 7/20/84

Nevada data

FREQUENCY TABLE FOR VARIABLE 34 (AA-AU-P)

LOG LIMITS LOWER - UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
N	22	22	75.86	75.86		
L	1	23	3.45	79.31		
T	0	23	0.00	79.31	14.48	14.48
-1.084E+00 - -9.173E-01	1	24	3.45	82.76	3.67	1.94
-9.173E-01 - -7.507E-01	0	24	0.00	82.76	3.31	3.31
-7.507E-01 - -5.840E-01	1	25	3.45	86.21	2.70	1.07
-5.840E-01 - -4.173E-01	1	26	3.45	89.66	1.98	0.48
-4.173E-01 - -2.507E-01	1	27	3.45	93.10	1.31	0.07
-2.507E-01 - -8.400E-02	0	27	0.00	93.10	0.78	0.78
-8.400E-02 - 3.267E-02	0	27	0.00	93.10	0.42	0.42
8.267E-02 - 2.493E-01	0	27	0.00	93.10	0.20	0.20
2.493E-01 - 4.160E-01	0	27	0.00	93.10	0.09	0.09
4.160E-01 - 5.827E-01	1	28	3.45	96.55	0.04	26.37
5.827E-01 - 7.493E-01	1	29	3.45	100.00	0.02	53.07
G	0	29	0.00	100.00	0.00	0.00
H	0	29				
B	0	29				

TOTALS LESS H AND B 29

HISTOGRAM FOR VARIABLE 34 (AA-AU-P)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
9.035E-02 XXX
1.466E-01
2.151E-01 XXX
3.157E-01 XXX
4.634E-01 XXX
6.802E-01
9.985E-01
1.466E+00
2.151E+00
3.157E+00 XXX
4.635E+00 XXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 1.00000E-01
MAXIMUM ANTILOG = 4.20000E+00
GEOMETRIC MEAN = 5.64203E-01
GEOMETRIC DEVIATION = 4.59519E+00
VARIANCE OF LOGS = 4.38645E-01

PERCENT TABLE FOR VARIABLE 34 (AA-AU-P) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	-4.006653E-01	3.974978E-01
95.00	2.076692E-01	1.613130E+00
98.00	1.000000E+35	1.000000E+35

D0036 GRAPHICAL ANALYSIS - U S G S STATPAC (02/07/82) DATE 7/20/84

Nevada data

FREQUENCY TABLE FOR VARIABLE 35 (INST-HG)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
		N	0	0	0.00	0.00		
		L	1	1	3.45	3.45		
		T	0	1	0.00	3.45	0.24	0.24
-1.750E+00	-	-1.583E+00	1	2	3.45	6.90	0.26	2.08
-1.583E+00	-	-1.417E+00	0	2	0.00	6.90	0.48	0.48
-1.417E+00	-	-1.250E+00	1	3	3.45	10.34	0.81	0.04
-1.250E+00	-	-1.083E+00	1	4	3.45	13.79	1.26	0.05
-1.083E+00	-	-9.167E-01	0	4	0.00	13.79	1.80	1.80
-9.167E-01	-	-7.500E-01	0	4	0.00	13.79	2.37	2.37
-7.500E-01	-	-5.833E-01	1	5	3.45	17.24	2.88	1.22
-5.833E-01	-	-4.167E-01	6	11	20.69	37.93	3.22	2.41
-4.167E-01	-	-2.500E-01	7	18	24.14	62.07	3.31	4.10
-2.500E-01	-	-8.333E-02	3	21	10.34	72.41	3.14	0.01
-8.333E-02	-	8.334E-02	3	24	10.34	82.76	2.75	0.02
8.334E-02	-	2.500E-01	1	25	3.45	86.21	2.21	0.66
2.500E-01	-	4.167E-01	2	27	6.90	93.10	1.64	0.08
4.167E-01	-	5.833E-01	1	28	3.45	96.55	1.12	0.01
5.833E-01	-	7.500E-01	1	29	3.45	100.00	1.52	0.18
		G	0	29	0.00	100.00	0.00	0.00
		H	0	29				
		B	0	29				

TOTALS LESS H AND B 29

HISTOGRAM FOR VARIABLE 35 (INST-HG)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
2.154E-02 XXX
3.162E-02
4.642E-02 XXX
6.813E-02 XXX
1.000E-01
1.468E-01
2.154E-01 XXX
3.162E-01 XXXXXXXXXXXXXXXXXXXXX
4.642E-01 XXXXXXXXXXXXXXXXXXXXXXXXX
6.813E-01 XXXXXXXXXX
1.000E+00 XXXXXXXXXX
1.468E+00 XXX
2.154E+00 XXXXXXX
3.162E+00 XXX
4.642E+00 XXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 2.00000E-02
MAXIMUM ANTILOG = 5.60000E+00
GEOMETRIC MEAN = 4.91131E-01

GEOMETRIC DEVIATION = 3.37564E+00
VARIANCE OF LOGS = 2.79160E-01

PERCENT TABLE FOR VARIABLE 35 (INST-HG) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	3.416708E-01	2.196195E+00
95.00	5.083378E-01	3.223575E+00
98.00	1.000000E+35	1.000000E+35

D0036 GRAPHICAL ANALYSIS - U S G S STATPAC (02/07/82) DATE 7/20/84

Nevada data

FREQUENCY TABLE FOR VARIABLE 36 (AA-AS-P)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		1	1	3.45	3.45		
	L		0	1	0.00	3.45		
	T		0	1	0.00	3.45	1.20	1.20
5.830E-01	-	7.497E-01	2	3	6.90	10.34	0.76	2.03
7.497E-01	-	9.163E-01	0	3	0.00	10.34	1.09	1.09
9.163E-01	-	1.083E+00	3	6	10.34	20.69	1.47	1.60
1.083E+00	-	1.250E+00	2	8	6.90	27.59	1.87	0.01
1.250E+00	-	1.416E+00	2	10	6.90	34.48	2.25	0.03
1.416E+00	-	1.583E+00	1	11	3.45	37.93	2.56	0.95
1.583E+00	-	1.750E+00	4	15	13.79	51.72	2.74	0.58
1.750E+00	-	1.916E+00	1	16	3.45	55.17	2.78	1.14
1.916E+00	-	2.083E+00	2	18	6.90	62.07	2.65	0.16
2.083E+00	-	2.250E+00	2	20	6.90	68.97	2.39	0.06
2.250E+00	-	2.416E+00	3	23	10.34	79.31	2.03	0.46
2.416E+00	-	2.583E+00	2	25	6.90	86.21	1.63	0.08
2.583E+00	-	2.750E+00	3	28	10.34	96.55	3.59	0.10
	G		1	29	3.45	100.00	0.00	0.00
	H		0	29				
	B		0	29				

TOTALS LESS H AND B 29

HISTOGRAM FOR VARIABLE 36 (AA-AS-P)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
4.638E+00 XXXXXXX
6.808E+00
9.992E+00 XXXXXXXXXX
1.467E+01 XXXXXXX
2.153E+01 XXXXXXX
3.160E+01 XXX
4.638E+01 XXXXXXXXXXXXXX
6.808E+01 XXX
9.992E+01 XXXXXXX
1.467E+02 XXXXXXX
2.153E+02 XXXXXXXXXX
3.160E+02 XXXXXXX
4.638E+02 XXXXXXXXXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 5.00000E+00
MAXIMUM ANTILOG = 4.50000E+02
GEOMETRIC MEAN = 5.85773E+01
GEOMETRIC DEVIATION = 4.13979E+00
VARIANCE OF LOGS = 3.80662E-01

PERCENT TABLE FOR VARIABLE 36 (AA-AS-P) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	2.644115E+00	4.406717E+02
95.00	2.724671E+00	5.304823E+02
98.00	1.000000E+35	1.000000E+35

D0036 GRAPHICAL ANALYSIS - U S G S STATPAC (02/07/82) DATE 7/20/84

Nevada data

FREQUENCY TABLE FOR VARIABLE 37 (AA-ZN-P)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		0	0	0.00	0.00		
	L		0	0	0.00	0.00		
	T		0	0	0.00	0.00	0.35	0.35
9.160E-01	-	1.083E+00	1	1	3.45	3.45	0.31	1.51
1.083E+00	-	1.249E+00	1	2	3.45	6.90	0.52	0.44
1.249E+00	-	1.416E+00	1	3	3.45	10.34	0.81	0.04
1.416E+00	-	1.583E+00	0	3	0.00	10.34	1.19	1.19
1.583E+00	-	1.749E+00	3	6	10.34	20.69	1.63	1.16
1.749E+00	-	1.916E+00	2	8	6.90	27.59	2.08	0.00
1.916E+00	-	2.083E+00	2	10	6.90	34.48	2.50	0.10
2.083E+00	-	2.249E+00	0	10	0.00	34.48	2.81	2.81
2.249E+00	-	2.416E+00	2	12	6.90	41.38	2.96	0.31
2.416E+00	-	2.583E+00	5	17	17.24	58.62	2.91	1.49
2.583E+00	-	2.749E+00	4	21	13.79	72.41	2.69	0.64
2.749E+00	-	2.916E+00	1	22	3.45	75.86	2.32	0.75
2.916E+00	-	3.083E+00	2	24	6.90	82.76	1.88	0.01
3.083E+00	-	3.249E+00	3	27	10.34	93.10	4.02	0.26
	G		2	29	6.90	100.00	0.35	7.78
	H		0	29				
	B		0	29				

TOTALS LESS H AND B 29

HISTOGRAM FOR VARIABLE 37 (AA-ZN-P)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
9.985E+00 XXX
1.466E+01 XXX
2.151E+01 XXX
3.157E+01
4.634E+01 XXXXXXXXXX
6.802E+01 XXXXXXX
9.985E+01 XXXXXXX
1.466E+02
2.151E+02 XXXXXXX
3.157E+02 XXXXXXXXXXXXXXXXX
4.635E+02 XXXXXXXXXXXXXX
6.803E+02 XXX
9.985E+02 XXXXXXX
1.466E+03 XXXXXXXXXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 1.00000E+01
MAXIMUM ANTILOG = 1.70000E+03
GEOMETRIC MEAN = 2.04224E+02
GEOMETRIC DEVIATION = 4.15518E+00
VARIANCE OF LOGS = 3.82654E-01

PERCENT TABLE FOR VARIABLE 37 (AA-ZN-P) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,
THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	3.199338E+00	1.582479E+03
95.00	1.000000E+35	1.000000E+35
98.00	1.000000E+35	1.000000E+35

D0036 GRAPHICAL ANALYSIS - U S G S STATPAC (02/07/82) DATE 7/20/84

Nevada data

FREQUENCY TABLE FOR VARIABLE 38 (AA-SB-P)

LOG LIMITS LOWER	-	UPPER	OBS FREQ	CUM FREQ	PERCENT FREQ	PERCENT CUM FREQ	THEOR FREQ (NORMAL DIST)	(THEOR FREQ - OBS FREQ)**2/THEOR FREQ
	N		1	1	3.45	3.45		
	L		0	1	0.00	3.45		
	T		0	1	0.00	3.45	1.94	1.94
2.500E-01	-	4.167E-01	4	5	13.79	17.24	1.18	6.77
4.167E-01	-	5.833E-01	0	5	0.00	17.24	1.62	1.62
5.833E-01	-	7.500E-01	2	7	6.90	24.14	2.09	0.00
7.500E-01	-	9.167E-01	5	12	17.24	41.38	2.52	2.45
9.167E-01	-	1.083E+00	2	14	6.90	48.28	2.84	0.25
1.083E+00	-	1.250E+00	2	16	6.90	55.17	2.99	0.33
1.250E+00	-	1.417E+00	1	17	3.45	58.62	2.94	1.28
1.417E+00	-	1.583E+00	1	18	3.45	62.07	2.71	1.08
1.583E+00	-	1.750E+00	2	20	6.90	68.97	2.34	0.05
1.750E+00	-	1.917E+00	4	24	13.79	82.76	1.88	2.38
1.917E+00	-	2.083E+00	3	27	10.34	93.10	1.42	1.76
2.083E+00	-	2.250E+00	2	29	6.90	100.00	2.54	0.11
	G		0	29	0.00	100.00	0.00	0.00
	H		0	29				
	B		0	29				

TOTALS LESS H AND B 29

HISTOGRAM FOR VARIABLE 38 (AA-SB-P)
MIDPOINTS ARE EXPRESSED AS ANTILOGS

```
2.154E+00 XXXXXXXXXXXXXX
3.162E+00
4.642E+00 XXXXXXX
6.813E+00 XXXXXXXXXXXXXXXXX
1.000E+01 XXXXXXX
1.468E+01 XXXXXXX
2.154E+01 XXX
3.162E+01 XXX
4.642E+01 XXXXXXX
6.813E+01 XXXXXXXXXXXXXX
1.000E+02 XXXXXXXXXX
1.468E+02 XXXXXXX
```

THE FOLLOWING STATISTICS ARE COMPUTED FOR THE UNQUALIFIED VALUES ONLY

MINIMUM ANTILOG = 2.00000E+00
MAXIMUM ANTILOG = 1.60000E+02
GEOMETRIC MEAN = 1.76049E+01
GEOMETRIC DEVIATION = 4.25417E+00
VARIANCE OF LOGS = 3.95408E-01

PERCENT TABLE FOR VARIABLE 38 (AA-SB-P) BY LINEAR INTERPOLATION FROM FREQUENCY TABLE
IF SELECTED PERCENTILES FALL WITHIN DATA EITHER ABOVE OR BELOW THE LIMITS OF DETECTION,

THE DATA VALUE ON THE TABLE IS GIVEN AS 0.9999991E 50

SELECTED PERCENTILE	DATA VALUE	ANTI LOG OF VALUE
90.00	2.033337E+00	1.079784E+02
95.00	1.000000E+35	1.000000E+35
98.00	1.000000E+35	1.000000E+35

```
$$$
```

D0101 CORRELATION ANALYSIS - USGS STATPAC (01/15/82)

DATE 7/20/84

TITLE	INPUT ID		N	M	***** OPTIONS *****	OUTPUT ID		N	M
	-ds-4	-	67	39	1 0 1 1 0 0 0 0 0 0	-	-	39	39

NUMBER OF SELECTED COLUMNS 39

SELECTED COLUMN INDICES

1	2	3	4	5	6	7	8	9	10
11	12	13	14	15	16	17	18	19	20
21	22	23	24	25	26	27	28	29	30
31	32	33	34	35	36	37	38	39	

SELECTED COLUMN IDENTIFIERS

X-COORD.	Y-COORD.	S-FE%	S-MG%	S-CA%	S-TI%	S-MN	S-AG	S-AS	S-AU
S-B	S-BA	S-BE	S-BI	S-CD	S-CO	S-CR	S-CU	S-LA	S-MO
S-NB	S-NI	S-PB	S-SB	S-SC	S-SN	S-SR	S-V	S-W	S-Y
S-ZN	S-ZR	S-TH	AA-AU-P	AA-AS-P	AA-ZN-P	AA-SB-P	SI-F	U-INST	

NUMBER OF SELECTED ROW PAIRS 1

SELECTED ROW PAIRS
1- 67

P H A S E T W O R E S U L T S

W A R N I N G * * * THE RESULTS FROM THIS PHASE "SHOULD NOT" BE ENTERED INTO D0096-FACTOR ANALYSIS.
THE CORRELATION MATRIX FROM THIS PHASE DOES NOT HAVE THE GRAMIAN PROPERTIES
WHICH ARE REQUIRED FOR FACTOR ANALYSIS.

D0101 CORRELATION ANALYSIS - USGS STATPAC (01/15/82) DATE 7/20/84

ARRAY OF MEANS -

		1 X-COORD.	2 Y-COORD.	3 S-FE%	4 S-MG%	5 S-CA%	6 S-TI%	7 S-MN	8 S-AG	9 S-AS	10 S-AU
1	X-COORD.	4.6221	4.6221	4.6221	4.6221	4.6221	4.6221	4.6221	4.6276	**********	**********
2	Y-COORD.	5.6208	5.6208	5.6208	5.6208	5.6208	5.6208	5.6208	5.6210	**********	**********
3	S-FE%	0.4521	0.4521	0.4521	0.4521	0.4521	0.4521	0.4521	0.5106	**********	**********
4	S-MG%	-0.1232	-0.1232	-0.1232	-0.1232	-0.1232	-0.1232	-0.1232	-0.2097	**********	**********
5	S-CA%	0.2387	0.2387	0.2387	0.2387	0.2387	0.2387	0.2387	0.0817	**********	**********
6	S-TI%	-0.4832	-0.4832	-0.4832	-0.4832	-0.4832	-0.4832	-0.4832	-0.4434	**********	**********
7	S-MN	2.7881	2.7881	2.7881	2.7881	2.7881	2.7881	2.7881	2.9650	**********	**********
8	S-AG	-0.1903	-0.1903	-0.1903	-0.1903	-0.1903	-0.1903	-0.1903	-0.1903	**********	**********
9	S-AS	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
10	S-AU	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
11	S-B	1.5404	1.5404	1.5404	1.5404	1.5404	1.5404	1.5404	1.4168	**********	**********
12	S-BA	2.7995	2.7995	2.7995	2.7995	2.7995	2.7995	2.7995	2.9833	**********	**********
13	S-BE	0.1121	0.1121	0.1121	0.1121	0.1121	0.1121	0.1121	0.1101	**********	**********
14	S-BI	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
15	S-CD	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
16	S-CO	1.1225	1.1225	1.1225	1.1225	1.1225	1.1225	1.1225	1.1193	**********	**********
17	S-CR	1.6313	1.6313	1.6313	1.6313	1.6313	1.6313	1.6313	1.4848	**********	**********
18	S-CU	1.2704	1.2704	1.2704	1.2704	1.2704	1.2704	1.2704	1.2293	**********	**********
19	S-LA	1.5395	1.5395	1.5395	1.5395	1.5395	1.5395	1.5395	1.6158	**********	**********
20	S-MO	0.7198	0.7198	0.7198	0.7198	0.7198	0.7198	0.7198	0.7720	**********	**********
21	S-NB	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
22	S-NI	1.1692	1.1692	1.1692	1.1692	1.1692	1.1692	1.1692	1.1257	**********	**********
23	S-PB	1.4803	1.4803	1.4803	1.4803	1.4803	1.4803	1.4803	1.8332	**********	**********
24	S-SB	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
25	S-SC	0.8772	0.8772	0.8772	0.8772	0.8772	0.8772	0.8772	0.8693	**********	**********
26	S-SN	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
27	S-SR	2.4545	2.4545	2.4545	2.4545	2.4545	2.4545	2.4545	2.3671	**********	**********
28	S-V	1.7623	1.7623	1.7623	1.7623	1.7623	1.7623	1.7623	1.7454	**********	**********
29	S-W	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
30	S-Y	1.2698	1.2698	1.2698	1.2698	1.2698	1.2698	1.2698	1.3074	**********	**********
31	S-ZN	2.3451	2.3451	2.3451	2.3451	2.3451	2.3451	2.3451	2.3010	**********	**********
32	S-ZR	2.1424	2.1424	2.1424	2.1424	2.1424	2.1424	2.1424	2.2386	**********	**********
33	S-TH	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
34	AA-AU-P	-1.3010	-1.3010	-1.3010	-1.3010	-1.3010	-1.3010	-1.3010	**********	**********	**********
35	AA-AS-P	1.1081	1.1081	1.1081	1.1081	1.1081	1.1081	1.1081	1.2454	**********	**********
36	AA-ZN-P	1.8432	1.8432	1.8432	1.8432	1.8432	1.8432	1.8432	2.0684	**********	**********
37	AA-SB-P	0.7804	0.7804	0.7804	0.7804	0.7804	0.7804	0.7804	0.8165	**********	**********
38	SI-F	2.6965	2.6965	2.6965	2.6965	2.6965	2.6965	2.6965	2.6945	**********	**********
39	U-INST	-0.0031	-0.0031	-0.0031	-0.0031	-0.0031	-0.0031	-0.0031	-0.0666	**********	**********

D0101 CORRELATION ANALYSIS - USGS STATPAC (01/15/82) DATE 7/20/84

ARRAY OF MEANS - CONT.

		11 S-B	12 S-BA	13 S-BE	14 S-BI	15 S-CD	16 S-CO	17 S-CR	18 S-CU	19 S-LA	20 S-MO
1	X-COORD.	4.6221	4.6221	4.6221	**********	**********	4.6221	4.6221	4.6221	4.6221	4.6206
2	Y-COORD.	5.6208	5.6208	5.6208	**********	**********	5.6208	5.6208	5.6208	5.6208	5.6207
3	S-FE%	0.4521	0.4521	0.4517	**********	**********	0.4521	0.4521	0.4521	0.4521	0.4333
4	S-MG%	-0.1232	-0.1232	-0.1205	**********	**********	-0.1232	-0.1232	-0.1232	-0.1232	-0.1064
5	S-CA%	0.2387	0.2387	0.2378	**********	**********	0.2387	0.2387	0.2387	0.2387	0.3499
6	S-TI%	-0.4832	-0.4832	-0.4859	**********	**********	-0.4832	-0.4832	-0.4832	-0.4832	-0.5593
7	S-MN	2.7881	2.7881	2.7849	**********	**********	2.7881	2.7881	2.7881	2.7881	2.7784
8	S-AG	-0.1903	-0.1903	-0.1903	**********	**********	-0.1903	-0.1903	-0.1903	-0.1903	-0.1505
9	S-AS	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
10	S-AU	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
11	S-B	1.5404	1.5404	1.5380	**********	**********	1.5404	1.5404	1.5404	1.5404	1.5267
12	S-BA	2.7995	2.7995	2.7988	**********	**********	2.7995	2.7995	2.7995	2.7995	2.8423
13	S-BE	0.1121	0.1121	0.1121	**********	**********	0.1121	0.1121	0.1121	0.1121	0.1258
14	S-BI	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
15	S-CD	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
16	S-CO	1.1225	1.1225	1.1217	**********	**********	1.1225	1.1225	1.1225	1.1225	1.1142
17	S-CR	1.6313	1.6313	1.6281	**********	**********	1.6313	1.6313	1.6313	1.6313	1.5571
18	S-CU	1.2704	1.2704	1.2745	**********	**********	1.2704	1.2704	1.2704	1.2704	1.4029
19	S-LA	1.5395	1.5395	1.5349	**********	**********	1.5395	1.5395	1.5395	1.5395	1.4794
20	S-MO	0.7198	0.7198	0.7198	**********	**********	0.7198	0.7198	0.7198	0.7198	0.7198
21	S-NB	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
22	S-NI	1.1692	1.1692	1.1691	**********	**********	1.1692	1.1692	1.1692	1.1692	1.3360
23	S-PB	1.4803	1.4803	1.4830	**********	**********	1.4803	1.4803	1.4803	1.4803	1.7042
24	S-SB	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
25	S-SC	0.8772	0.8772	0.8776	**********	**********	0.8772	0.8772	0.8772	0.8772	0.8255
26	S-SN	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
27	S-SR	2.4545	2.4545	2.4508	**********	**********	2.4545	2.4545	2.4545	2.4545	2.3513
28	S-V	1.7623	1.7623	1.7611	**********	**********	1.7623	1.7623	1.7623	1.7623	1.8949
29	S-W	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
30	S-Y	1.2698	1.2698	1.2712	**********	**********	1.2698	1.2698	1.2698	1.2698	1.2726
31	S-ZN	2.3451	2.3451	2.3451	**********	**********	2.3451	2.3451	2.3451	2.3451	2.3010
32	S-ZR	2.1424	2.1424	2.1445	**********	**********	2.1424	2.1424	2.1424	2.1424	2.0712
33	S-TH	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
34	AA-AU-P	-1.3010	-1.3010	-1.3010	**********	**********	-1.3010	-1.3010	-1.3010	-1.3010	**********
35	AA-AS-P	1.1081	1.1081	1.1098	**********	**********	1.1081	1.1081	1.1081	1.1081	1.3348
36	AA-ZN-P	1.8432	1.8432	1.8427	**********	**********	1.8432	1.8432	1.8432	1.8432	1.9697
37	AA-SB-P	0.7804	0.7804	0.7804	**********	**********	0.7804	0.7804	0.7804	0.7804	0.9621
38	SI-F	2.6965	2.6965	2.6965	**********	**********	2.6965	2.6965	2.6965	2.6965	2.7943
39	U-INST	-0.0031	-0.0031	-0.0031	**********	**********	-0.0031	-0.0031	-0.0031	-0.0031	0.0426

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ARRAY OF MEANS - CONT.

		21 S-NB	22 S-NI	23 S-PB	24 S-SB	25 S-SC	26 S-SN	27 S-SR	28 S-V	29 S-W	30 S-Y
1	X-COORD.	**********	4.6221	4.6221	**********	4.6221	**********	4.6221	4.6221	**********	4.6221
2	Y-COORD.	**********	5.6208	5.6208	**********	5.6208	**********	5.6208	5.6208	**********	5.6208
3	S-FE%	**********	0.4521	0.4521	**********	0.4521	**********	0.4521	0.4521	**********	0.4521
4	S-MG%	**********	-0.1232	-0.1232	**********	-0.1232	**********	-0.1232	-0.1232	**********	-0.1232
5	S-CA%	**********	0.2387	0.2387	**********	0.2387	**********	0.2387	0.2387	**********	0.2387
6	S-TI%	**********	-0.4832	-0.4832	**********	-0.4832	**********	-0.4832	-0.4832	**********	-0.4832
7	S-MN	**********	2.7881	2.7881	**********	2.7881	**********	2.7881	2.7881	**********	2.7881
8	S-AG	**********	-0.1903	-0.1903	**********	-0.1903	**********	-0.1903	-0.1903	**********	-0.1903
9	S-AS	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
10	S-AU	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
11	S-B	**********	1.5404	1.5404	**********	1.5404	**********	1.5404	1.5404	**********	1.5404
12	S-BA	**********	2.7995	2.7995	**********	2.7995	**********	2.7995	2.7995	**********	2.7995
13	S-BE	**********	0.1121	0.1121	**********	0.1121	**********	0.1121	0.1121	**********	0.1121
14	S-BI	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
15	S-CD	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
16	S-CO	**********	1.1225	1.1225	**********	1.1225	**********	1.1225	1.1225	**********	1.1225
17	S-CR	**********	1.6313	1.6313	**********	1.6313	**********	1.6313	1.6313	**********	1.6313
18	S-CU	**********	1.2704	1.2704	**********	1.2704	**********	1.2704	1.2704	**********	1.2704
19	S-LA	**********	1.5395	1.5395	**********	1.5395	**********	1.5395	1.5395	**********	1.5395
20	S-MO	**********	0.7198	0.7198	**********	0.7198	**********	0.7198	0.7198	**********	0.7198
21	S-NB	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
22	S-NI	**********	1.1692	1.1692	**********	1.1692	**********	1.1692	1.1692	**********	1.1692
23	S-PB	**********	1.4803	1.4803	**********	1.4803	**********	1.4803	1.4803	**********	1.4803
24	S-SB	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
25	S-SC	**********	0.8772	0.8772	**********	0.8772	**********	0.8772	0.8772	**********	0.8772
26	S-SN	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
27	S-SR	**********	2.4545	2.4545	**********	2.4545	**********	2.4545	2.4545	**********	2.4545
28	S-V	**********	1.7623	1.7623	**********	1.7623	**********	1.7623	1.7623	**********	1.7623
29	S-W	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
30	S-Y	**********	1.2698	1.2698	**********	1.2698	**********	1.2698	1.2698	**********	1.2698
31	S-ZN	**********	2.3451	2.3451	**********	2.3451	**********	2.3451	2.3451	**********	2.3451
32	S-ZR	**********	2.1424	2.1424	**********	2.1424	**********	2.1424	2.1424	**********	2.1424
33	S-TH	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
34	AA-AU-P	**********	-1.3010	-1.3010	**********	-1.3010	**********	-1.3010	-1.3010	**********	-1.3010
35	AA-AS-P	**********	1.1081	1.1081	**********	1.1081	**********	1.1081	1.1081	**********	1.1081
36	AA-ZN-P	**********	1.8432	1.8432	**********	1.8432	**********	1.8432	1.8432	**********	1.8432
37	AA-SB-P	**********	0.7804	0.7804	**********	0.7804	**********	0.7804	0.7804	**********	0.7804
38	SI-F	**********	2.6965	2.6965	**********	2.6965	**********	2.6965	2.6965	**********	2.6965
39	U-INST	**********	-0.0031	-0.0031	**********	-0.0031	**********	-0.0031	-0.0031	**********	-0.0031

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ARRAY OF MEANS - CONT.

		31 S-ZN	32 S-ZR	33 S-TH	34 AA-AU-P	35 AA-AS-P	36 AA-ZN-P	37 AA-SB-P	38 SI-F	39 U-INST
1	X-COORD.	4.6196	4.6221	**********	4.6298	4.6221	4.6221	4.6292	4.6208	4.6208
2	Y-COORD.	5.6210	5.6208	**********	5.6204	5.6208	5.6208	5.6213	5.6208	5.6208
3	S-FE%	0.6246	0.4521	**********	0.3010	0.4521	0.4521	0.4585	0.4620	0.4620
4	S-MG%	-0.0722	-0.1232	**********	-0.3010	-0.1232	-0.1232	-0.1967	-0.1316	-0.1316
5	S-CA%	0.2628	0.2387	**********	0.0000	0.2387	0.2387	0.0755	0.2454	0.2454
6	S-TI%	-0.3754	-0.4832	**********	-0.5229	-0.4832	-0.4832	-0.5480	-0.4836	-0.4836
7	S-MN	2.9688	2.7881	**********	2.6990	2.7881	2.7881	2.9809	2.7846	2.7846
8	S-AG	0.0000	-0.1903	**********	**********	-0.1903	-0.1903	-0.2116	-0.1903	-0.1903
9	S-AS	**********	**********	**********	**********	**********	**********	**********	**********	**********
10	S-AU	**********	**********	**********	**********	**********	**********	**********	**********	**********
11	S-B	1.3891	1.5404	**********	1.3010	1.5404	1.5404	1.4902	1.4927	1.4927
12	S-BA	2.8746	2.7995	**********	2.8451	2.7995	2.7995	3.0239	2.7975	2.7975
13	S-BE	0.0880	0.1121	**********	0.0000	0.1121	0.1121	0.1509	0.1161	0.1161
14	S-BI	**********	**********	**********	**********	**********	**********	**********	**********	**********
15	S-CD	**********	**********	**********	**********	**********	**********	**********	**********	**********
16	S-CO	1.2826	1.1225	**********	1.0000	1.1225	1.1225	1.0503	1.1364	1.1364
17	S-CR	1.8746	1.6313	**********	1.3010	1.6313	1.6313	1.4333	1.6473	1.6473
18	S-CU	1.5053	1.2704	**********	1.0000	1.2704	1.2704	1.2118	1.2974	1.2974
19	S-LA	1.6998	1.5395	**********	1.4771	1.5395	1.5395	1.5722	1.5415	1.5415
20	S-MO	0.6990	0.7198	**********	**********	0.7198	0.7198	0.7720	0.7198	0.7198
21	S-NB	**********	**********	**********	**********	**********	**********	**********	**********	**********
22	S-NI	1.2940	1.1692	**********	1.0000	1.1692	1.1692	1.0503	1.2013	1.2013
23	S-PB	1.6998	1.4803	**********	1.3010	1.4803	1.4803	1.8728	1.5289	1.5289
24	S-SB	**********	**********	**********	**********	**********	**********	**********	**********	**********
25	S-SC	0.9660	0.8772	**********	0.8451	0.8772	0.8772	0.8033	0.8966	0.8966
26	S-SN	**********	**********	**********	**********	**********	**********	**********	**********	**********
27	S-SR	2.5000	2.4545	**********	2.6990	2.4545	2.4545	2.3765	2.4264	2.4264
28	S-V	2.1558	1.7623	**********	1.6990	1.7623	1.7623	1.7090	1.7939	1.7939
29	S-W	**********	**********	**********	**********	**********	**********	**********	**********	**********
30	S-Y	1.3451	1.2698	**********	1.1761	1.2698	1.2698	1.2832	1.2761	1.2761
31	S-ZN	2.3451	2.3451	**********	**********	2.3451	2.3451	2.3010	2.3451	2.3451
32	S-ZR	2.1945	2.1424	**********	2.1761	2.1424	2.1424	2.2223	2.1414	2.1414
33	S-TH	**********	**********	**********	**********	**********	**********	**********	**********	**********
34	AA-AU-P	**********	-1.3010	**********	-1.3010	-1.3010	-1.3010	**********	-1.3010	-1.3010
35	AA-AS-P	1.2113	1.1081	**********	0.6990	1.1081	1.1081	1.4580	1.1258	1.1258
36	AA-ZN-P	2.3367	1.8432	**********	1.5441	1.8432	1.8432	2.1855	1.8866	1.8866
37	AA-SB-P	1.1461	0.7804	**********	**********	0.7804	0.7804	0.7804	0.8101	0.8101
38	SI-F	2.6391	2.6965	**********	2.4771	2.6965	2.6965	2.7336	2.6965	2.6965
39	U-INST	0.1678	-0.0031	**********	-0.0706	-0.0031	-0.0031	-0.0917	-0.0031	-0.0031

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ARRAY OF VARIANCES -

		1 X-COORD.	2 Y-COORD.	3 S-FE%	4 S-MG%	5 S-CA%	6 S-TI%	7 S-MN	8 S-AG	9 S-AS	10 S-AU
1	X-COORD.	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	**********	**********
2	Y-COORD.	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	**********	**********
3	S-FE%	0.017	0.017	0.017	0.017	0.017	0.017	0.017	0.017	**********	**********
4	S-MG%	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.006	**********	**********
5	S-CA%	0.037	0.037	0.037	0.037	0.037	0.037	0.037	0.014	**********	**********
6	S-TI%	0.017	0.017	0.017	0.017	0.017	0.017	0.017	0.031	**********	**********
7	S-MN	0.018	0.018	0.018	0.018	0.018	0.018	0.018	0.019	**********	**********
8	S-AG	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.011	**********	**********
9	S-AS	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
10	S-AU	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
11	S-B	0.050	0.050	0.050	0.050	0.050	0.050	0.050	0.021	**********	**********
12	S-BA	0.027	0.027	0.027	0.027	0.027	0.027	0.027	0.037	**********	**********
13	S-BE	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.008	**********	**********
14	S-BI	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
15	S-CD	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
16	S-CO	0.015	0.015	0.015	0.015	0.015	0.015	0.015	0.018	**********	**********
17	S-CR	0.053	0.053	0.053	0.053	0.053	0.053	0.053	0.040	**********	**********
18	S-CU	0.055	0.055	0.055	0.055	0.055	0.055	0.055	0.012	**********	**********
19	S-LA	0.025	0.025	0.025	0.025	0.025	0.025	0.025	0.013	**********	**********
20	S-MO	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.011	**********	**********
21	S-NB	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
22	S-NI	0.035	0.035	0.035	0.035	0.035	0.035	0.035	0.028	**********	**********
23	S-PB	0.044	0.044	0.044	0.044	0.044	0.044	0.044	0.061	**********	**********
24	S-SB	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
25	S-SC	0.012	0.012	0.012	0.012	0.012	0.012	0.012	0.025	**********	**********
26	S-SN	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
27	S-SR	0.020	0.020	0.020	0.020	0.020	0.020	0.020	0.008	**********	**********
28	S-V	0.030	0.030	0.030	0.030	0.030	0.030	0.030	0.024	**********	**********
29	S-W	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
30	S-Y	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.007	**********	**********
31	S-ZN	0.008	0.008	0.008	0.008	0.008	0.008	0.008	**********	**********	**********
32	S-ZR	0.020	0.020	0.020	0.020	0.020	0.020	0.020	0.020	**********	**********
33	S-TH	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
34	AA-AU-P	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
35	AA-AS-P	0.095	0.095	0.095	0.095	0.095	0.095	0.095	0.128	**********	**********
36	AA-ZN-P	0.047	0.047	0.047	0.047	0.047	0.047	0.047	0.056	**********	**********
37	AA-SB-P	0.033	0.033	0.033	0.033	0.033	0.033	0.033	0.040	**********	**********
38	SI-F	0.022	0.022	0.022	0.022	0.022	0.022	0.022	0.004	**********	**********
39	U-INST	0.021	0.021	0.021	0.021	0.021	0.021	0.021	0.019	**********	**********

D0101 CORRELATION ANALYSIS - USGS STATPAC (01/15/82) DATE 7/20/84

ARRAY OF VARIANCES - CONT.

		11 S-B	12 S-BA	13 S-BE	14 S-BI	15 S-CD	16 S-CO	17 S-CR	18 S-CU	19 S-LA	20 S-MO
1	X-COORD.	0.000	0.000	0.000	**********	**********	0.000	0.000	0.000	0.000	0.000
2	Y-COORD.	0.000	0.000	0.000	**********	**********	0.000	0.000	0.000	0.000	0.000
3	S-FE%	0.017	0.017	0.017	**********	**********	0.017	0.017	0.017	0.017	0.021
4	S-MG%	0.011	0.011	0.011	**********	**********	0.011	0.011	0.011	0.011	0.023
5	S-CA%	0.037	0.037	0.038	**********	**********	0.037	0.037	0.037	0.037	0.112
6	S-TI%	0.017	0.017	0.016	**********	**********	0.017	0.017	0.017	0.017	0.027
7	S-MN	0.018	0.018	0.017	**********	**********	0.018	0.018	0.018	0.018	0.054
8	S-AG	0.011	0.011	0.011	**********	**********	0.011	0.011	0.011	0.011	0.045
9	S-AS	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
10	S-AU	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
11	S-B	0.050	0.050	0.051	**********	**********	0.050	0.050	0.050	0.050	0.048
12	S-BA	0.027	0.027	0.028	**********	**********	0.027	0.027	0.027	0.027	0.086
13	S-BE	0.007	0.007	0.007	**********	**********	0.007	0.007	0.007	0.007	0.007
14	S-BI	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
15	S-CD	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
16	S-CO	0.015	0.015	0.015	**********	**********	0.015	0.015	0.015	0.015	0.029
17	S-CR	0.053	0.053	0.053	**********	**********	0.053	0.053	0.053	0.053	0.043
18	S-CU	0.055	0.055	0.055	**********	**********	0.055	0.055	0.055	0.055	0.112
19	S-LA	0.025	0.025	0.024	**********	**********	0.025	0.025	0.025	0.025	0.033
20	S-MO	0.003	0.003	0.003	**********	**********	0.003	0.003	0.003	0.003	0.003
21	S-NB	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
22	S-NI	0.035	0.035	0.035	**********	**********	0.035	0.035	0.035	0.035	0.089
23	S-PB	0.044	0.044	0.044	**********	**********	0.044	0.044	0.044	0.044	0.089
24	S-SB	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
25	S-SC	0.012	0.012	0.012	**********	**********	0.012	0.012	0.012	0.012	0.011
26	S-SN	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
27	S-SR	0.020	0.020	0.020	**********	**********	0.020	0.020	0.020	0.020	0.007
28	S-V	0.030	0.030	0.030	**********	**********	0.030	0.030	0.030	0.030	0.061
29	S-W	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
30	S-Y	0.005	0.005	0.005	**********	**********	0.005	0.005	0.005	0.005	0.012
31	S-ZN	0.008	0.008	0.008	**********	**********	0.008	0.008	0.008	0.008	0.000
32	S-ZR	0.020	0.020	0.020	**********	**********	0.020	0.020	0.020	0.020	0.024
33	S-TH	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
34	AA-AU-P	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
35	AA-AS-P	0.095	0.095	0.097	**********	**********	0.095	0.095	0.095	0.095	0.078
36	AA-ZN-P	0.047	0.047	0.048	**********	**********	0.047	0.047	0.047	0.047	0.093
37	AA-SB-P	0.033	0.033	0.033	**********	**********	0.033	0.033	0.033	0.033	0.068
38	SI-F	0.022	0.022	0.022	**********	**********	0.022	0.022	0.022	0.022	0.014
39	U-INST	0.021	0.021	0.021	**********	**********	0.021	0.021	0.021	0.021	0.025

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ARRAY OF VARIANCES - CONT.

		21 S-NB	22 S-NI	23 S-PB	24 S-SB	25 S-SC	26 S-SN	27 S-SR	28 S-V	29 S-W	30 S-Y
1	X-COORD.	**********	0.000	0.000	**********	0.000	**********	0.000	0.000	**********	0.000
2	Y-COORD.	**********	0.000	0.000	**********	0.000	**********	0.000	0.000	**********	0.000
3	S-FE%	**********	0.017	0.017	**********	0.017	**********	0.017	0.017	**********	0.017
4	S-MG%	**********	0.011	0.011	**********	0.011	**********	0.011	0.011	**********	0.011
5	S-CA%	**********	0.037	0.037	**********	0.037	**********	0.037	0.037	**********	0.037
6	S-TI%	**********	0.017	0.017	**********	0.017	**********	0.017	0.017	**********	0.017
7	S-MN	**********	0.018	0.018	**********	0.018	**********	0.018	0.018	**********	0.018
8	S-AG	**********	0.011	0.011	**********	0.011	**********	0.011	0.011	**********	0.011
9	S-AS	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
10	S-AU	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
11	S-B	**********	0.050	0.050	**********	0.050	**********	0.050	0.050	**********	0.050
12	S-BA	**********	0.027	0.027	**********	0.027	**********	0.027	0.027	**********	0.027
13	S-BE	**********	0.007	0.007	**********	0.007	**********	0.007	0.007	**********	0.007
14	S-BI	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
15	S-CD	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
16	S-CO	**********	0.015	0.015	**********	0.015	**********	0.015	0.015	**********	0.015
17	S-CR	**********	0.053	0.053	**********	0.053	**********	0.053	0.053	**********	0.053
18	S-CU	**********	0.055	0.055	**********	0.055	**********	0.055	0.055	**********	0.055
19	S-LA	**********	0.025	0.025	**********	0.025	**********	0.025	0.025	**********	0.025
20	S-MO	**********	0.003	0.003	**********	0.003	**********	0.003	0.003	**********	0.003
21	S-NB	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
22	S-NI	**********	0.035	0.035	**********	0.035	**********	0.035	0.035	**********	0.035
23	S-PB	**********	0.044	0.044	**********	0.044	**********	0.044	0.044	**********	0.044
24	S-SB	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
25	S-SC	**********	0.012	0.012	**********	0.012	**********	0.012	0.012	**********	0.012
26	S-SN	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
27	S-SR	**********	0.020	0.020	**********	0.020	**********	0.020	0.020	**********	0.020
28	S-V	**********	0.030	0.030	**********	0.030	**********	0.030	0.030	**********	0.030
29	S-W	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
30	S-Y	**********	0.005	0.005	**********	0.005	**********	0.005	0.005	**********	0.005
31	S-ZN	**********	0.008	0.008	**********	0.008	**********	0.008	0.008	**********	0.008
32	S-ZR	**********	0.020	0.020	**********	0.020	**********	0.020	0.020	**********	0.020
33	S-TH	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
34	AA-AU-P	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
35	AA-AS-P	**********	0.095	0.095	**********	0.095	**********	0.095	0.095	**********	0.095
36	AA-ZN-P	**********	0.047	0.047	**********	0.047	**********	0.047	0.047	**********	0.047
37	AA-SB-P	**********	0.033	0.033	**********	0.033	**********	0.033	0.033	**********	0.033
38	SI-F	**********	0.022	0.022	**********	0.022	**********	0.022	0.022	**********	0.022
39	U-INST	**********	0.021	0.021	**********	0.021	**********	0.021	0.021	**********	0.021

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ARRAY OF VARIANCES - CONT.

		31 S-ZN	32 S-ZR	33 S-TH	34 AA-AU-P	35 AA-AS-P	36 AA-ZN-P	37 AA-SB-P	38 SI-F	39 U-INST
1	X-COORD.	0.000	0.000	**********	**********	0.000	0.000	0.000	0.000	0.000
2	Y-COORD.	0.000	0.000	**********	**********	0.000	0.000	0.000	0.000	0.000
3	S-FE%	0.033	0.017	**********	**********	0.017	0.017	0.018	0.020	0.020
4	S-MG%	0.027	0.011	**********	**********	0.011	0.011	0.005	0.012	0.012
5	S-CA%	0.091	0.037	**********	**********	0.037	0.037	0.009	0.048	0.048
6	S-TI%	0.033	0.017	**********	**********	0.017	0.017	0.004	0.020	0.020
7	S-MN	0.039	0.018	**********	**********	0.018	0.018	0.013	0.023	0.023
8	S-AG	**********	0.011	**********	**********	0.011	0.011	0.018	0.011	0.011
9	S-AS	**********	**********	**********	**********	**********	**********	**********	**********	**********
10	S-AU	**********	**********	**********	**********	**********	**********	**********	**********	**********
11	S-B	0.010	0.050	**********	**********	0.050	0.050	0.027	0.038	0.038
12	S-BA	0.088	0.027	**********	**********	0.027	0.027	0.028	0.029	0.029
13	S-BE	0.010	0.007	**********	**********	0.007	0.007	0.004	0.007	0.007
14	S-BI	**********	**********	**********	**********	**********	**********	**********	**********	**********
15	S-CD	**********	**********	**********	**********	**********	**********	**********	**********	**********
16	S-CO	0.020	0.015	**********	**********	0.015	0.015	0.007	0.015	0.015
17	S-CR	0.171	0.053	**********	**********	0.053	0.053	0.021	0.058	0.058
18	S-CU	0.101	0.055	**********	**********	0.055	0.055	0.004	0.042	0.042
19	S-LA	0.070	0.025	**********	**********	0.025	0.025	0.014	0.029	0.029
20	S-MO	0.000	0.003	**********	**********	0.003	0.003	0.011	0.003	0.003
21	S-NB	**********	**********	**********	**********	**********	**********	**********	**********	**********
22	S-NI	0.088	0.035	**********	**********	0.035	0.035	0.007	0.033	0.033
23	S-PB	0.152	0.044	**********	**********	0.044	0.044	0.028	0.054	0.054
24	S-SB	**********	**********	**********	**********	**********	**********	**********	**********	**********
25	S-SC	0.025	0.012	**********	**********	0.012	0.012	0.005	0.014	0.014
26	S-SN	**********	**********	**********	**********	**********	**********	**********	**********	**********
27	S-SR	0.053	0.020	**********	**********	0.020	0.020	0.009	0.016	0.016
28	S-V	0.046	0.030	**********	**********	0.030	0.030	0.015	0.032	0.032
29	S-W	**********	**********	**********	**********	**********	**********	**********	**********	**********
30	S-Y	0.008	0.005	**********	**********	0.005	0.005	0.002	0.006	0.006
31	S-ZN	0.008	0.008	**********	**********	0.008	0.008	**********	0.008	0.008
32	S-ZR	0.020	0.020	**********	**********	0.020	0.020	0.013	0.025	0.025
33	S-TH	**********	**********	**********	**********	**********	**********	**********	**********	**********
34	AA-AU-P	**********	**********	**********	**********	**********	**********	**********	**********	**********
35	AA-AS-P	0.069	0.095	**********	**********	0.095	0.095	0.046	0.070	0.070
36	AA-ZN-P	0.001	0.047	**********	**********	0.047	0.047	0.011	0.050	0.050
37	AA-SB-P	**********	0.033	**********	**********	0.033	0.033	0.033	0.032	0.032
38	SI-F	0.042	0.022	**********	**********	0.022	0.022	0.007	0.022	0.022
39	U-INST	0.040	0.021	**********	**********	0.021	0.021	0.019	0.021	0.021

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COLUMN	VERSUS	COLUMN	CORRELATION COEFFICIENT	NO. OF PAIRS
1 (X-COORD.)	2	(Y-COORD.)	0.0527	67
1 (X-COORD.)	3	(S-FE%)	0.0001	67
1 (X-COORD.)	4	(S-MG%)	-0.2905	67
1 (X-COORD.)	5	(S-CA%)	-0.5124	67
1 (X-COORD.)	6	(S-TI%)	0.0410	67
1 (X-COORD.)	7	(S-MN)	0.4743	67
1 (X-COORD.)	8	(S-AG)	-0.2211	8
1 (X-COORD.)	9	(S-AS)	********	0
1 (X-COORD.)	10	(S-AU)	********	0
1 (X-COORD.)	11	(S-B)	-0.2118	67
1 (X-COORD.)	12	(S-BA)	0.4606	67
1 (X-COORD.)	13	(S-BE)	-0.0167	66
1 (X-COORD.)	14	(S-BI)	********	0
1 (X-COORD.)	15	(S-CD)	********	0
1 (X-COORD.)	16	(S-CO)	-0.4308	67
1 (X-COORD.)	17	(S-CR)	-0.5536	67
1 (X-COORD.)	18	(S-CU)	-0.4831	67
1 (X-COORD.)	19	(S-LA)	0.0417	67
1 (X-COORD.)	20	(S-MO)	0.5838	7
1 (X-COORD.)	21	(S-NB)	********	0
1 (X-COORD.)	22	(S-NI)	-0.6344	67
1 (X-COORD.)	23	(S-PB)	0.2838	67
1 (X-COORD.)	24	(S-SB)	********	0
1 (X-COORD.)	25	(S-SC)	-0.2956	67
1 (X-COORD.)	26	(S-SN)	********	0
1 (X-COORD.)	27	(S-SR)	0.2935	67
1 (X-COORD.)	28	(S-V)	-0.1566	67
1 (X-COORD.)	29	(S-W)	********	0
1 (X-COORD.)	30	(S-Y)	0.0435	67
1 (X-COORD.)	31	(S-ZN)	-0.4147	4
1 (X-COORD.)	32	(S-ZR)	0.4091	67
1 (X-COORD.)	33	(S-TH)	********	0
1 (X-COORD.)	34	(AA-AU-P)	********	1
1 (X-COORD.)	35	(AA-AS-P)	-0.1830	67
1 (X-COORD.)	36	(AA-ZN-P)	-0.0568	67
1 (X-COORD.)	37	(AA-SB-P)	-0.3439	7
1 (X-COORD.)	38	(SI-F)	-0.4261	44
1 (X-COORD.)	39	(U-INST)	-0.5010	44
2 (Y-COORD.)	3	(S-FE%)	0.1026	67
2 (Y-COORD.)	4	(S-MG%)	-0.1299	67
2 (Y-COORD.)	5	(S-CA%)	-0.3102	67
2 (Y-COORD.)	6	(S-TI%)	0.0737	67
2 (Y-COORD.)	7	(S-MN)	0.2357	67
2 (Y-COORD.)	8	(S-AG)	-0.0476	8
2 (Y-COORD.)	9	(S-AS)	********	0
2 (Y-COORD.)	10	(S-AU)	********	0
2 (Y-COORD.)	11	(S-B)	0.0942	67
2 (Y-COORD.)	12	(S-BA)	0.4336	67
2 (Y-COORD.)	13	(S-BE)	-0.0526	66
2 (Y-COORD.)	14	(S-BI)	********	0

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COLUMN	VERSUS	COLUMN	CORRELATION COEFFICIENT	NO. OF PAIRS
2 (Y-COORD.)	15	(S-CD)	********	0
2 (Y-COORD.)	16	(S-CO)	0.1285	67
2 (Y-COORD.)	17	(S-CR)	0.0485	67
2 (Y-COORD.)	18	(S-CU)	-0.2057	67
2 (Y-COORD.)	19	(S-LA)	-0.0522	67
2 (Y-COORD.)	20	(S-MO)	0.2119	7
2 (Y-COORD.)	21	(S-NB)	********	0
2 (Y-COORD.)	22	(S-NI)	-0.2707	67
2 (Y-COORD.)	23	(S-PB)	0.0874	67
2 (Y-COORD.)	24	(S-SB)	********	0
2 (Y-COORD.)	25	(S-SC)	0.0295	67
2 (Y-COORD.)	26	(S-SN)	********	0
2 (Y-COORD.)	27	(S-SR)	0.0994	67
2 (Y-COORD.)	28	(S-V)	-0.0799	67
2 (Y-COORD.)	29	(S-W)	********	0
2 (Y-COORD.)	30	(S-Y)	-0.2386	67
2 (Y-COORD.)	31	(S-ZN)	0.2685	4
2 (Y-COORD.)	32	(S-ZR)	0.1723	67
2 (Y-COORD.)	33	(S-TH)	********	0
2 (Y-COORD.)	34	(AA-AU-P)	********	1
2 (Y-COORD.)	35	(AA-AS-P)	0.5433	67
2 (Y-COORD.)	36	(AA-ZN-P)	0.1804	67
2 (Y-COORD.)	37	(AA-SB-P)	-0.0148	7
2 (Y-COORD.)	38	(SI-F)	-0.1660	44
2 (Y-COORD.)	39	(U-INST)	-0.1429	44
3 (S-FE%)	4	(S-MG%)	-0.0638	67
3 (S-FE%)	5	(S-CA%)	-0.2285	67
3 (S-FE%)	6	(S-TI%)	0.6121	67
3 (S-FE%)	7	(S-MN)	0.4280	67
3 (S-FE%)	8	(S-AG)	0.0288	8
3 (S-FE%)	9	(S-AS)	********	0
3 (S-FE%)	10	(S-AU)	********	0
3 (S-FE%)	11	(S-B)	-0.4251	67
3 (S-FE%)	12	(S-BA)	0.1767	67
3 (S-FE%)	13	(S-BE)	-0.2876	66
3 (S-FE%)	14	(S-BI)	********	0
3 (S-FE%)	15	(S-CD)	********	0
3 (S-FE%)	16	(S-CO)	0.4938	67
3 (S-FE%)	17	(S-CR)	0.3774	67
3 (S-FE%)	18	(S-CU)	0.1509	67
3 (S-FE%)	19	(S-LA)	0.1935	67
3 (S-FE%)	20	(S-MO)	0.7993	7
3 (S-FE%)	21	(S-NB)	********	0
3 (S-FE%)	22	(S-NI)	0.0550	67
3 (S-FE%)	23	(S-PB)	-0.0274	67
3 (S-FE%)	24	(S-SB)	********	0
3 (S-FE%)	25	(S-SC)	0.4768	67
3 (S-FE%)	26	(S-SN)	********	0
3 (S-FE%)	27	(S-SR)	0.1359	67
3 (S-FE%)	28	(S-V)	0.6368	67

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COLUMN	VERSUS	COLUMN	CORRELATION COEFFICIENT	NO. OF PAIRS
3 (S-FE%)	29	(S-W)	********	0
3 (S-FE%)	30	(S-Y)	0.2966	67
3 (S-FE%)	31	(S-ZN)	0.8149	4
3 (S-FE%)	32	(S-ZR)	0.4414	67
3 (S-FE%)	33	(S-TH)	********	0
3 (S-FE%)	34	(AA-AU-P)	********	1
3 (S-FE%)	35	(AA-AS-P)	-0.0451	67
3 (S-FE%)	36	(AA-ZN-P)	0.3604	67
3 (S-FE%)	37	(AA-SB-P)	0.2136	7
3 (S-FE%)	38	(SI-F)	-0.2954	44
3 (S-FE%)	39	(U-INST)	0.1443	44
4 (S-MG%)	5	(S-CA%)	0.5526	67
4 (S-MG%)	6	(S-TI%)	-0.2468	67
4 (S-MG%)	7	(S-MN)	-0.1930	67
4 (S-MG%)	8	(S-AG)	0.1041	8
4 (S-MG%)	9	(S-AS)	********	0
4 (S-MG%)	10	(S-AU)	********	0
4 (S-MG%)	11	(S-B)	0.1681	67
4 (S-MG%)	12	(S-BA)	-0.3156	67
4 (S-MG%)	13	(S-BE)	0.0579	66
4 (S-MG%)	14	(S-BI)	********	0
4 (S-MG%)	15	(S-CD)	********	0
4 (S-MG%)	16	(S-CO)	0.2590	67
4 (S-MG%)	17	(S-CR)	0.2047	67
4 (S-MG%)	18	(S-CU)	0.4023	67
4 (S-MG%)	19	(S-LA)	-0.1981	67
4 (S-MG%)	20	(S-MO)	-0.5652	7
4 (S-MG%)	21	(S-NB)	********	0
4 (S-MG%)	22	(S-NI)	0.3091	67
4 (S-MG%)	23	(S-PB)	-0.0049	67
4 (S-MG%)	24	(S-SB)	********	0
4 (S-MG%)	25	(S-SC)	0.0326	67
4 (S-MG%)	26	(S-SN)	********	0
4 (S-MG%)	27	(S-SR)	-0.0790	67
4 (S-MG%)	28	(S-V)	0.1330	67
4 (S-MG%)	29	(S-W)	********	0
4 (S-MG%)	30	(S-Y)	0.0049	67
4 (S-MG%)	31	(S-ZN)	-0.3333	4
4 (S-MG%)	32	(S-ZR)	-0.4443	67
4 (S-MG%)	33	(S-TH)	********	0
4 (S-MG%)	34	(AA-AU-P)	********	1
4 (S-MG%)	35	(AA-AS-P)	0.0831	67
4 (S-MG%)	36	(AA-ZN-P)	0.1711	67
4 (S-MG%)	37	(AA-SB-P)	0.0085	7
4 (S-MG%)	38	(SI-F)	0.3513	44
4 (S-MG%)	39	(U-INST)	0.2281	44
5 (S-CA%)	6	(S-TI%)	-0.3267	67
5 (S-CA%)	7	(S-MN)	-0.3229	67
5 (S-CA%)	8	(S-AG)	-0.0294	8
5 (S-CA%)	9	(S-AS)	********	0

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COLUMN	VERSUS	COLUMN	CORRELATION COEFFICIENT	NO. OF PAIRS
5 (S-CA%)	10	(S-AU)	********	0
5 (S-CA%)	11	(S-B)	0.3440	67
5 (S-CA%)	12	(S-BA)	-0.5354	67
5 (S-CA%)	13	(S-BE)	-0.0048	66
5 (S-CA%)	14	(S-BI)	********	0
5 (S-CA%)	15	(S-CD)	********	0
5 (S-CA%)	16	(S-CO)	0.2946	67
5 (S-CA%)	17	(S-CR)	0.3547	67
5 (S-CA%)	18	(S-CU)	0.5952	67
5 (S-CA%)	19	(S-LA)	-0.0400	67
5 (S-CA%)	20	(S-MO)	-0.4614	7
5 (S-CA%)	21	(S-NB)	********	0
5 (S-CA%)	22	(S-NI)	0.6650	67
5 (S-CA%)	23	(S-PB)	-0.0840	67
5 (S-CA%)	24	(S-SB)	********	0
5 (S-CA%)	25	(S-SC)	0.0162	67
5 (S-CA%)	26	(S-SN)	********	0
5 (S-CA%)	27	(S-SR)	-0.1973	67
5 (S-CA%)	28	(S-V)	0.1686	67
5 (S-CA%)	29	(S-W)	********	0
5 (S-CA%)	30	(S-Y)	0.0096	67
5 (S-CA%)	31	(S-ZN)	-0.1911	4
5 (S-CA%)	32	(S-ZR)	-0.6052	67
5 (S-CA%)	33	(S-TH)	********	0
5 (S-CA%)	34	(AA-AU-P)	********	1
5 (S-CA%)	35	(AA-AS-P)	0.1621	67
5 (S-CA%)	36	(AA-ZN-P)	0.1844	67
5 (S-CA%)	37	(AA-SB-P)	-0.3144	7
5 (S-CA%)	38	(SI-F)	0.5603	44
5 (S-CA%)	39	(U-INST)	0.4280	44
6 (S-TI%)	7	(S-MN)	0.3457	67
6 (S-TI%)	8	(S-AG)	0.3732	8
6 (S-TI%)	9	(S-AS)	********	0
6 (S-TI%)	10	(S-AU)	********	0
6 (S-TI%)	11	(S-B)	-0.2067	67
6 (S-TI%)	12	(S-BA)	0.0380	67
6 (S-TI%)	13	(S-BE)	-0.0756	66
6 (S-TI%)	14	(S-BI)	********	0
6 (S-TI%)	15	(S-CD)	********	0
6 (S-TI%)	16	(S-CO)	0.5116	67
6 (S-TI%)	17	(S-CR)	0.2766	67
6 (S-TI%)	18	(S-CU)	0.0078	67
6 (S-TI%)	19	(S-LA)	0.3331	67
6 (S-TI%)	20	(S-MO)	0.0980	7
6 (S-TI%)	21	(S-NB)	********	0
6 (S-TI%)	22	(S-NI)	-0.0133	67
6 (S-TI%)	23	(S-PB)	-0.1224	67
6 (S-TI%)	24	(S-SB)	********	0
6 (S-TI%)	25	(S-SC)	0.5617	67
6 (S-TI%)	26	(S-SN)	********	0

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COLUMN	VERSUS COLUMN	CORRELATION COEFFICIENT	NO. OF PAIRS
6 (S-TI%)	27 (S-SR)	0.1406	67
6 (S-TI%)	28 (S-V)	0.4873	67
6 (S-TI%)	29 (S-W)	********	0
6 (S-TI%)	30 (S-Y)	0.4618	67
6 (S-TI%)	31 (S-ZN)	0.8149	4
6 (S-TI%)	32 (S-ZR)	0.5698	67
6 (S-TI%)	33 (S-TH)	********	0
6 (S-TI%)	34 (AA-AU-P)	********	1
6 (S-TI%)	35 (AA-AS-P)	-0.1953	67
6 (S-TI%)	36 (AA-ZN-P)	0.0310	67
6 (S-TI%)	37 (AA-SB-P)	0.4336	7
6 (S-TI%)	38 (SI-F)	-0.4315	44
6 (S-TI%)	39 (U-INST)	0.0016	44
7 (S-MN)	8 (S-AG)	0.3885	8
7 (S-MN)	9 (S-AS)	********	0
7 (S-MN)	10 (S-AU)	********	0
7 (S-MN)	11 (S-B)	-0.3179	67
7 (S-MN)	12 (S-BA)	0.4061	67
7 (S-MN)	13 (S-BE)	0.0119	66
7 (S-MN)	14 (S-BI)	********	0
7 (S-MN)	15 (S-CD)	********	0
7 (S-MN)	16 (S-CO)	0.1642	67
7 (S-MN)	17 (S-CR)	-0.0129	67
7 (S-MN)	18 (S-CU)	-0.0820	67
7 (S-MN)	19 (S-LA)	0.2158	67
7 (S-MN)	20 (S-MO)	0.4209	7
7 (S-MN)	21 (S-NB)	********	0
7 (S-MN)	22 (S-NI)	-0.2574	67
7 (S-MN)	23 (S-PB)	0.3455	67
7 (S-MN)	24 (S-SB)	********	0
7 (S-MN)	25 (S-SC)	0.0275	67
7 (S-MN)	26 (S-SN)	********	0
7 (S-MN)	27 (S-SR)	0.0324	67
7 (S-MN)	28 (S-V)	0.2445	67
7 (S-MN)	29 (S-W)	********	0
7 (S-MN)	30 (S-Y)	0.1634	67
7 (S-MN)	31 (S-ZN)	0.1051	4
7 (S-MN)	32 (S-ZR)	0.3435	67
7 (S-MN)	33 (S-TH)	********	0
7 (S-MN)	34 (AA-AU-P)	********	1
7 (S-MN)	35 (AA-AS-P)	0.1111	67
7 (S-MN)	36 (AA-ZN-P)	0.5251	67
7 (S-MN)	37 (AA-SB-P)	0.7520	7
7 (S-MN)	38 (SI-F)	-0.3883	44
7 (S-MN)	39 (U-INST)	-0.1741	44
8 (S-AG)	9 (S-AS)	********	0
8 (S-AG)	10 (S-AU)	********	0
8 (S-AG)	11 (S-B)	0.0814	8
8 (S-AG)	12 (S-BA)	-0.1512	8
8 (S-AG)	13 (S-BE)	0.1041	8

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COLUMN	VERSUS	COLUMN	CORRELATION COEFFICIENT	NO. OF PAIRS
8 (S-AG)	14	(S-BI)	********	0
8 (S-AG)	15	(S-CD)	********	0
8 (S-AG)	16	(S-CO)	0.6080	8
8 (S-AG)	17	(S-CR)	0.0043	8
8 (S-AG)	18	(S-CU)	0.4267	8
8 (S-AG)	19	(S-LA)	0.0812	8
8 (S-AG)	20	(S-MO)	-1.0000	2
8 (S-AG)	21	(S-NB)	********	0
8 (S-AG)	22	(S-NI)	-0.1286	8
8 (S-AG)	23	(S-PB)	0.1384	8
8 (S-AG)	24	(S-SB)	********	0
8 (S-AG)	25	(S-SC)	0.4285	8
8 (S-AG)	26	(S-SN)	********	0
8 (S-AG)	27	(S-SR)	-0.4862	8
8 (S-AG)	28	(S-V)	0.4127	8
8 (S-AG)	29	(S-W)	********	0
8 (S-AG)	30	(S-Y)	0.3340	8
8 (S-AG)	31	(S-ZN)	********	1
8 (S-AG)	32	(S-ZR)	0.0669	8
8 (S-AG)	33	(S-TH)	********	0
8 (S-AG)	34	(AA-AU-P)	********	0
8 (S-AG)	35	(AA-AS-P)	-0.2021	8
8 (S-AG)	36	(AA-ZN-P)	-0.1474	8
8 (S-AG)	37	(AA-SB-P)	0.8749	5
8 (S-AG)	38	(SI-F)	-0.4948	8
8 (S-AG)	39	(U-INST)	0.1922	8
9 (S-AS)	10	(S-AU)	********	0
9 (S-AS)	11	(S-B)	********	0
9 (S-AS)	12	(S-BA)	********	0
9 (S-AS)	13	(S-BE)	********	0
9 (S-AS)	14	(S-BI)	********	0
9 (S-AS)	15	(S-CD)	********	0
9 (S-AS)	16	(S-CO)	********	0
9 (S-AS)	17	(S-CR)	********	0
9 (S-AS)	18	(S-CU)	********	0
9 (S-AS)	19	(S-LA)	********	0
9 (S-AS)	20	(S-MO)	********	0
9 (S-AS)	21	(S-NB)	********	0
9 (S-AS)	22	(S-NI)	********	0
9 (S-AS)	23	(S-PB)	********	0
9 (S-AS)	24	(S-SB)	********	0
9 (S-AS)	25	(S-SC)	********	0
9 (S-AS)	26	(S-SN)	********	0
9 (S-AS)	27	(S-SR)	********	0
9 (S-AS)	28	(S-V)	********	0
9 (S-AS)	29	(S-W)	********	0
9 (S-AS)	30	(S-Y)	********	0
9 (S-AS)	31	(S-ZN)	********	0
9 (S-AS)	32	(S-ZR)	********	0
9 (S-AS)	33	(S-TH)	********	0

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COLUMN	VERSUS COLUMN	CORRELATION COEFFICIENT	NO. OF PAIRS
9 (S-AS)	34 (AA-AU-P)	********	0
9 (S-AS)	35 (AA-AS-P)	********	0
9 (S-AS)	36 (AA-ZN-P)	********	0
9 (S-AS)	37 (AA-SB-P)	********	0
9 (S-AS)	38 (SI-F)	********	0
9 (S-AS)	39 (U-INST)	********	0
10 (S-AU)	11 (S-B)	********	0
10 (S-AU)	12 (S-BA)	********	0
10 (S-AU)	13 (S-BE)	********	0
10 (S-AU)	14 (S-BI)	********	0
10 (S-AU)	15 (S-CD)	********	0
10 (S-AU)	16 (S-CO)	********	0
10 (S-AU)	17 (S-CR)	********	0
10 (S-AU)	18 (S-CU)	********	0
10 (S-AU)	19 (S-LA)	********	0
10 (S-AU)	20 (S-MO)	********	0
10 (S-AU)	21 (S-NB)	********	0
10 (S-AU)	22 (S-NI)	********	0
10 (S-AU)	23 (S-PB)	********	0
10 (S-AU)	24 (S-SB)	********	0
10 (S-AU)	25 (S-SC)	********	0
10 (S-AU)	26 (S-SN)	********	0
10 (S-AU)	27 (S-SR)	********	0
10 (S-AU)	28 (S-V)	********	0
10 (S-AU)	29 (S-W)	********	0
10 (S-AU)	30 (S-Y)	********	0
10 (S-AU)	31 (S-ZN)	********	0
10 (S-AU)	32 (S-ZR)	********	0
10 (S-AU)	33 (S-TH)	********	0
10 (S-AU)	34 (AA-AU-P)	********	0
10 (S-AU)	35 (AA-AS-P)	********	0
10 (S-AU)	36 (AA-ZN-P)	********	0
10 (S-AU)	37 (AA-SB-P)	********	0
10 (S-AU)	38 (SI-F)	********	0
10 (S-AU)	39 (U-INST)	********	0
11 (S-B)	12 (S-BA)	-0.2946	67
11 (S-B)	13 (S-BE)	0.1802	66
11 (S-B)	14 (S-BI)	********	0
11 (S-B)	15 (S-CD)	********	0
11 (S-B)	16 (S-CO)	0.0047	67
11 (S-B)	17 (S-CR)	-0.0335	67
11 (S-B)	18 (S-CU)	0.2329	67
11 (S-B)	19 (S-LA)	0.1505	67
11 (S-B)	20 (S-MO)	-0.4547	7
11 (S-B)	21 (S-NB)	********	0
11 (S-B)	22 (S-NI)	0.2193	67
11 (S-B)	23 (S-PB)	-0.0564	67
11 (S-B)	24 (S-SB)	********	0
11 (S-B)	25 (S-SC)	-0.1394	67
11 (S-B)	26 (S-SN)	********	0

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COLUMN	VERSUS	COLUMN	CORRELATION COEFFICIENT	NO. OF PAIRS
11 (S-B)	27	(S-SR)	-0.0509	67
11 (S-B)	28	(S-V)	-0.2819	67
11 (S-B)	29	(S-W)	********	0
11 (S-B)	30	(S-Y)	0.0287	67
11 (S-B)	31	(S-ZN)	-0.5774	4
11 (S-B)	32	(S-ZR)	-0.2867	67
11 (S-B)	33	(S-TH)	********	0
11 (S-B)	34	(AA-AU-P)	********	1
11 (S-B)	35	(AA-AS-P)	0.5128	67
11 (S-B)	36	(AA-ZN-P)	-0.0567	67
11 (S-B)	37	(AA-SB-P)	-0.2215	7
11 (S-B)	38	(SI-F)	0.6000	44
11 (S-B)	39	(U-INST)	0.2020	44
12 (S-BA)	13	(S-BE)	-0.2019	66
12 (S-BA)	14	(S-BI)	********	0
12 (S-BA)	15	(S-CD)	********	0
12 (S-BA)	16	(S-CO)	-0.1940	67
12 (S-BA)	17	(S-CR)	-0.2213	67
12 (S-BA)	18	(S-CU)	-0.3493	67
12 (S-BA)	19	(S-LA)	0.1041	67
12 (S-BA)	20	(S-MO)	0.6892	7
12 (S-BA)	21	(S-NB)	********	0
12 (S-BA)	22	(S-NI)	-0.4734	67
12 (S-BA)	23	(S-PB)	0.3139	67
12 (S-BA)	24	(S-SB)	********	0
12 (S-BA)	25	(S-SC)	0.0111	67
12 (S-BA)	26	(S-SN)	********	0
12 (S-BA)	27	(S-SR)	0.3081	67
12 (S-BA)	28	(S-V)	0.0093	67
12 (S-BA)	29	(S-W)	********	0
12 (S-BA)	30	(S-Y)	-0.0767	67
12 (S-BA)	31	(S-ZN)	-0.0661	4
12 (S-BA)	32	(S-ZR)	0.3709	67
12 (S-BA)	33	(S-TH)	********	0
12 (S-BA)	34	(AA-AU-P)	********	1
12 (S-BA)	35	(AA-AS-P)	0.1128	67
12 (S-BA)	36	(AA-ZN-P)	0.1393	67
12 (S-BA)	37	(AA-SB-P)	0.5072	7
12 (S-BA)	38	(SI-F)	-0.3018	44
12 (S-BA)	39	(U-INST)	-0.3103	44
13 (S-BE)	14	(S-BI)	********	0
13 (S-BE)	15	(S-CD)	********	0
13 (S-BE)	16	(S-CO)	-0.1398	66
13 (S-BE)	17	(S-CR)	-0.1122	66
13 (S-BE)	18	(S-CU)	0.0428	66
13 (S-BE)	19	(S-LA)	-0.0626	66
13 (S-BE)	20	(S-MO)	-0.6455	7
13 (S-BE)	21	(S-NB)	********	0
13 (S-BE)	22	(S-NI)	0.0038	66
13 (S-BE)	23	(S-PB)	0.0816	66

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COLUMN	VERSUS	COLUMN	CORRELATION COEFFICIENT	NO. OF PAIRS
13 (S-BE)	24	(S-SB)	********	0
13 (S-BE)	25	(S-SC)	-0.1492	66
13 (S-BE)	26	(S-SN)	********	0
13 (S-BE)	27	(S-SR)	-0.3865	66
13 (S-BE)	28	(S-V)	-0.1605	66
13 (S-BE)	29	(S-W)	********	0
13 (S-BE)	30	(S-Y)	0.0785	66
13 (S-BE)	31	(S-ZN)	-0.5774	4
13 (S-BE)	32	(S-ZR)	0.0012	66
13 (S-BE)	33	(S-TH)	********	0
13 (S-BE)	34	(AA-AU-P)	********	1
13 (S-BE)	35	(AA-AS-P)	0.1287	66
13 (S-BE)	36	(AA-ZN-P)	0.0355	66
13 (S-BE)	37	(AA-SB-P)	0.0055	7
13 (S-BE)	38	(SI-F)	0.0275	44
13 (S-BE)	39	(U-INST)	-0.3313	44
14 (S-BI)	15	(S-CD)	********	0
14 (S-BI)	16	(S-CO)	********	0
14 (S-BI)	17	(S-CR)	********	0
14 (S-BI)	18	(S-CU)	********	0
14 (S-BI)	19	(S-LA)	********	0
14 (S-BI)	20	(S-MO)	********	0
14 (S-BI)	21	(S-NB)	********	0
14 (S-BI)	22	(S-NI)	********	0
14 (S-BI)	23	(S-PB)	********	0
14 (S-BI)	24	(S-SB)	********	0
14 (S-BI)	25	(S-SC)	********	0
14 (S-BI)	26	(S-SN)	********	0
14 (S-BI)	27	(S-SR)	********	0
14 (S-BI)	28	(S-V)	********	0
14 (S-BI)	29	(S-W)	********	0
14 (S-BI)	30	(S-Y)	********	0
14 (S-BI)	31	(S-ZN)	********	0
14 (S-BI)	32	(S-ZR)	********	0
14 (S-BI)	33	(S-TH)	********	0
14 (S-BI)	34	(AA-AU-P)	********	0
14 (S-BI)	35	(AA-AS-P)	********	0
14 (S-BI)	36	(AA-ZN-P)	********	0
14 (S-BI)	37	(AA-SB-P)	********	0
14 (S-BI)	38	(SI-F)	********	0
14 (S-BI)	39	(U-INST)	********	0
15 (S-CD)	16	(S-CO)	********	0
15 (S-CD)	17	(S-CR)	********	0
15 (S-CD)	18	(S-CU)	********	0
15 (S-CD)	19	(S-LA)	********	0
15 (S-CD)	20	(S-MO)	********	0
15 (S-CD)	21	(S-NB)	********	0
15 (S-CD)	22	(S-NI)	********	0
15 (S-CD)	23	(S-PB)	********	0
15 (S-CD)	24	(S-SB)	********	0

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COLUMN	VERSUS COLUMN	CORRELATION COEFFICIENT	NO. OF PAIRS
15 (S-CD)	25 (S-SC)	********	0
15 (S-CD)	26 (S-SN)	********	0
15 (S-CD)	27 (S-SR)	********	0
15 (S-CD)	28 (S-V)	********	0
15 (S-CD)	29 (S-W)	********	0
15 (S-CD)	30 (S-Y)	********	0
15 (S-CD)	31 (S-ZN)	********	0
15 (S-CD)	32 (S-ZR)	********	0
15 (S-CD)	33 (S-TH)	********	0
15 (S-CD)	34 (AA-AU-P)	********	0
15 (S-CD)	35 (AA-AS-P)	********	0
15 (S-CD)	36 (AA-ZN-P)	********	0
15 (S-CD)	37 (AA-SB-P)	********	0
15 (S-CD)	38 (SI-F)	********	0
15 (S-CD)	39 (U-INST)	********	0
16 (S-CO)	17 (S-CR)	0.6967	67
16 (S-CO)	18 (S-CU)	0.6123	67
16 (S-CO)	19 (S-LA)	0.1478	67
16 (S-CO)	20 (S-MO)	-0.2940	7
16 (S-CO)	21 (S-NB)	********	0
16 (S-CO)	22 (S-NI)	0.5818	67
16 (S-CO)	23 (S-PB)	-0.0995	67
16 (S-CO)	24 (S-SB)	********	0
16 (S-CO)	25 (S-SC)	0.6195	67
16 (S-CO)	26 (S-SN)	********	0
16 (S-CO)	27 (S-SR)	-0.1073	67
16 (S-CO)	28 (S-V)	0.6138	67
16 (S-CO)	29 (S-W)	********	0
16 (S-CO)	30 (S-Y)	0.3370	67
16 (S-CO)	31 (S-ZN)	0.9105	4
16 (S-CO)	32 (S-ZR)	0.0210	67
16 (S-CO)	33 (S-TH)	********	0
16 (S-CO)	34 (AA-AU-P)	********	1
16 (S-CO)	35 (AA-AS-P)	0.2170	67
16 (S-CO)	36 (AA-ZN-P)	0.4544	67
16 (S-CO)	37 (AA-SB-P)	0.6845	7
16 (S-CO)	38 (SI-F)	0.1484	44
16 (S-CO)	39 (U-INST)	0.4000	44
17 (S-CR)	18 (S-CU)	0.5246	67
17 (S-CR)	19 (S-LA)	0.1763	67
17 (S-CR)	20 (S-MO)	-0.1704	7
17 (S-CR)	21 (S-NB)	********	0
17 (S-CR)	22 (S-NI)	0.6398	67
17 (S-CR)	23 (S-PB)	-0.3558	67
17 (S-CR)	24 (S-SB)	********	0
17 (S-CR)	25 (S-SC)	0.5335	67
17 (S-CR)	26 (S-SN)	********	0
17 (S-CR)	27 (S-SR)	-0.0917	67
17 (S-CR)	28 (S-V)	0.5299	67
17 (S-CR)	29 (S-W)	********	0

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COLUMN	VERSUS	COLUMN	CORRELATION COEFFICIENT	NO. OF PAIRS
17 (S-CR)	30	(S-Y)	0.1416	67
17 (S-CR)	31	(S-ZN)	0.4867	4
17 (S-CR)	32	(S-ZR)	-0.1073	67
17 (S-CR)	33	(S-TH)	********	0
17 (S-CR)	34	(AA-AU-P)	********	1
17 (S-CR)	35	(AA-AS-P)	0.0954	67
17 (S-CR)	36	(AA-ZN-P)	0.3523	67
17 (S-CR)	37	(AA-SB-P)	-0.4020	7
17 (S-CR)	38	(SI-F)	0.1309	44
17 (S-CR)	39	(U-INST)	0.5446	44
18 (S-CU)	19	(S-LA)	0.1240	67
18 (S-CU)	20	(S-MO)	-0.2989	7
18 (S-CU)	21	(S-NB)	********	0
18 (S-CU)	22	(S-NI)	0.7879	67
18 (S-CU)	23	(S-PB)	0.0098	67
18 (S-CU)	24	(S-SB)	********	0
18 (S-CU)	25	(S-SC)	0.3028	67
18 (S-CU)	26	(S-SN)	********	0
18 (S-CU)	27	(S-SR)	-0.2986	67
18 (S-CU)	28	(S-V)	0.4917	67
18 (S-CU)	29	(S-W)	********	0
18 (S-CU)	30	(S-Y)	0.4107	67
18 (S-CU)	31	(S-ZN)	0.4062	4
18 (S-CU)	32	(S-ZR)	-0.2969	67
18 (S-CU)	33	(S-TH)	********	0
18 (S-CU)	34	(AA-AU-P)	********	1
18 (S-CU)	35	(AA-AS-P)	0.3216	67
18 (S-CU)	36	(AA-ZN-P)	0.5142	67
18 (S-CU)	37	(AA-SB-P)	0.6845	7
18 (S-CU)	38	(SI-F)	0.4265	44
18 (S-CU)	39	(U-INST)	0.5642	44
19 (S-LA)	20	(S-MO)	-0.0055	7
19 (S-LA)	21	(S-NB)	********	0
19 (S-LA)	22	(S-NI)	0.0422	67
19 (S-LA)	23	(S-PB)	0.0813	67
19 (S-LA)	24	(S-SB)	********	0
19 (S-LA)	25	(S-SC)	0.3222	67
19 (S-LA)	26	(S-SN)	********	0
19 (S-LA)	27	(S-SR)	0.1720	67
19 (S-LA)	28	(S-V)	0.3487	67
19 (S-LA)	29	(S-W)	********	0
19 (S-LA)	30	(S-Y)	0.4930	67
19 (S-LA)	31	(S-ZN)	0.3657	4
19 (S-LA)	32	(S-ZR)	0.2433	67
19 (S-LA)	33	(S-TH)	********	0
19 (S-LA)	34	(AA-AU-P)	********	1
19 (S-LA)	35	(AA-AS-P)	-0.0011	67
19 (S-LA)	36	(AA-ZN-P)	0.2075	67
19 (S-LA)	37	(AA-SB-P)	-0.0116	7
19 (S-LA)	38	(SI-F)	-0.0723	44

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COLUMN	VERSUS	COLUMN	CORRELATION COEFFICIENT	NO. OF PAIRS
19 (S-LA)	39	(U-INST)	0.3055	44
20 (S-MO)	21	(S-NB)	********	0
20 (S-MO)	22	(S-NI)	-0.2360	7
20 (S-MO)	23	(S-PB)	0.4362	7
20 (S-MO)	24	(S-SB)	********	0
20 (S-MO)	25	(S-SC)	-0.5401	7
20 (S-MO)	26	(S-SN)	********	0
20 (S-MO)	27	(S-SR)	0.6455	7
20 (S-MO)	28	(S-V)	-0.0891	7
20 (S-MO)	29	(S-W)	********	0
20 (S-MO)	30	(S-Y)	-0.3881	7
20 (S-MO)	31	(S-ZN)	********	2
20 (S-MO)	32	(S-ZR)	0.6608	7
20 (S-MO)	33	(S-TH)	********	0
20 (S-MO)	34	(AA-AU-P)	********	0
20 (S-MO)	35	(AA-AS-P)	0.8049	7
20 (S-MO)	36	(AA-ZN-P)	0.2550	7
20 (S-MO)	37	(AA-SB-P)	-1.0000	2
20 (S-MO)	38	(SI-F)	-0.0591	7
20 (S-MO)	39	(U-INST)	-0.3151	7
21 (S-NB)	22	(S-NI)	********	0
21 (S-NB)	23	(S-PB)	********	0
21 (S-NB)	24	(S-SB)	********	0
21 (S-NB)	25	(S-SC)	********	0
21 (S-NB)	26	(S-SN)	********	0
21 (S-NB)	27	(S-SR)	********	0
21 (S-NB)	28	(S-V)	********	0
21 (S-NB)	29	(S-W)	********	0
21 (S-NB)	30	(S-Y)	********	0
21 (S-NB)	31	(S-ZN)	********	0
21 (S-NB)	32	(S-ZR)	********	0
21 (S-NB)	33	(S-TH)	********	0
21 (S-NB)	34	(AA-AU-P)	********	0
21 (S-NB)	35	(AA-AS-P)	********	0
21 (S-NB)	36	(AA-ZN-P)	********	0
21 (S-NB)	37	(AA-SB-P)	********	0
21 (S-NB)	38	(SI-F)	********	0
21 (S-NB)	39	(U-INST)	********	0
22 (S-NI)	23	(S-PB)	-0.0763	67
22 (S-NI)	24	(S-SB)	********	0
22 (S-NI)	25	(S-SC)	0.2817	67
22 (S-NI)	26	(S-SN)	********	0
22 (S-NI)	27	(S-SR)	-0.4010	67
22 (S-NI)	28	(S-V)	0.4436	67
22 (S-NI)	29	(S-W)	********	0
22 (S-NI)	30	(S-Y)	0.2115	67
22 (S-NI)	31	(S-ZN)	0.0157	4
22 (S-NI)	32	(S-ZR)	-0.3713	67
22 (S-NI)	33	(S-TH)	********	0
22 (S-NI)	34	(AA-AU-P)	********	1

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COLUMN	VERSUS	COLUMN	CORRELATION COEFFICIENT	NO. OF PAIRS
22 (S-NI)	35	(AA-AS-P)	0.2333	67
22 (S-NI)	36	(AA-ZN-P)	0.4017	67
22 (S-NI)	37	(AA-SB-P)	-0.3401	7
22 (S-NI)	38	(SI-F)	0.4658	44
22 (S-NI)	39	(U-INST)	0.5714	44
23 (S-PB)	24	(S-SB)	********	0
23 (S-PB)	25	(S-SC)	-0.1940	67
23 (S-PB)	26	(S-SN)	********	0
23 (S-PB)	27	(S-SR)	-0.1371	67
23 (S-PB)	28	(S-V)	-0.0036	67
23 (S-PB)	29	(S-W)	********	0
23 (S-PB)	30	(S-Y)	0.2452	67
23 (S-PB)	31	(S-ZN)	-0.3806	4
23 (S-PB)	32	(S-ZR)	0.1680	67
23 (S-PB)	33	(S-TH)	********	0
23 (S-PB)	34	(AA-AU-P)	********	1
23 (S-PB)	35	(AA-AS-P)	0.2585	67
23 (S-PB)	36	(AA-ZN-P)	0.4039	67
23 (S-PB)	37	(AA-SB-P)	0.8009	7
23 (S-PB)	38	(SI-F)	0.1589	44
23 (S-PB)	39	(U-INST)	-0.1889	44
24 (S-SB)	25	(S-SC)	********	0
24 (S-SB)	26	(S-SN)	********	0
24 (S-SB)	27	(S-SR)	********	0
24 (S-SB)	28	(S-V)	********	0
24 (S-SB)	29	(S-W)	********	0
24 (S-SB)	30	(S-Y)	********	0
24 (S-SB)	31	(S-ZN)	********	0
24 (S-SB)	32	(S-ZR)	********	0
24 (S-SB)	33	(S-TH)	********	0
24 (S-SB)	34	(AA-AU-P)	********	0
24 (S-SB)	35	(AA-AS-P)	********	0
24 (S-SB)	36	(AA-ZN-P)	********	0
24 (S-SB)	37	(AA-SB-P)	********	0
24 (S-SB)	38	(SI-F)	********	0
24 (S-SB)	39	(U-INST)	********	0
25 (S-SC)	26	(S-SN)	********	0
25 (S-SC)	27	(S-SR)	0.1079	67
25 (S-SC)	28	(S-V)	0.5126	67
25 (S-SC)	29	(S-W)	********	0
25 (S-SC)	30	(S-Y)	0.4198	67
25 (S-SC)	31	(S-ZN)	0.1414	4
25 (S-SC)	32	(S-ZR)	0.2490	67
25 (S-SC)	33	(S-TH)	********	0
25 (S-SC)	34	(AA-AU-P)	********	1
25 (S-SC)	35	(AA-AS-P)	-0.0520	67
25 (S-SC)	36	(AA-ZN-P)	0.2031	67
25 (S-SC)	37	(AA-SB-P)	0.3401	7
25 (S-SC)	38	(SI-F)	-0.1818	44
25 (S-SC)	39	(U-INST)	0.2372	44

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COLUMN	VERSUS	COLUMN	CORRELATION COEFFICIENT	NO. OF PAIRS
26 (S-SN)	27	(S-SR)	********	0
26 (S-SN)	28	(S-V)	********	0
26 (S-SN)	29	(S-W)	********	0
26 (S-SN)	30	(S-Y)	********	0
26 (S-SN)	31	(S-ZN)	********	0
26 (S-SN)	32	(S-ZR)	********	0
26 (S-SN)	33	(S-TH)	********	0
26 (S-SN)	34	(AA-AU-P)	********	0
26 (S-SN)	35	(AA-AS-P)	********	0
26 (S-SN)	36	(AA-ZN-P)	********	0
26 (S-SN)	37	(AA-SB-P)	********	0
26 (S-SN)	38	(SI-F)	********	0
26 (S-SN)	39	(U-INST)	********	0
27 (S-SR)	28	(S-V)	0.0515	67
27 (S-SR)	29	(S-W)	********	0
27 (S-SR)	30	(S-Y)	-0.0760	67
27 (S-SR)	31	(S-ZN)	0.5774	4
27 (S-SR)	32	(S-ZR)	0.1134	67
27 (S-SR)	33	(S-TH)	********	0
27 (S-SR)	34	(AA-AU-P)	********	1
27 (S-SR)	35	(AA-AS-P)	-0.2141	67
27 (S-SR)	36	(AA-ZN-P)	-0.1583	67
27 (S-SR)	37	(AA-SB-P)	-0.3144	7
27 (S-SR)	38	(SI-F)	-0.4522	44
27 (S-SR)	39	(U-INST)	0.0124	44
28 (S-V)	29	(S-W)	********	0
28 (S-V)	30	(S-Y)	0.4741	67
28 (S-V)	31	(S-ZN)	0.4495	4
28 (S-V)	32	(S-ZR)	0.2029	67
28 (S-V)	33	(S-TH)	********	0
28 (S-V)	34	(AA-AU-P)	********	1
28 (S-V)	35	(AA-AS-P)	-0.0222	67
28 (S-V)	36	(AA-ZN-P)	0.4958	67
28 (S-V)	37	(AA-SB-P)	0.6907	7
28 (S-V)	38	(SI-F)	-0.1146	44
28 (S-V)	39	(U-INST)	0.3607	44
29 (S-W)	30	(S-Y)	********	0
29 (S-W)	31	(S-ZN)	********	0
29 (S-W)	32	(S-ZR)	********	0
29 (S-W)	33	(S-TH)	********	0
29 (S-W)	34	(AA-AU-P)	********	0
29 (S-W)	35	(AA-AS-P)	********	0
29 (S-W)	36	(AA-ZN-P)	********	0
29 (S-W)	37	(AA-SB-P)	********	0
29 (S-W)	38	(SI-F)	********	0
29 (S-W)	39	(U-INST)	********	0
30 (S-Y)	31	(S-ZN)	1.0000	4
30 (S-Y)	32	(S-ZR)	0.2945	67
30 (S-Y)	33	(S-TH)	********	0
30 (S-Y)	34	(AA-AU-P)	********	1

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COLUMN	VERSUS	COLUMN	CORRELATION COEFFICIENT	NO. OF PAIRS
30 (S-Y)	35	(AA-AS-P)	-0.1018	67
30 (S-Y)	36	(AA-ZN-P)	0.2320	67
30 (S-Y)	37	(AA-SB-P)	0.0055	7
30 (S-Y)	38	(SI-F)	-0.1453	44
30 (S-Y)	39	(U-INST)	0.2221	44
31 (S-ZN)	32	(S-ZR)	0.4984	4
31 (S-ZN)	33	(S-TH)	********	0
31 (S-ZN)	34	(AA-AU-P)	********	0
31 (S-ZN)	35	(AA-AS-P)	-0.5348	4
31 (S-ZN)	36	(AA-ZN-P)	0.5531	4
31 (S-ZN)	37	(AA-SB-P)	********	1
31 (S-ZN)	38	(SI-F)	-0.5274	4
31 (S-ZN)	39	(U-INST)	0.4439	4
32 (S-ZR)	33	(S-TH)	********	0
32 (S-ZR)	34	(AA-AU-P)	********	1
32 (S-ZR)	35	(AA-AS-P)	-0.0454	67
32 (S-ZR)	36	(AA-ZN-P)	-0.0161	67
32 (S-ZR)	37	(AA-SB-P)	0.0665	7
32 (S-ZR)	38	(SI-F)	-0.4128	44
32 (S-ZR)	39	(U-INST)	-0.3712	44
33 (S-TH)	34	(AA-AU-P)	********	0
33 (S-TH)	35	(AA-AS-P)	********	0
33 (S-TH)	36	(AA-ZN-P)	********	0
33 (S-TH)	37	(AA-SB-P)	********	0
33 (S-TH)	38	(SI-F)	********	0
33 (S-TH)	39	(U-INST)	********	0
34 (AA-AU-P)	35	(AA-AS-P)	********	1
34 (AA-AU-P)	36	(AA-ZN-P)	********	1
34 (AA-AU-P)	37	(AA-SB-P)	********	0
34 (AA-AU-P)	38	(SI-F)	********	1
34 (AA-AU-P)	39	(U-INST)	********	1
35 (AA-AS-P)	36	(AA-ZN-P)	0.4676	67
35 (AA-AS-P)	37	(AA-SB-P)	0.3937	7
35 (AA-AS-P)	38	(SI-F)	0.4941	44
35 (AA-AS-P)	39	(U-INST)	-0.0012	44
36 (AA-ZN-P)	37	(AA-SB-P)	0.4836	7
36 (AA-ZN-P)	38	(SI-F)	0.1143	44
36 (AA-ZN-P)	39	(U-INST)	0.2454	44
37 (AA-SB-P)	38	(SI-F)	-0.0873	6
37 (AA-SB-P)	39	(U-INST)	-0.1800	6
38 (SI-F)	39	(U-INST)	0.1929	44

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TITLE	INPUT ID		N	M	***** OPTIONS *****	OUTPUT ID		N	M
	-ds-5	-	67	34	1 0 1 1 0 0 0 0 0 0	-	-	34	34

NUMBER OF SELECTED COLUMNS 34

SELECTED COLUMN INDICES

1	2	3	4	5	6	7	8	9	10
11	12	13	14	15	16	17	18	19	20
21	22	23	24	25	26	27	28	29	30
31	32	33	34						

SELECTED COLUMN IDENTIFIERS

X-COORD.	Y-COORD.	S-FE%	S-MG%	S-CA%	S-TI%	S-MN	S-AG	S-AS	S-AU
S-B	S-BA	S-BE	S-BI	S-CD	S-CO	S-CR	S-CU	S-LA	S-MO
S-NB	S-NI	S-PB	S-SB	S-SC	S-SN	S-SR	S-V	S-W	S-Y
S-ZN	S-ZR	S-TH	INST-HG						

NUMBER OF SELECTED ROW PAIRS 1

SELECTED ROW PAIRS
1- 67

P H A S E T W O R E S U L T S

W A R N I N G * * * THE RESULTS FROM THIS PHASE "SHOULD NOT" BE ENTERED INTO D0096-FACTOR ANALYSIS.
THE CORRELATION MATRIX FROM THIS PHASE DOES NOT HAVE THE GRAMIAN PROPERTIES
WHICH ARE REQUIRED FOR FACTOR ANALYSIS.

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ARRAY OF MEANS -

		1 X-COORD.	2 Y-COORD.	3 S-FE%	4 S-MG%	5 S-CA%	6 S-TI%	7 S-MN	8 S-AG	9 S-AS	10 S-AU
1	X-COORD.	4.6223	4.6223	4.6223	4.6223	4.6223	4.6233	4.6223	4.6250	4.6293	**********
2	Y-COORD.	5.6208	5.6208	5.6208	5.6208	5.6208	5.6208	5.6208	5.6210	5.6211	**********
3	S-FE%	-0.1373	-0.1373	-0.1373	-0.1373	-0.1373	-0.1110	-0.1373	-0.1869	-0.2280	**********
4	S-MG%	-0.3996	-0.3996	-0.3996	-0.3996	-0.3996	-0.3891	-0.3996	-0.5150	-1.0000	**********
5	S-CA%	0.7747	0.7747	0.7747	0.7747	0.7747	0.7607	0.7747	0.6343	0.3010	**********
6	S-TI%	0.0315	0.0315	0.0315	0.0315	0.0315	0.0315	0.0315	0.0453	-0.3389	**********
7	S-MN	2.5659	2.5659	2.5659	2.5659	2.5659	2.5734	2.5659	2.5599	2.5880	**********
8	S-AG	0.8218	0.8218	0.8218	0.8218	0.8218	0.8218	0.8218	0.8218	0.9225	**********
9	S-AS	2.7720	2.7720	2.7720	2.7720	2.7720	2.7720	2.7720	2.7720	2.7720	**********
10	S-AU	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
11	S-B	1.5932	1.5932	1.5932	1.5932	1.5932	1.5958	1.5932	1.5556	1.3010	**********
12	S-BA	3.0996	3.0996	3.0996	3.0996	3.0996	3.0237	3.0996	3.1633	**********	**********
13	S-BE	0.3451	0.3451	0.3451	0.3451	0.3451	0.3451	0.3451	0.4771	0.4771	**********
14	S-BI	2.0000	2.0000	2.0000	2.0000	2.0000	2.0000	2.0000	2.0000	**********	**********
15	S-CD	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
16	S-CO	1.1396	1.1396	1.1396	1.1396	1.1396	1.2755	1.1396	1.0000	**********	**********
17	S-CR	1.6406	1.6406	1.6406	1.6406	1.6406	1.5903	1.6406	1.5566	1.3010	**********
18	S-CU	1.5030	1.5030	1.5030	1.5030	1.5030	1.5233	1.5030	1.8380	1.1761	**********
19	S-LA	2.3422	2.3422	2.3422	2.3422	2.3422	2.2988	2.3422	2.2070	1.8495	**********
20	S-MO	1.1424	1.1424	1.1424	1.1424	1.1424	1.1529	1.1424	1.1761	**********	**********
21	S-NB	1.7463	1.7463	1.7463	1.7463	1.7463	1.7233	1.7463	1.7477	**********	**********
22	S-NI	1.1824	1.1824	1.1824	1.1824	1.1824	1.1959	1.1824	1.1505	**********	**********
23	S-PB	1.9397	1.9397	1.9397	1.9397	1.9397	1.8913	1.9397	2.5181	3.3266	**********
24	S-SB	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
25	S-SC	1.2981	1.2981	1.2981	1.2981	1.2981	1.2197	1.2981	1.3195	1.0000	**********
26	S-SN	2.1496	2.1496	2.1496	2.1496	2.1496	2.4824	2.1496	3.3010	**********	**********
27	S-SR	2.8033	2.8033	2.8033	2.8033	2.8033	2.8351	2.8033	2.9650	3.3266	**********
28	S-V	1.8478	1.8478	1.8478	1.8478	1.8478	1.8203	1.8478	1.8131	1.5880	**********
29	S-W	2.8758	2.8758	2.8758	2.8758	2.8758	3.0880	2.8758	3.5880	**********	**********
30	S-Y	2.2161	2.2161	2.2161	2.2161	2.2161	2.1583	2.2161	2.1289	1.7386	**********
31	S-ZN	2.9282	2.9282	2.9282	2.9282	2.9282	2.9855	2.9282	2.7477	2.6990	**********
32	S-ZR	3.0607	3.0607	3.0607	3.0607	3.0607	3.0607	3.0607	3.3010	**********	**********
33	S-TH	2.4771	2.4771	2.4771	2.4771	2.4771	2.4771	2.4771	2.4771	**********	**********
34	INST-HG	-0.1636	-0.1636	-0.1636	-0.1636	-0.1636	-0.1853	-0.1636	-0.6109	**********	**********

D0101 CORRELATION ANALYSIS - USGS STATPAC (01/15/82) DATE 8/10/84

ARRAY OF MEANS - CONT.

		11 S-B	12 S-BA	13 S-BE	14 S-BI	15 S-CD	16 S-CO	17 S-CR	18 S-CU	19 S-LA	20 S-MO
1	X-COORD.	4.6190	4.6223	4.6259	4.6136	**********	4.6174	4.6213	4.6191	4.6223	4.6217
2	Y-COORD.	5.6208	5.6206	5.6203	5.6206	**********	5.6209	5.6208	5.6208	5.6208	5.6205
3	S-FE%	-0.0754	-0.1533	-0.0700	-0.4120	**********	-0.0065	-0.1149	-0.0453	-0.1373	-0.1310
4	S-MG%	-0.2373	-0.3282	-0.5555	0.0106	**********	-0.4087	-0.3414	-0.2413	-0.3996	-0.3018
5	S-CA%	0.8963	0.8183	0.7188	0.8266	**********	0.8250	0.8207	0.8931	0.7747	0.9396
6	S-TI%	0.0758	0.0504	-0.4560	0.2386	**********	0.0795	0.0835	0.0424	0.0315	0.0207
7	S-MN	2.6718	2.5759	2.5326	2.3891	**********	2.5921	2.6044	2.6463	2.5659	2.5850
8	S-AG	0.8102	1.0128	0.8451	0.9375	**********	0.8451	0.8343	0.8935	0.8218	1.6990
9	S-AS	2.8451	**********	2.6990	**********	**********	**********	2.8451	2.8451	2.7720	**********
10	S-AU	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
11	S-B	1.5932	1.6097	1.6990	1.7386	**********	1.6100	1.5932	1.5995	1.5932	1.5973
12	S-BA	3.0869	3.0996	2.8257	2.8891	**********	3.2410	3.0708	3.0426	3.0996	3.0245
13	S-BE	0.3010	0.3010	0.3451	**********	**********	**********	0.3010	0.3010	0.3451	0.3010
14	S-BI	2.0000	2.0000	**********	2.0000	**********	**********	2.0000	2.0000	2.0000	2.0000
15	S-CD	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
16	S-CO	1.1954	1.0778	**********	**********	**********	1.1396	1.1396	1.3257	1.1396	1.1590
17	S-CR	1.7683	1.7040	1.8451	1.7720	**********	1.8554	1.6406	1.7105	1.6406	1.7763
18	S-CU	1.6310	1.6126	1.6990	2.5000	**********	1.6960	1.5349	1.5030	1.5030	1.6743
19	S-LA	2.3858	2.3332	1.9688	2.1505	**********	2.4950	2.3882	2.3090	2.3422	2.3254
20	S-MO	1.1569	1.1140	1.1761	1.1761	**********	1.0000	1.1507	1.1185	1.1424	1.1424
21	S-NB	1.7622	1.7541	**********	1.7720	**********	1.7875	1.7499	1.7529	1.7463	1.7491
22	S-NI	1.2281	1.1719	1.2386	1.3010	**********	1.3821	1.1846	1.2518	1.1824	1.2167
23	S-PB	2.1941	1.8749	1.9939	2.5000	**********	2.2434	1.9600	2.0975	1.9397	1.8383
24	S-SB	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
25	S-SC	1.3827	1.3188	1.0000	1.4375	**********	1.5282	1.3142	1.2372	1.2981	1.2852
26	S-SN	2.0487	1.8618	**********	**********	**********	2.2007	2.1496	2.4225	2.1496	1.6505
27	S-SR	2.6621	2.6088	3.1761	2.5880	**********	2.6930	2.7731	2.8535	2.8033	2.6856
28	S-V	1.9713	1.8904	1.5638	2.0106	**********	2.0030	1.8975	1.9425	1.8478	1.8861
29	S-W	3.0217	3.0217	**********	3.5880	**********	2.6945	2.8758	2.9659	2.8758	3.1590
30	S-Y	2.3155	2.2303	1.5806	2.2386	**********	2.4451	2.2819	2.2017	2.2161	2.2020
31	S-ZN	3.1990	3.1990	2.6990	**********	**********	2.6990	2.9855	3.1990	2.9282	2.6990
32	S-ZR	3.0438	3.0340	2.8257	3.3010	**********	3.1761	3.0759	3.0438	3.0607	3.2386
33	S-TH	2.4771	2.4771	**********	2.4771	**********	2.4771	2.4771	2.4771	2.4771	**********
34	INST-HG	-0.1233	-0.1304	-0.6198	**********	**********	-0.2398	-0.1390	-0.0494	-0.1636	-0.0242

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ARRAY OF MEANS - CONT.

		21 S-NB	22 S-NI	23 S-PB	24 S-SB	25 S-SC	26 S-SN	27 S-SR	28 S-V	29 S-W	30 S-Y
1	X-COORD.	4.6200	4.6209	4.6225	**********	4.6220	4.6213	4.6230	4.6223	4.6133	4.6223
2	Y-COORD.	5.6208	5.6205	5.6208	**********	5.6209	5.6208	5.6208	5.6208	5.6208	5.6208
3	S-FE%	-0.1656	-0.0401	-0.1288	**********	-0.1314	-0.0651	-0.1367	-0.1373	-0.1690	-0.1373
4	S-MG%	-0.3747	-0.2339	-0.3885	**********	-0.3823	-0.3915	-0.4084	-0.3996	-0.1894	-0.3996
5	S-CA%	0.7998	0.9261	0.7839	**********	0.7832	0.8352	0.7621	0.7747	0.9965	0.7747
6	S-TI%	0.1989	0.0767	0.0315	**********	0.0921	0.1590	0.0361	0.0315	0.1945	0.0315
7	S-MN	2.5450	2.6498	2.5714	**********	2.5729	2.6335	2.5551	2.5659	2.4542	2.5659
8	S-AG	1.1174	1.5880	0.8218	**********	0.8343	0.8451	0.8218	0.8218	0.9375	0.8218
9	S-AS	**********	**********	2.7720	**********	2.8451	**********	2.7720	2.7720	**********	2.7720
10	S-AU	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
11	S-B	1.6225	1.6588	1.5976	**********	1.5965	1.4337	1.6088	1.5932	1.8369	1.5932
12	S-BA	3.1921	3.0002	3.1107	**********	3.1256	3.3253	3.1450	3.0996	3.3612	3.0996
13	S-BE	**********	0.3010	0.3451	**********	0.3010	**********	0.3597	0.3451	**********	0.3451
14	S-BI	2.0000	2.0000	2.0000	**********	2.0000	**********	2.0000	2.0000	2.0000	2.0000
15	S-CD	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
16	S-CO	1.1477	1.2792	1.1629	**********	1.1503	1.0000	1.1954	1.1396	1.1193	1.1396
17	S-CR	1.7632	1.7589	1.6358	**********	1.6475	1.6627	1.6178	1.6406	1.9905	1.6406
18	S-CU	1.6642	1.6056	1.5030	**********	1.5087	1.1505	1.4964	1.5030	1.9204	1.5030
19	S-LA	2.4790	2.3329	2.3408	**********	2.3952	2.4704	2.3283	2.3422	2.4681	2.3422
20	S-MO	1.1382	1.1526	1.1424	**********	1.1276	1.0000	1.1526	1.1424	1.0587	1.1424
21	S-NB	1.7463	1.7425	1.7386	**********	1.7480	1.8480	1.7459	1.7463	1.7979	1.7463
22	S-NI	1.1473	1.1824	1.1824	**********	1.1870	1.1761	1.1788	1.1824	1.2954	1.1824
23	S-PB	2.0178	1.9339	1.9397	**********	1.9564	2.3409	1.9210	1.9397	2.2918	1.9397
24	S-SB	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
25	S-SC	1.4110	1.2526	1.2832	**********	1.2981	1.4451	1.2598	1.2981	1.5249	1.2981
26	S-SN	1.5340	1.6505	2.1496	**********	2.1496	2.1496	2.3618	2.1496	2.0000	2.1496
27	S-SR	2.6514	2.6464	2.8033	**********	2.8039	2.7188	2.8033	2.8033	2.6678	2.8033
28	S-V	1.9112	1.9310	1.8431	**********	1.8753	1.9088	1.8221	1.8478	1.9870	1.8478
29	S-W	2.8551	2.9908	2.8758	**********	2.8758	2.4771	2.8758	2.8758	2.8758	2.8758
30	S-Y	2.4104	2.2241	2.2080	**********	2.2839	2.4894	2.1901	2.2161	2.3473	2.2161
31	S-ZN	3.1990	3.1990	2.9282	**********	2.9855	2.6990	2.9282	2.9282	3.1990	2.9282
32	S-ZR	3.3010	3.0759	3.0607	**********	3.1113	**********	3.1037	3.0607	3.2386	3.0607
33	S-TH	2.4771	**********	2.4771	**********	2.4771	**********	2.4771	2.4771	2.4771	2.4771
34	INST-HG	-0.2572	-0.1058	-0.1611	**********	-0.1229	-0.5540	-0.1451	-0.1636	0.0898	-0.1636

D0101 CORRELATION ANALYSIS - USGS STATPAC (01/15/82) DATE 8/10/84

ARRAY OF MEANS - CONT.

		31 S-ZN	32 S-ZR	33 S-TH	34 INST-HG
1	X-COORD.	4.6225	4.6189	4.6132	4.6203
2	Y-COORD.	5.6211	5.6202	5.6207	5.6207
3	S-FE%	-0.0577	0.0278	-0.4120	-0.1099
4	S-MG%	-0.6341	0.0033	-0.4894	-0.3532
5	S-CA%	0.8000	1.0057	0.4771	0.8191
6	S-TI%	-0.0114	-0.2113	0.3010	-0.0015
7	S-MN	2.4803	2.6997	2.3891	2.5971
8	S-AG	0.6637	1.6990	0.1761	1.1611
9	S-AS	2.6990	**********	**********	**********
10	S-AU	**********	**********	**********	**********
11	S-B	1.7720	1.6743	1.7386	1.5864
12	S-BA	3.9225	2.6092	3.0731	2.8820
13	S-BE	0.4771	0.3010	**********	0.3010
14	S-BI	**********	2.0000	2.0000	**********
15	S-CD	**********	**********	**********	**********
16	S-CO	1.0000	1.2386	1.0000	1.1470
17	S-CR	1.6611	1.8473	1.7720	1.6805
18	S-CU	1.3010	1.6786	3.3010	1.5429
19	S-LA	2.2954	2.1607	2.3891	2.3531
20	S-MO	1.0000	1.1633	**********	1.2045
21	S-NB	1.8495	1.6990	1.8451	1.7379
22	S-NI	1.0880	1.2975	**********	1.1620
23	S-PB	2.6965	1.9775	2.3010	1.9195
24	S-SB	**********	**********	**********	**********
25	S-SC	1.3891	1.1306	1.6990	1.3001
26	S-SN	2.6505	**********	**********	2.3010
27	S-SR	2.9793	2.6538	2.6990	2.7649
28	S-V	1.7733	1.9386	1.9225	1.9013
29	S-W	2.3266	3.5000	3.1761	2.6505
30	S-Y	2.1010	1.9328	2.3891	2.2317
31	S-ZN	2.9282	**********	**********	2.6990
32	S-ZR	**********	3.0607	**********	3.0217
33	S-TH	**********	**********	2.4771	2.4771
34	INST-HG	-0.5229	-0.1999	-0.6990	-0.1636

D0101 CORRELATION ANALYSIS - USGS STATPAC (01/15/82) DATE 8/10/84

ARRAY OF VARIANCES -

		1 X-COORD.	2 Y-COORD.	3 S-FE%	4 S-MG%	5 S-CA%	6 S-TI%	7 S-MN	8 S-AG	9 S-AS	10 S-AU
1	X-COORD.	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	**********
2	Y-COORD.	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	**********
3	S-FE%	0.074	0.074	0.074	0.074	0.074	0.079	0.074	0.068	0.011	**********
4	S-MG%	0.117	0.117	0.117	0.117	0.117	0.131	0.117	0.144	0.000	**********
5	S-CA%	0.083	0.083	0.083	0.083	0.083	0.082	0.083	0.084	0.000	**********
6	S-TI%	0.062	0.062	0.062	0.062	0.062	0.062	0.062	0.081	0.068	**********
7	S-MN	0.056	0.056	0.056	0.056	0.056	0.061	0.056	0.040	0.025	**********
8	S-AG	0.230	0.230	0.230	0.230	0.230	0.230	0.230	0.230	0.012	**********
9	S-AS	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.011	**********
10	S-AU	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
11	S-B	0.072	0.072	0.072	0.072	0.072	0.076	0.072	0.088	**********	**********
12	S-BA	0.233	0.233	0.233	0.233	0.233	0.205	0.233	0.259	**********	**********
13	S-BE	0.008	0.008	0.008	0.008	0.008	0.008	0.008	**********	**********	**********
14	S-BI	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	**********	**********
15	S-CD	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
16	S-CO	0.110	0.110	0.110	0.110	0.110	0.231	0.110	**********	**********	**********
17	S-CR	0.076	0.076	0.076	0.076	0.076	0.072	0.076	0.031	**********	**********
18	S-CU	0.252	0.252	0.252	0.252	0.252	0.269	0.252	1.012	**********	**********
19	S-LA	0.070	0.070	0.070	0.070	0.070	0.064	0.070	0.110	0.045	**********
20	S-MO	0.021	0.021	0.021	0.021	0.021	0.020	0.021	**********	**********	**********
21	S-NB	0.007	0.007	0.007	0.007	0.007	0.003	0.007	0.007	**********	**********
22	S-NI	0.053	0.053	0.053	0.053	0.053	0.059	0.053	0.045	**********	**********
23	S-PB	0.283	0.283	0.283	0.283	0.283	0.289	0.283	0.503	0.045	**********
24	S-SB	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
25	S-SC	0.065	0.065	0.065	0.065	0.065	0.038	0.065	0.042	**********	**********
26	S-SN	0.818	0.818	0.818	0.818	0.818	1.099	0.818	**********	**********	**********
27	S-SR	0.162	0.162	0.162	0.162	0.162	0.165	0.162	0.120	0.045	**********
28	S-V	0.058	0.058	0.058	0.058	0.058	0.061	0.058	0.036	0.025	**********
29	S-W	0.494	0.494	0.494	0.494	0.494	0.560	0.494	0.339	**********	**********
30	S-Y	0.105	0.105	0.105	0.105	0.105	0.096	0.105	0.164	0.383	**********
31	S-ZN	0.190	0.190	0.190	0.190	0.190	0.231	0.190	0.007	**********	**********
32	S-ZR	0.097	0.097	0.097	0.097	0.097	0.097	0.097	**********	**********	**********
33	S-TH	0.000	0.000	0.000	0.000	0.000	**********	0.000	**********	**********	**********
34	INST-HG	0.196	0.196	0.196	0.196	0.196	0.196	0.196	0.016	**********	**********

D0101 CORRELATION ANALYSIS - USGS STATPAC (01/15/82) DATE 8/10/84

ARRAY OF VARIANCES - CONT.

		11 S-B	12 S-BA	13 S-BE	14 S-BI	15 S-CD	16 S-CO	17 S-CR	18 S-CU	19 S-LA	20 S-MO
1	X-COORD.	0.000	0.000	0.000	0.000	**********	0.000	0.000	0.000	0.000	0.000
2	Y-COORD.	0.000	0.000	0.000	0.000	**********	0.000	0.000	0.000	0.000	0.000
3	S-FE%	0.116	0.063	0.138	0.025	**********	0.185	0.081	0.101	0.074	0.098
4	S-MG%	0.149	0.118	0.341	0.055	**********	0.132	0.111	0.170	0.117	0.124
5	S-CA%	0.094	0.095	0.128	0.244	**********	0.083	0.078	0.100	0.083	0.065
6	S-TI%	0.034	0.068	0.037	0.008	**********	0.017	0.044	0.027	0.062	0.038
7	S-MN	0.064	0.062	0.199	0.016	**********	0.046	0.054	0.075	0.056	0.070
8	S-AG	0.338	0.495	**********	1.160	**********	**********	0.293	0.404	0.230	**********
9	S-AS	**********	**********	**********	**********	**********	**********	**********	**********	0.011	**********
10	S-AU	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
11	S-B	0.072	0.068	**********	0.137	**********	0.077	0.072	0.066	0.072	0.089
12	S-BA	0.380	0.233	0.214	0.339	**********	0.392	0.251	0.412	0.233	0.173
13	S-BE	**********	0.000	0.008	**********	**********	**********	**********	**********	0.008	**********
14	S-BI	0.000	0.000	**********	0.000	**********	**********	0.000	0.000	0.000	**********
15	S-CD	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
16	S-CO	0.147	0.029	**********	**********	**********	0.110	0.110	0.213	0.110	0.076
17	S-CR	0.082	0.080	**********	0.011	**********	0.101	0.076	0.093	0.076	0.120
18	S-CU	0.304	0.253	**********	1.283	**********	0.269	0.257	0.252	0.252	0.053
19	S-LA	0.058	0.070	0.039	0.045	**********	0.042	0.056	0.044	0.070	0.099
20	S-MO	0.035	0.014	**********	**********	**********	0.000	0.022	0.014	0.021	0.021
21	S-NB	0.009	0.007	**********	0.011	**********	0.011	0.007	0.010	0.007	0.015
22	S-NI	0.078	0.044	0.008	**********	**********	0.146	0.055	0.075	0.053	0.068
23	S-PB	0.229	0.173	0.651	0.079	**********	0.264	0.279	0.259	0.283	0.181
24	S-SB	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
25	S-SC	0.064	0.074	**********	0.137	**********	0.070	0.066	0.045	0.065	0.050
26	S-SN	0.598	0.538	**********	**********	**********	1.030	0.818	0.357	0.818	0.244
27	S-SR	0.129	0.072	0.000	0.025	**********	0.087	0.155	0.253	0.162	0.089
28	S-V	0.036	0.063	0.091	0.055	**********	0.022	0.043	0.051	0.058	0.076
29	S-W	0.414	0.414	**********	0.339	**********	0.330	0.494	0.494	0.494	0.599
30	S-Y	0.053	0.107	0.058	0.008	**********	0.047	0.072	0.033	0.105	0.088
31	S-ZN	0.500	0.500	**********	**********	**********	0.000	0.231	0.500	0.190	**********
32	S-ZR	0.104	0.101	0.182	**********	**********	0.000	0.098	0.104	0.097	0.005
33	S-TH	0.000	0.000	**********	**********	**********	**********	0.000	**********	0.000	**********
34	INST-HG	0.197	0.251	**********	**********	**********	0.151	0.200	0.210	0.196	0.295

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ARRAY OF VARIANCES - CONT.

		21 S-NB	22 S-NI	23 S-PB	24 S-SB	25 S-SC	26 S-SN	27 S-SR	28 S-V	29 S-W	30 S-Y
1	X-COORD.	0.000	0.000	0.000	**********	0.000	0.000	0.000	0.000	0.000	0.000
2	Y-COORD.	0.000	0.000	0.000	**********	0.000	0.000	0.000	0.000	0.000	0.000
3	S-FE%	0.083	0.098	0.073	**********	0.080	0.156	0.068	0.074	0.158	0.074
4	S-MG%	0.081	0.132	0.116	**********	0.095	0.081	0.109	0.117	0.104	0.117
5	S-CA%	0.072	0.067	0.083	**********	0.076	0.102	0.080	0.083	0.075	0.083
6	S-TI%	0.023	0.039	0.062	**********	0.047	0.023	0.061	0.062	0.020	0.062
7	S-MN	0.038	0.070	0.057	**********	0.052	0.057	0.052	0.056	0.037	0.056
8	S-AG	0.677	0.025	0.230	**********	0.293	**********	0.230	0.230	1.160	0.230
9	S-AS	**********	**********	0.011	**********	**********	**********	0.011	0.011	**********	0.011
10	S-AU	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
11	S-B	0.074	0.069	0.075	**********	0.077	0.053	0.077	0.072	0.046	0.072
12	S-BA	0.217	0.267	0.240	**********	0.209	0.283	0.245	0.233	0.420	0.233
13	S-BE	**********	0.000	0.008	**********	**********	**********	0.010	0.008	**********	0.008
14	S-BI	0.000	**********	0.000	**********	0.000	**********	0.000	0.000	0.000	0.000
15	S-CD	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
16	S-CO	0.140	0.193	0.126	**********	0.117	0.000	0.147	0.110	0.057	0.110
17	S-CR	0.034	0.077	0.078	**********	0.078	0.066	0.082	0.076	0.139	0.076
18	S-CU	0.456	0.108	0.252	**********	0.281	0.045	0.271	0.252	0.682	0.252
19	S-LA	0.045	0.060	0.072	**********	0.059	0.055	0.070	0.070	0.074	0.070
20	S-MO	0.014	0.021	0.021	**********	0.022	0.000	0.021	0.021	0.010	0.021
21	S-NB	0.007	0.008	0.006	**********	0.007	0.023	0.007	0.007	0.015	0.007
22	S-NI	0.045	0.053	0.053	**********	0.058	0.000	0.059	0.053	0.171	0.053
23	S-PB	0.169	0.170	0.283	**********	0.280	0.296	0.295	0.283	0.178	0.283
24	S-SB	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
25	S-SC	0.082	0.041	0.061	**********	0.065	0.056	0.048	0.065	0.057	0.065
26	S-SN	0.163	0.244	0.818	**********	0.818	0.818	0.791	0.818	**********	0.818
27	S-SR	0.098	0.131	0.162	**********	0.171	0.128	0.162	0.162	0.042	0.162
28	S-V	0.035	0.063	0.059	**********	0.041	0.018	0.057	0.058	0.031	0.058
29	S-W	0.590	0.511	0.494	**********	0.494	**********	0.494	0.494	0.494	0.494
30	S-Y	0.043	0.060	0.106	**********	0.079	0.069	0.095	0.105	0.034	0.105
31	S-ZN	0.500	0.500	0.190	**********	0.231	0.000	0.190	0.190	0.500	0.190
32	S-ZR	0.000	0.098	0.097	**********	0.129	**********	0.066	0.097	0.008	0.097
33	S-TH	0.000	**********	**********	**********	0.000	**********	**********	0.000	**********	0.000
34	INST-HG	0.191	0.211	0.192	**********	0.222	0.002	0.190	0.196	0.108	0.196

D0101 CORRELATION ANALYSIS - USGS STATPAC (01/15/82) DATE 8/10/84

ARRAY OF VARIANCES - CONT.

		31 S-ZN	32 S-ZR	33 S-TH	34 INST-HG
1	X-COORD.	0.000	0.000	0.000	0.000
2	Y-COORD.	0.000	0.000	0.000	0.000
3	S-FE%	0.093	0.150	0.025	0.101
4	S-MG%	0.076	0.197	0.224	0.138
5	S-CA%	0.140	0.078	0.000	0.104
6	S-TI%	0.132	0.067	**********	0.055
7	S-MN	0.049	0.144	0.016	0.069
8	S-AG	0.099	**********	**********	0.200
9	S-AS	**********	**********	**********	**********
10	S-AU	**********	**********	**********	**********
11	S-B	0.011	0.053	0.137	0.073
12	S-BA	0.012	0.103	0.104	0.194
13	S-BE	**********	0.000	**********	**********
14	S-BI	**********	**********	**********	**********
15	S-CD	**********	**********	**********	**********
16	S-CO	0.000	0.114	**********	0.173
17	S-CR	0.045	0.153	0.011	0.053
18	S-CU	0.000	0.031	**********	0.151
19	S-LA	0.138	0.027	0.016	0.053
20	S-MO	**********	0.015	**********	0.030
21	S-NB	0.045	0.000	0.000	0.004
22	S-NI	0.016	0.098	**********	0.047
23	S-PB	0.207	0.228	**********	0.245
24	S-SB	**********	**********	**********	**********
25	S-SC	0.010	0.017	0.000	0.074
26	S-SN	0.846	**********	**********	2.000
27	S-SR	0.044	0.132	**********	0.213
28	S-V	0.039	0.169	0.012	0.061
29	S-W	0.045	0.500	**********	0.846
30	S-Y	0.200	0.089	0.016	0.088
31	S-ZN	0.190	**********	**********	**********
32	S-ZR	**********	0.097	**********	0.121
33	S-TH	**********	**********	0.000	**********
34	INST-HG	**********	0.093	**********	0.196

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COLUMN	VERSUS	COLUMN	CORRELATION COEFFICIENT	NO. OF PAIRS
1 (X-COORD.)	2	(Y-COORD.)	0.0731	67
1 (X-COORD.)	3	(S-FE%)	-0.1247	67
1 (X-COORD.)	4	(S-MG%)	-0.3340	67
1 (X-COORD.)	5	(S-CA%)	-0.4967	67
1 (X-COORD.)	6	(S-TI%)	-0.0597	57
1 (X-COORD.)	7	(S-MN)	-0.0653	67
1 (X-COORD.)	8	(S-AG)	0.0354	10
1 (X-COORD.)	9	(S-AS)	-1.0000	2
1 (X-COORD.)	10	(S-AU)	********	0
1 (X-COORD.)	11	(S-B)	-0.4607	27
1 (X-COORD.)	12	(S-BA)	0.1096	48
1 (X-COORD.)	13	(S-BE)	0.4035	4
1 (X-COORD.)	14	(S-BI)	********	2
1 (X-COORD.)	15	(S-CD)	********	0
1 (X-COORD.)	16	(S-CO)	-0.2235	14
1 (X-COORD.)	17	(S-CR)	-0.5576	57
1 (X-COORD.)	18	(S-CU)	-0.5086	28
1 (X-COORD.)	19	(S-LA)	-0.2331	67
1 (X-COORD.)	20	(S-MO)	0.0895	15
1 (X-COORD.)	21	(S-NB)	-0.3066	28
1 (X-COORD.)	22	(S-NI)	-0.3062	32
1 (X-COORD.)	23	(S-PB)	-0.0788	65
1 (X-COORD.)	24	(S-SB)	********	0
1 (X-COORD.)	25	(S-SC)	-0.2954	56
1 (X-COORD.)	26	(S-SN)	0.6286	5
1 (X-COORD.)	27	(S-SR)	0.0894	60
1 (X-COORD.)	28	(S-V)	-0.3868	67
1 (X-COORD.)	29	(S-W)	0.2827	7
1 (X-COORD.)	30	(S-Y)	-0.2608	67
1 (X-COORD.)	31	(S-ZN)	-0.5322	5
1 (X-COORD.)	32	(S-ZR)	-0.0957	10
1 (X-COORD.)	33	(S-TH)	********	2
1 (X-COORD.)	34	(INST-HG)	-0.0765	30
2 (Y-COORD.)	3	(S-FE%)	-0.1076	67
2 (Y-COORD.)	4	(S-MG%)	-0.3563	67
2 (Y-COORD.)	5	(S-CA%)	-0.3565	67
2 (Y-COORD.)	6	(S-TI%)	0.0363	57
2 (Y-COORD.)	7	(S-MN)	-0.2014	67
2 (Y-COORD.)	8	(S-AG)	-0.6059	10
2 (Y-COORD.)	9	(S-AS)	1.0000	2
2 (Y-COORD.)	10	(S-AU)	********	0
2 (Y-COORD.)	11	(S-B)	-0.1616	27
2 (Y-COORD.)	12	(S-BA)	0.4862	48
2 (Y-COORD.)	13	(S-BE)	0.9960	4
2 (Y-COORD.)	14	(S-BI)	********	2
2 (Y-COORD.)	15	(S-CD)	********	0
2 (Y-COORD.)	16	(S-CO)	-0.4348	14
2 (Y-COORD.)	17	(S-CR)	-0.3935	57
2 (Y-COORD.)	18	(S-CU)	-0.4374	28
2 (Y-COORD.)	19	(S-LA)	0.2744	67

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COLUMN	VERSUS	COLUMN	CORRELATION COEFFICIENT	NO. OF PAIRS
2 (Y-COORD.)	20	(S-MO)	0.2998	15
2 (Y-COORD.)	21	(S-NB)	-0.0999	28
2 (Y-COORD.)	22	(S-NI)	-0.2587	32
2 (Y-COORD.)	23	(S-PB)	0.1461	65
2 (Y-COORD.)	24	(S-SB)	********	0
2 (Y-COORD.)	25	(S-SC)	0.2985	56
2 (Y-COORD.)	26	(S-SN)	0.5320	5
2 (Y-COORD.)	27	(S-SR)	0.5214	60
2 (Y-COORD.)	28	(S-V)	-0.2016	67
2 (Y-COORD.)	29	(S-W)	-0.7371	7
2 (Y-COORD.)	30	(S-Y)	0.1599	67
2 (Y-COORD.)	31	(S-ZN)	-0.0547	5
2 (Y-COORD.)	32	(S-ZR)	0.3392	10
2 (Y-COORD.)	33	(S-TH)	********	2
2 (Y-COORD.)	34	(INST-HG)	-0.0685	30
3 (S-FE%)	4	(S-MG%)	0.3085	67
3 (S-FE%)	5	(S-CA%)	0.1719	67
3 (S-FE%)	6	(S-TI%)	-0.0605	57
3 (S-FE%)	7	(S-MN)	0.5315	67
3 (S-FE%)	8	(S-AG)	-0.2827	10
3 (S-FE%)	9	(S-AS)	-1.0000	2
3 (S-FE%)	10	(S-AU)	********	0
3 (S-FE%)	11	(S-B)	0.1345	27
3 (S-FE%)	12	(S-BA)	-0.2747	48
3 (S-FE%)	13	(S-BE)	-0.1526	4
3 (S-FE%)	14	(S-BI)	********	2
3 (S-FE%)	15	(S-CD)	********	0
3 (S-FE%)	16	(S-CO)	0.6970	14
3 (S-FE%)	17	(S-CR)	0.2821	57
3 (S-FE%)	18	(S-CU)	0.4182	28
3 (S-FE%)	19	(S-LA)	-0.1024	67
3 (S-FE%)	20	(S-MO)	-0.0824	15
3 (S-FE%)	21	(S-NB)	-0.0518	28
3 (S-FE%)	22	(S-NI)	0.5984	32
3 (S-FE%)	23	(S-PB)	0.1176	65
3 (S-FE%)	24	(S-SB)	********	0
3 (S-FE%)	25	(S-SC)	-0.2707	56
3 (S-FE%)	26	(S-SN)	0.4596	5
3 (S-FE%)	27	(S-SR)	-0.1448	60
3 (S-FE%)	28	(S-V)	0.3228	67
3 (S-FE%)	29	(S-W)	-0.1094	7
3 (S-FE%)	30	(S-Y)	-0.0940	67
3 (S-FE%)	31	(S-ZN)	-0.4837	5
3 (S-FE%)	32	(S-ZR)	-0.3323	10
3 (S-FE%)	33	(S-TH)	********	2
3 (S-FE%)	34	(INST-HG)	0.0221	30
4 (S-MG%)	5	(S-CA%)	0.7004	67
4 (S-MG%)	6	(S-TI%)	0.2310	57
4 (S-MG%)	7	(S-MN)	0.6493	67
4 (S-MG%)	8	(S-AG)	0.1161	10

DC101 CORRELATION ANALYSIS - USGS STATPAC (01/15/82) DATE 8/10/84

COLUMN	VERSUS	COLUMN	CORRELATION COEFFICIENT	NO. OF PAIRS
4 (S-MG%)	9	(S-AS)	********	2
4 (S-MG%)	10	(S-AU)	********	0
4 (S-MG%)	11	(S-B)	0.2937	27
4 (S-MG%)	12	(S-BA)	-0.4503	48
4 (S-MG%)	13	(S-BE)	-0.5073	4
4 (S-MG%)	14	(S-BI)	********	2
4 (S-MG%)	15	(S-CD)	********	0
4 (S-MG%)	16	(S-CO)	-0.2069	14
4 (S-MG%)	17	(S-CR)	0.5181	57
4 (S-MG%)	18	(S-CU)	0.2549	28
4 (S-MG%)	19	(S-LA)	0.2173	67
4 (S-MG%)	20	(S-MO)	0.0655	15
4 (S-MG%)	21	(S-NB)	0.0090	28
4 (S-MG%)	22	(S-NI)	0.1033	32
4 (S-MG%)	23	(S-PB)	0.0091	65
4 (S-MG%)	24	(S-SB)	********	0
4 (S-MG%)	25	(S-SC)	-0.0321	56
4 (S-MG%)	26	(S-SN)	-0.4234	5
4 (S-MG%)	27	(S-SR)	-0.5869	60
4 (S-MG%)	28	(S-V)	0.6806	67
4 (S-MG%)	29	(S-W)	0.7393	7
4 (S-MG%)	30	(S-Y)	0.1960	67
4 (S-MG%)	31	(S-ZN)	0.2648	5
4 (S-MG%)	32	(S-ZR)	-0.0180	10
4 (S-MG%)	33	(S-TH)	********	2
4 (S-MG%)	34	(INST-HG)	0.1633	30
5 (S-CA%)	6	(S-TI%)	0.2612	57
5 (S-CA%)	7	(S-MN)	0.4626	67
5 (S-CA%)	8	(S-AG)	0.3703	10
5 (S-CA%)	9	(S-AS)	********	2
5 (S-CA%)	10	(S-AU)	********	0
5 (S-CA%)	11	(S-B)	0.2607	27
5 (S-CA%)	12	(S-BA)	-0.3052	48
5 (S-CA%)	13	(S-BE)	-0.7780	4
5 (S-CA%)	14	(S-BI)	********	2
5 (S-CA%)	15	(S-CD)	********	0
5 (S-CA%)	16	(S-CO)	-0.2926	14
5 (S-CA%)	17	(S-CR)	0.5394	57
5 (S-CA%)	18	(S-CU)	0.0859	28
5 (S-CA%)	19	(S-LA)	0.3174	67
5 (S-CA%)	20	(S-MO)	-0.1550	15
5 (S-CA%)	21	(S-NB)	0.0344	28
5 (S-CA%)	22	(S-NI)	0.0388	32
5 (S-CA%)	23	(S-PB)	0.0721	65
5 (S-CA%)	24	(S-SB)	********	0
5 (S-CA%)	25	(S-SC)	0.1140	56
5 (S-CA%)	26	(S-SN)	-0.4318	5
5 (S-CA%)	27	(S-SR)	-0.3683	60
5 (S-CA%)	28	(S-V)	0.6440	67
5 (S-CA%)	29	(S-W)	0.1138	7

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COLUMN	VERSUS COLUMN	CORRELATION COEFFICIENT	NO. OF PAIRS
5 (S-CA%)	30 (S-Y)	0.3293	67
5 (S-CA%)	31 (S-ZN)	0.2841	5
5 (S-CA%)	32 (S-ZR)	-0.1482	10
5 (S-CA%)	33 (S-TH)	********	2
5 (S-CA%)	34 (INST-HG)	0.2422	30
6 (S-TI%)	7 (S-MN)	0.1737	57
6 (S-TI%)	8 (S-AG)	-0.0508	10
6 (S-TI%)	9 (S-AS)	1.0000	2
6 (S-TI%)	10 (S-AU)	********	0
6 (S-TI%)	11 (S-B)	-0.0224	20
6 (S-TI%)	12 (S-BA)	-0.0149	39
6 (S-TI%)	13 (S-BE)	-0.2313	4
6 (S-TI%)	14 (S-BI)	********	2
6 (S-TI%)	15 (S-CD)	********	0
6 (S-TI%)	16 (S-CO)	0.2432	6
6 (S-TI%)	17 (S-CR)	0.1323	47
6 (S-TI%)	18 (S-CU)	0.2007	25
6 (S-TI%)	19 (S-LA)	0.6866	57
6 (S-TI%)	20 (S-MO)	-0.0742	12
6 (S-TI%)	21 (S-NB)	0.3075	18
6 (S-TI%)	22 (S-NI)	-0.0514	28
6 (S-TI%)	23 (S-PB)	-0.0341	57
6 (S-TI%)	24 (S-SB)	********	0
6 (S-TI%)	25 (S-SC)	0.3885	46
6 (S-TI%)	26 (S-SN)	-0.9202	3
6 (S-TI%)	27 (S-SR)	-0.2191	54
6 (S-TI%)	28 (S-V)	0.3980	57
6 (S-TI%)	29 (S-W)	-0.2735	4
6 (S-TI%)	30 (S-Y)	0.8503	57
6 (S-TI%)	31 (S-ZN)	0.6500	4
6 (S-TI%)	32 (S-ZR)	0.3784	10
6 (S-TI%)	33 (S-TH)	********	1
6 (S-TI%)	34 (INST-HG)	-0.2010	24
7 (S-MN)	8 (S-AG)	0.0713	10
7 (S-MN)	9 (S-AS)	1.0000	2
7 (S-MN)	10 (S-AU)	********	0
7 (S-MN)	11 (S-B)	0.0033	27
7 (S-MN)	12 (S-BA)	-0.3994	48
7 (S-MN)	13 (S-BE)	-0.0828	4
7 (S-MN)	14 (S-BI)	********	2
7 (S-MN)	15 (S-CD)	********	0
7 (S-MN)	16 (S-CO)	-0.2050	14
7 (S-MN)	17 (S-CR)	0.2866	57
7 (S-MN)	18 (S-CU)	-0.0058	28
7 (S-MN)	19 (S-LA)	0.1078	67
7 (S-MN)	20 (S-MO)	0.1747	15
7 (S-MN)	21 (S-NB)	-0.1770	28
7 (S-MN)	22 (S-NI)	0.0416	32
7 (S-MN)	23 (S-PB)	0.2171	65
7 (S-MN)	24 (S-SB)	********	0

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COLUMN	VERSUS	COLUMN	CORRELATION COEFFICIENT	NO. OF PAIRS
7 (S-MN)	25	(S-SC)	-0.0461	56
7 (S-MN)	26	(S-SN)	0.3375	5
7 (S-MN)	27	(S-SR)	-0.3775	60
7 (S-MN)	28	(S-V)	0.6222	67
7 (S-MN)	29	(S-W)	0.2281	7
7 (S-MN)	30	(S-Y)	0.2587	67
7 (S-MN)	31	(S-ZN)	-0.4644	5
7 (S-MN)	32	(S-ZR)	-0.3120	10
7 (S-MN)	33	(S-TH)	********	2
7 (S-MN)	34	(INST-HG)	0.0259	30
8 (S-AG)	9	(S-AS)	1.0000	2
8 (S-AG)	10	(S-AU)	********	0
8 (S-AG)	11	(S-B)	-0.6064	5
8 (S-AG)	12	(S-BA)	-0.6966	4
8 (S-AG)	13	(S-BE)	********	1
8 (S-AG)	14	(S-BI)	********	2
8 (S-AG)	15	(S-CD)	********	0
8 (S-AG)	16	(S-CO)	********	1
8 (S-AG)	17	(S-CR)	0.0961	8
8 (S-AG)	18	(S-CU)	-0.5750	4
8 (S-AG)	19	(S-LA)	-0.3387	10
8 (S-AG)	20	(S-MO)	********	1
8 (S-AG)	21	(S-NB)	-0.9909	3
8 (S-AG)	22	(S-NI)	1.0000	2
8 (S-AG)	23	(S-PB)	0.1259	10
8 (S-AG)	24	(S-SB)	********	0
8 (S-AG)	25	(S-SC)	-0.5723	8
8 (S-AG)	26	(S-SN)	********	1
8 (S-AG)	27	(S-SR)	-0.3601	10
8 (S-AG)	28	(S-V)	0.4325	10
8 (S-AG)	29	(S-W)	1.0000	2
8 (S-AG)	30	(S-Y)	-0.0779	10
8 (S-AG)	31	(S-ZN)	-1.0000	3
8 (S-AG)	32	(S-ZR)	********	1
8 (S-AG)	33	(S-TH)	********	1
8 (S-AG)	34	(INST-HG)	-1.0000	2
9 (S-AS)	10	(S-AU)	********	0
9 (S-AS)	11	(S-B)	********	1
9 (S-AS)	12	(S-BA)	********	0
9 (S-AS)	13	(S-BE)	********	1
9 (S-AS)	14	(S-BI)	********	0
9 (S-AS)	15	(S-CD)	********	0
9 (S-AS)	16	(S-CO)	********	0
9 (S-AS)	17	(S-CR)	********	1
9 (S-AS)	18	(S-CU)	********	1
9 (S-AS)	19	(S-LA)	1.0000	2
9 (S-AS)	20	(S-MO)	********	0
9 (S-AS)	21	(S-NB)	********	0
9 (S-AS)	22	(S-NI)	********	0
9 (S-AS)	23	(S-PB)	1.0000	2

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9 (S-AS)	24 (S-SB)	********	0
9 (S-AS)	25 (S-SC)	********	1
9 (S-AS)	26 (S-SN)	********	0
9 (S-AS)	27 (S-SR)	1.0000	2
9 (S-AS)	28 (S-V)	1.0000	2
9 (S-AS)	29 (S-W)	********	0
9 (S-AS)	30 (S-Y)	1.0000	2
9 (S-AS)	31 (S-ZN)	********	1
9 (S-AS)	32 (S-ZR)	********	0
9 (S-AS)	33 (S-TH)	********	0
9 (S-AS)	34 (INST-HG)	********	0
10 (S-AU)	11 (S-B)	********	0
10 (S-AU)	12 (S-BA)	********	0
10 (S-AU)	13 (S-BE)	********	0
10 (S-AU)	14 (S-BI)	********	0
10 (S-AU)	15 (S-CD)	********	0
10 (S-AU)	16 (S-CO)	********	0
10 (S-AU)	17 (S-CR)	********	0
10 (S-AU)	18 (S-CU)	********	0
10 (S-AU)	19 (S-LA)	********	0
10 (S-AU)	20 (S-MO)	********	0
10 (S-AU)	21 (S-NB)	********	0
10 (S-AU)	22 (S-NI)	********	0
10 (S-AU)	23 (S-PB)	********	0
10 (S-AU)	24 (S-SB)	********	0
10 (S-AU)	25 (S-SC)	********	0
10 (S-AU)	26 (S-SN)	********	0
10 (S-AU)	27 (S-SR)	********	0
10 (S-AU)	28 (S-V)	********	0
10 (S-AU)	29 (S-W)	********	0
10 (S-AU)	30 (S-Y)	********	0
10 (S-AU)	31 (S-ZN)	********	0
10 (S-AU)	32 (S-ZR)	********	0
10 (S-AU)	33 (S-TH)	********	0
10 (S-AU)	34 (INST-HG)	********	0
11 (S-B)	12 (S-BA)	0.0833	22
11 (S-B)	13 (S-BE)	********	1
11 (S-B)	14 (S-BI)	********	2
11 (S-B)	15 (S-CD)	********	0
11 (S-B)	16 (S-CO)	-0.1112	10
11 (S-B)	17 (S-CR)	0.5422	27
11 (S-B)	18 (S-CU)	0.4485	18
11 (S-B)	19 (S-LA)	0.0164	27
11 (S-B)	20 (S-MO)	-0.0189	8
11 (S-B)	21 (S-NB)	0.2669	14
11 (S-B)	22 (S-NI)	0.0367	18
11 (S-B)	23 (S-PB)	-0.0893	26
11 (S-B)	24 (S-SB)	********	0
11 (S-B)	25 (S-SC)	0.1046	24
11 (S-B)	26 (S-SN)	-0.0546	3

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11 (S-B)	27	(S-SR)	-0.1796	22
11 (S-B)	28	(S-V)	0.2384	27
11 (S-B)	29	(S-W)	-0.3150	6
11 (S-B)	30	(S-Y)	-0.2214	27
11 (S-B)	31	(S-ZN)	1.0000	2
11 (S-B)	32	(S-ZR)	-0.0728	7
11 (S-B)	33	(S-TH)	********	2
11 (S-B)	34	(INST-HG)	0.0458	13
12 (S-BA)	13	(S-BE)	********	3
12 (S-BA)	14	(S-BI)	********	2
12 (S-BA)	15	(S-CD)	********	0
12 (S-BA)	16	(S-CO)	-0.0316	10
12 (S-BA)	17	(S-CR)	-0.0854	40
12 (S-BA)	18	(S-CU)	-0.2200	18
12 (S-BA)	19	(S-LA)	0.0577	48
12 (S-BA)	20	(S-MO)	-0.2347	13
12 (S-BA)	21	(S-NB)	0.2237	24
12 (S-BA)	22	(S-NI)	-0.2356	27
12 (S-BA)	23	(S-PB)	0.1520	46
12 (S-BA)	24	(S-SB)	********	0
12 (S-BA)	25	(S-SC)	0.2123	39
12 (S-BA)	26	(S-SN)	0.3709	4
12 (S-BA)	27	(S-SR)	0.3010	41
12 (S-BA)	28	(S-V)	-0.2981	48
12 (S-BA)	29	(S-W)	-0.7105	6
12 (S-BA)	30	(S-Y)	-0.0314	48
12 (S-BA)	31	(S-ZN)	-1.0000	2
12 (S-BA)	32	(S-ZR)	0.0630	9
12 (S-BA)	33	(S-TH)	********	2
12 (S-BA)	34	(INST-HG)	-0.0266	19
13 (S-BE)	14	(S-BI)	********	0
13 (S-BE)	15	(S-CD)	********	0
13 (S-BE)	16	(S-CO)	********	0
13 (S-BE)	17	(S-CR)	********	1
13 (S-BE)	18	(S-CU)	********	1
13 (S-BE)	19	(S-LA)	-0.9080	4
13 (S-BE)	20	(S-MO)	********	1
13 (S-BE)	21	(S-NB)	********	0
13 (S-BE)	22	(S-NI)	********	2
13 (S-BE)	23	(S-PB)	0.9766	4
13 (S-BE)	24	(S-SB)	********	0
13 (S-BE)	25	(S-SC)	********	1
13 (S-BE)	26	(S-SN)	********	0
13 (S-BE)	27	(S-SR)	********	3
13 (S-BE)	28	(S-V)	-0.1911	4
13 (S-BE)	29	(S-W)	********	0
13 (S-BE)	30	(S-Y)	-0.7764	4
13 (S-BE)	31	(S-ZN)	********	1
13 (S-BE)	32	(S-ZR)	********	3
13 (S-BE)	33	(S-TH)	********	0

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COLUMN	VERSUS	COLUMN	CORRELATION COEFFICIENT	NO. OF PAIRS
13 (S-BE)	34	(INST-HG)	********	1
14 (S-BI)	15	(S-CD)	********	0
14 (S-BI)	16	(S-CO)	********	0
14 (S-BI)	17	(S-CR)	********	2
14 (S-BI)	18	(S-CU)	********	2
14 (S-BI)	19	(S-LA)	********	2
14 (S-BI)	20	(S-MO)	********	1
14 (S-BI)	21	(S-NB)	********	2
14 (S-BI)	22	(S-NI)	********	1
14 (S-BI)	23	(S-PB)	********	2
14 (S-BI)	24	(S-SB)	********	0
14 (S-BI)	25	(S-SC)	********	2
14 (S-BI)	26	(S-SN)	********	0
14 (S-BI)	27	(S-SR)	********	2
14 (S-BI)	28	(S-V)	********	2
14 (S-BI)	29	(S-W)	********	2
14 (S-BI)	30	(S-Y)	********	2
14 (S-BI)	31	(S-ZN)	********	0
14 (S-BI)	32	(S-ZR)	********	1
14 (S-BI)	33	(S-TH)	********	1
14 (S-BI)	34	(INST-HG)	********	0
15 (S-CD)	16	(S-CO)	********	0
15 (S-CD)	17	(S-CR)	********	0
15 (S-CD)	18	(S-CU)	********	0
15 (S-CD)	19	(S-LA)	********	0
15 (S-CD)	20	(S-MO)	********	0
15 (S-CD)	21	(S-NB)	********	0
15 (S-CD)	22	(S-NI)	********	0
15 (S-CD)	23	(S-PB)	********	0
15 (S-CD)	24	(S-SB)	********	0
15 (S-CD)	25	(S-SC)	********	0
15 (S-CD)	26	(S-SN)	********	0
15 (S-CD)	27	(S-SR)	********	0
15 (S-CD)	28	(S-V)	********	0
15 (S-CD)	29	(S-W)	********	0
15 (S-CD)	30	(S-Y)	********	0
15 (S-CD)	31	(S-ZN)	********	0
15 (S-CD)	32	(S-ZR)	********	0
15 (S-CD)	33	(S-TH)	********	0
15 (S-CD)	34	(INST-HG)	********	0
16 (S-CO)	17	(S-CR)	0.1911	14
16 (S-CO)	18	(S-CU)	0.8902	6
16 (S-CO)	19	(S-LA)	-0.5020	14
16 (S-CO)	20	(S-MO)	********	3
16 (S-CO)	21	(S-NB)	-0.3736	10
16 (S-CO)	22	(S-NI)	0.7726	7
16 (S-CO)	23	(S-PB)	0.0509	12
16 (S-CO)	24	(S-SB)	********	0
16 (S-CO)	25	(S-SC)	-0.7361	13
16 (S-CO)	26	(S-SN)	********	3

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COLUMN	VERSUS	COLUMN	CORRELATION COEFFICIENT	NO. OF PAIRS
16 (S-CO)	27	(S-SR)	0.1377	10
16 (S-CO)	28	(S-V)	-0.4279	14
16 (S-CO)	29	(S-W)	0.3544	4
16 (S-CO)	30	(S-Y)	-0.5249	14
16 (S-CO)	31	(S-ZN)	********	2
16 (S-CO)	32	(S-ZR)	********	2
16 (S-CO)	33	(S-TH)	********	1
16 (S-CO)	34	(INST-HG)	-0.1646	8
17 (S-CR)	18	(S-CU)	0.4308	26
17 (S-CR)	19	(S-LA)	0.2534	57
17 (S-CR)	20	(S-MO)	-0.2744	13
17 (S-CR)	21	(S-NB)	0.2920	26
17 (S-CR)	22	(S-NI)	0.4617	30
17 (S-CR)	23	(S-PB)	0.2405	55
17 (S-CR)	24	(S-SB)	********	0
17 (S-CR)	25	(S-SC)	0.3313	52
17 (S-CR)	26	(S-SN)	-0.8613	5
17 (S-CR)	27	(S-SR)	-0.4903	50
17 (S-CR)	28	(S-V)	0.6811	57
17 (S-CR)	29	(S-W)	0.2445	7
17 (S-CR)	30	(S-Y)	0.3096	57
17 (S-CR)	31	(S-ZN)	0.5129	4
17 (S-CR)	32	(S-ZR)	0.0041	8
17 (S-CR)	33	(S-TH)	********	2
17 (S-CR)	34	(INST-HG)	0.0396	28
18 (S-CU)	19	(S-LA)	-0.1919	28
18 (S-CU)	20	(S-MO)	-0.1255	7
18 (S-CU)	21	(S-NB)	0.0482	11
18 (S-CU)	22	(S-NI)	0.7137	18
18 (S-CU)	23	(S-PB)	0.1317	28
18 (S-CU)	24	(S-SB)	********	0
18 (S-CU)	25	(S-SC)	0.1879	24
18 (S-CU)	26	(S-SN)	-1.0000	2
18 (S-CU)	27	(S-SR)	-0.3941	26
18 (S-CU)	28	(S-V)	0.2835	28
18 (S-CU)	29	(S-W)	0.3684	5
18 (S-CU)	30	(S-Y)	-0.0689	28
18 (S-CU)	31	(S-ZN)	********	2
18 (S-CU)	32	(S-ZR)	-0.1366	7
18 (S-CU)	33	(S-TH)	********	1
18 (S-CU)	34	(INST-HG)	-0.0376	14
19 (S-LA)	20	(S-MO)	0.0887	15
19 (S-LA)	21	(S-NB)	0.0422	28
19 (S-LA)	22	(S-NI)	-0.1169	32
19 (S-LA)	23	(S-PB)	-0.1209	65
19 (S-LA)	24	(S-SB)	********	0
19 (S-LA)	25	(S-SC)	0.5264	56
19 (S-LA)	26	(S-SN)	-0.7470	5
19 (S-LA)	27	(S-SR)	-0.0861	60
19 (S-LA)	28	(S-V)	0.2857	67

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COLUMN	VERSUS COLUMN	CORRELATION COEFFICIENT	NO. OF PAIRS
19 (S-LA)	29 (S-W)	-0.8727	7
19 (S-LA)	30 (S-Y)	0.7882	67
19 (S-LA)	31 (S-ZN)	0.2821	5
19 (S-LA)	32 (S-ZR)	0.2644	10
19 (S-LA)	33 (S-TH)	********	2
19 (S-LA)	34 (INST-HG)	-0.1813	30
20 (S-MO)	21 (S-NB)	-0.5763	6
20 (S-MO)	22 (S-NI)	-0.2774	14
20 (S-MO)	23 (S-PB)	0.1862	15
20 (S-MO)	24 (S-SB)	********	0
20 (S-MO)	25 (S-SC)	-0.1005	13
20 (S-MO)	26 (S-SN)	********	2
20 (S-MO)	27 (S-SR)	-0.0526	14
20 (S-MO)	28 (S-V)	0.0271	15
20 (S-MO)	29 (S-W)	0.9412	3
20 (S-MO)	30 (S-Y)	0.0460	15
20 (S-MO)	31 (S-ZN)	********	1
20 (S-MO)	32 (S-ZR)	0.1193	4
20 (S-MO)	33 (S-TH)	********	0
20 (S-MO)	34 (INST-HG)	-0.1355	7
21 (S-NB)	22 (S-NI)	-0.1021	17
21 (S-NB)	23 (S-PB)	0.3058	26
21 (S-NB)	24 (S-SB)	********	0
21 (S-NB)	25 (S-SC)	0.2530	27
21 (S-NB)	26 (S-SN)	0.8743	3
21 (S-NB)	27 (S-SR)	-0.2391	22
21 (S-NB)	28 (S-V)	0.1254	28
21 (S-NB)	29 (S-W)	-0.0036	6
21 (S-NB)	30 (S-Y)	0.1640	28
21 (S-NB)	31 (S-ZN)	-1.0000	2
21 (S-NB)	32 (S-ZR)	********	2
21 (S-NB)	33 (S-TH)	********	2
21 (S-NB)	34 (INST-HG)	0.0787	15
22 (S-NI)	23 (S-PB)	0.1680	32
22 (S-NI)	24 (S-SB)	********	0
22 (S-NI)	25 (S-SC)	-0.2286	28
22 (S-NI)	26 (S-SN)	********	2
22 (S-NI)	27 (S-SR)	0.0275	29
22 (S-NI)	28 (S-V)	0.2176	32
22 (S-NI)	29 (S-W)	0.1881	5
22 (S-NI)	30 (S-Y)	-0.0627	32
22 (S-NI)	31 (S-ZN)	-1.0000	2
22 (S-NI)	32 (S-ZR)	0.3335	8
22 (S-NI)	33 (S-TH)	********	0
22 (S-NI)	34 (INST-HG)	0.2157	17
23 (S-PB)	24 (S-SB)	********	0
23 (S-PB)	25 (S-SC)	0.2845	54
23 (S-PB)	26 (S-SN)	0.7683	5
23 (S-PB)	27 (S-SR)	0.0094	60
23 (S-PB)	28 (S-V)	0.3271	65

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23 (S-PB)	29 (S-W)		0.6546	7
23 (S-PB)	30 (S-Y)		0.1159	65
23 (S-PB)	31 (S-ZN)		-0.6975	5
23 (S-PB)	32 (S-ZR)		0.2435	10
23 (S-PB)	33 (S-TH)		********	1
23 (S-PB)	34 (INST-HG)		-0.1724	28
24 (S-SB)	25 (S-SC)		********	0
24 (S-SB)	26 (S-SN)		********	0
24 (S-SB)	27 (S-SR)		********	0
24 (S-SB)	28 (S-V)		********	0
24 (S-SB)	29 (S-W)		********	0
24 (S-SB)	30 (S-Y)		********	0
24 (S-SB)	31 (S-ZN)		********	0
24 (S-SB)	32 (S-ZR)		********	0
24 (S-SB)	33 (S-TH)		********	0
24 (S-SB)	34 (INST-HG)		********	0
25 (S-SC)	26 (S-SN)		-0.5710	5
25 (S-SC)	27 (S-SR)		-0.1980	49
25 (S-SC)	28 (S-V)		0.3033	56
25 (S-SC)	29 (S-W)		-0.5198	7
25 (S-SC)	30 (S-Y)		0.6309	56
25 (S-SC)	31 (S-ZN)		0.5129	4
25 (S-SC)	32 (S-ZR)		0.4641	5
25 (S-SC)	33 (S-TH)		********	2
25 (S-SC)	34 (INST-HG)		-0.0645	25
26 (S-SN)	27 (S-SR)		0.9114	4
26 (S-SN)	28 (S-V)		-0.3808	5
26 (S-SN)	29 (S-W)		********	1
26 (S-SN)	30 (S-Y)		-0.8398	5
26 (S-SN)	31 (S-ZN)		********	2
26 (S-SN)	32 (S-ZR)		********	0
26 (S-SN)	33 (S-TH)		********	0
26 (S-SN)	34 (INST-HG)		1.0000	2
27 (S-SR)	28 (S-V)		-0.4646	60
27 (S-SR)	29 (S-W)		-0.8199	7
27 (S-SR)	30 (S-Y)		-0.2314	60
27 (S-SR)	31 (S-ZN)		0.0032	5
27 (S-SR)	32 (S-ZR)		-0.0211	8
27 (S-SR)	33 (S-TH)		********	1
27 (S-SR)	34 (INST-HG)		-0.1327	25
28 (S-V)	29 (S-W)		0.7423	7
28 (S-V)	30 (S-Y)		0.4842	67
28 (S-V)	31 (S-ZN)		0.1779	5
28 (S-V)	32 (S-ZR)		0.0743	10
28 (S-V)	33 (S-TH)		********	2
28 (S-V)	34 (INST-HG)		0.2716	30
29 (S-W)	30 (S-Y)		-0.5502	7
29 (S-W)	31 (S-ZN)		-1.0000	2
29 (S-W)	32 (S-ZR)		1.0000	2
29 (S-W)	33 (S-TH)		********	1

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29 (S-W)	34 (INST-HG)	-1.0000	2
30 (S-Y)	31 (S-ZN)	0.2942	5
30 (S-Y)	32 (S-ZR)	0.4088	10
30 (S-Y)	33 (S-TH)	********	2
30 (S-Y)	34 (INST-HG)	-0.0441	30
31 (S-ZN)	32 (S-ZR)	********	0
31 (S-ZN)	33 (S-TH)	********	0
31 (S-ZN)	34 (INST-HG)	********	1
32 (S-ZR)	33 (S-TH)	********	0
32 (S-ZR)	34 (INST-HG)	0.7349	6
33 (S-TH)	34 (INST-HG)	********	1

D0101 CORRELATION ANALYSIS - USGS STATPAC (01/15/82) DATE 7/20/84

TITLE	INPUT ID		N	M	***** OPTIONS *****	OUTPUT ID		N	M
	-ds-6	-	29	38	1 0 1 1 0 0 0 0 0 0	-	-	38	38

NUMBER OF SELECTED COLUMNS 38

SELECTED COLUMN INDICES

1	2	3	4	5	6	7	8	9	10
11	12	13	14	15	16	17	18	19	20
21	22	23	24	25	26	27	28	29	30
31	32	33	34	35	36	37	38		

SELECTED COLUMN IDENTIFIERS

X-COORD.	Y-COORD.	S-FE%	S-MG%	S-CA%	S-TI%	S-MN	S-AG	S-AS	S-AU
S-B	S-BA	S-BE	S-BI	S-CD	S-CO	S-CR	S-CU	S-LA	S-MO
S-NB	S-NI	S-PB	S-SB	S-SC	S-SN	S-SR	S-V	S-W	S-Y
S-ZN	S-ZR	S-TH	AA-AU-P	INST-HG	AA-AS-P	AA-ZN-P	AA-SB-P		

NUMBER OF SELECTED ROW PAIRS 1

SELECTED ROW PAIRS
1- 29

P H A S E T W O R E S U L T S

W A R N I N G * * * THE RESULTS FROM THIS PHASE "SHOULD NOT" BE ENTERED INTO D0096-FACTOR ANALYSIS.
THE CORRELATION MATRIX FROM THIS PHASE DOES NOT HAVE THE GRAMIAN PROPERTIES
WHICH ARE REQUIRED FOR FACTOR ANALYSIS.

D0101 CORRELATION ANALYSIS - USGS STATPAC (01/15/82) DATE 7/20/84

ARRAY OF MEANS -

		1 X-COORD.	2 Y-COORD.	3 S-FE%	4 S-MG%	5 S-CA%	6 S-TI%	7 S-MN	8 S-AG	9 S-AS	10 S-AU
1	X-COORD.	4.6285	4.6285	4.6285	4.6283	4.6285	4.6276	4.6276	4.6273	4.6241	**********
2	Y-COORD.	5.6201	5.6201	5.6201	5.6199	5.6201	5.6198	5.6204	5.6203	5.6197	**********
3	S-FE%	-0.1145	-0.1145	-0.1145	-0.0386	-0.0937	0.0032	-0.0456	-0.1133	0.0012	**********
4	S-MG%	-1.2044	-1.2044	-1.2044	-1.2044	-1.2044	-1.0391	-1.1032	-1.2429	-1.1631	**********
5	S-CA%	0.0081	0.0081	0.0081	0.0512	0.0081	-0.1166	-0.2091	0.0833	0.2666	**********
6	S-TI%	-1.5239	-1.5239	-1.5239	-1.5107	-1.4867	-1.5239	-1.4002	-1.5472	-1.4207	**********
7	S-MN	2.7026	2.7026	2.7026	2.6966	2.7290	2.4670	2.7026	2.7475	2.3659	**********
8	S-AG	1.6985	1.6985	1.6985	1.4924	1.7473	1.2360	1.6219	1.6985	1.8298	**********
9	S-AS	2.6720	2.6720	2.6720	2.7330	2.6720	2.7398	2.8486	2.6720	2.6720	**********
10	S-AU	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
11	S-B	1.4982	1.4982	1.4982	1.4938	1.5102	1.5782	1.4910	1.5182	1.7143	**********
12	S-BA	2.6770	2.6770	2.6770	2.7070	2.7065	2.5596	2.4882	2.7223	2.7306	**********
13	S-BE	1.2078	1.2078	1.2078	1.1112	1.2427	0.8195	1.0865	1.2586	1.2539	**********
14	S-BI	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
15	S-CD	1.5557	1.5557	1.5557	1.5557	1.5557	1.6391	1.3891	1.5557	1.6391	**********
16	S-CO	1.0335	1.0335	1.0335	1.0335	1.0335	0.9889	1.0335	1.1088	1.3495	**********
17	S-CR	1.2362	1.2362	1.2362	1.2362	1.2362	1.2755	1.3306	1.2755	1.4924	**********
18	S-CU	1.9106	1.9106	1.9106	1.6928	1.9106	1.8163	1.9302	1.9965	2.4395	**********
19	S-LA	1.3967	1.3967	1.3967	1.4225	1.4054	1.4082	1.4286	1.3692	1.3010	**********
20	S-MO	1.2327	1.2327	1.2327	1.1006	1.1770	1.5071	1.3244	1.2327	1.1215	**********
21	S-NB	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
22	S-NI	1.1134	1.1134	1.1134	1.1817	1.1134	1.2191	1.1662	1.1185	1.3884	**********
23	S-PB	2.2720	2.2720	2.2720	2.1174	2.3126	2.0582	2.1726	2.3768	2.6518	**********
24	S-SB	2.1676	2.1676	2.1676	2.1456	2.1676	2.1626	2.1003	2.1787	2.3465	**********
25	S-SC	0.7720	0.7720	0.7720	0.7720	0.7720	0.7720	0.7720	0.7720	0.7720	**********
26	S-SN	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
27	S-SR	2.6747	2.6747	2.6747	2.5691	2.6747	2.7796	2.6398	2.6747	2.5398	**********
28	S-V	1.3803	1.3803	1.3803	1.5043	1.3841	1.5009	1.4216	1.4152	1.5383	**********
29	S-W	2.0000	2.0000	2.0000	2.0000	2.0000	2.0000	2.0000	2.0000	**********	**********
30	S-Y	1.1698	1.1698	1.1698	1.1910	1.1698	1.2183	1.1698	1.1690	1.2500	**********
31	S-ZN	2.8253	2.8253	2.8253	2.8217	2.8253	2.8118	2.7522	2.8253	2.9567	**********
32	S-ZR	1.5963	1.5963	1.5963	1.5849	1.5963	1.5963	1.5963	1.6839	1.7477	**********
33	S-TH	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
34	AA-AU-P	-0.2486	-0.2486	-0.2486	-0.6549	-0.3993	-0.1386	-0.0234	-0.2486	-0.3244	**********
35	INST-HG	-0.3088	-0.3088	-0.3088	-0.3731	-0.3379	-0.3212	-0.3488	-0.2650	-0.2246	**********
36	AA-AS-P	1.7677	1.7677	1.7677	1.6574	1.7973	1.6487	1.7294	1.8132	2.4355	**********
37	AA-ZN-P	2.3101	2.3101	2.3101	2.3078	2.3605	2.1320	2.2090	2.4135	2.5239	**********
38	AA-SB-P	1.2456	1.2456	1.2456	1.1360	1.2806	1.1077	1.1326	1.3349	1.7277	**********

D0101 CORRELATION ANALYSIS - USGS STATPAC (01/15/82) DATE 7/20/84

ARRAY OF MEANS - CONT.

		11 S-B	12 S-BA	13 S-BE	14 S-BI	15 S-CD	16 S-CO	17 S-CR	18 S-CU	19 S-LA	20 S-MO
1	X-COORD.	4.6290	4.6276	4.6297	**********	4.6252	4.6274	4.6189	4.6281	4.6310	4.6254
2	Y-COORD.	5.6201	5.6198	5.6201	**********	5.6190	5.6197	5.6204	5.6200	5.6208	5.6199
3	S-FE%	-0.1131	0.0130	-0.1350	**********	-0.0091	0.2570	0.2349	-0.0422	-0.3044	-0.0861
4	S-MG%	-1.1885	-1.1543	-1.1825	**********	-1.3040	-0.8111	-1.0287	-1.1317	-1.2713	-1.2535
5	S-CA%	0.0455	-0.0041	0.0472	**********	0.8110	-0.1937	0.3139	-0.0367	-0.1575	0.2918
6	S-TI%	-1.5136	-1.4345	-1.5456	**********	-1.6620	-1.0836	-1.3876	-1.4735	-1.5684	-1.5832
7	S-MN	2.7378	2.5662	2.7608	**********	2.2386	2.3539	2.0102	2.6600	2.9280	2.3224
8	S-AG	1.6985	1.0997	1.6985	**********	1.4827	1.0511	0.7204	1.7101	1.9662	1.4052
9	S-AS	2.6720	2.8194	2.5579	**********	2.8495	2.5000	2.4337	2.6720	2.6150	2.5493
10	S-AU	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
11	S-B	1.4982	1.4546	1.4990	**********	1.7254	1.5411	1.7239	1.5740	1.4108	1.6657
12	S-BA	2.7476	2.6770	2.8132	**********	2.7306	2.4346	2.3465	2.6400	2.8103	2.7151
13	S-BE	1.2078	0.8467	1.2078	**********	0.9982	0.5795	0.4164	1.2549	1.3326	0.9453
14	S-BI	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
15	S-CD	1.5557	1.3715	1.5715	**********	1.5557	**********	1.8891	1.5715	1.7518	1.6391
16	S-CO	1.0649	0.9889	1.0649	**********	**********	1.0335	1.0973	1.0335	1.0000	1.3495
17	S-CR	1.2755	1.3306	1.2755	**********	1.0880	1.3693	1.2362	1.2362	1.0000	1.4133
18	S-CU	1.9550	1.5957	1.9454	**********	1.5951	1.8524	1.8954	1.9106	1.7267	2.1541
19	S-LA	1.3967	1.4225	1.3967	**********	1.3010	1.3891	1.3010	1.3844	1.3967	1.3010
20	S-MO	1.2327	1.3959	1.2327	**********	1.0128	1.3266	1.2073	1.2248	1.5440	1.2327
21	S-NB	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
22	S-NI	1.1237	1.2465	1.1237	**********	1.0000	1.3788	1.3997	1.1134	0.7993	1.2553
23	S-PB	2.3126	1.7709	2.2977	**********	2.5398	1.8106	1.8853	2.3536	2.3200	2.2981
24	S-SB	2.1676	2.2168	2.1676	**********	2.4337	2.0000	2.1505	2.1787	2.1720	2.2954
25	S-SC	0.7720	0.7720	0.8451	**********	0.6990	0.8451	0.8451	0.7720	**********	0.8451
26	S-SN	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
27	S-SR	2.6747	2.2557	2.7197	**********	2.6000	2.2330	2.7993	2.7281	2.7281	2.4337
28	S-V	1.3757	1.5384	1.3857	**********	1.4407	1.7012	1.9589	1.4033	1.2085	1.6393
29	S-W	2.0000	**********	2.0000	**********	**********	**********	**********	2.0000	2.0000	2.0000
30	S-Y	1.1698	1.1910	1.1910	**********	1.0000	1.3380	1.3920	1.1690	1.0704	1.3333
31	S-ZN	2.8253	2.7750	2.8323	**********	3.0957	2.8266	2.9133	2.8251	3.1532	2.9509
32	S-ZR	1.6430	1.5963	1.6360	**********	1.6990	1.6200	1.4300	1.6626	1.6360	1.7477
33	S-TH	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
34	AA-AU-P	-0.2486	-0.3539	-0.1937	**********	-0.6403	-0.6990	**********	-0.3993	-0.3979	0.2435
35	INST-HG	-0.3091	-0.3458	-0.2672	**********	-0.4782	-0.3491	-0.2123	-0.3402	-0.1115	-0.1430
36	AA-AS-P	1.7826	1.5830	1.7820	**********	2.0863	1.8753	1.6964	1.8489	1.7340	2.0601
37	AA-ZN-P	2.3557	2.1154	2.3399	**********	2.9401	1.9650	2.0976	2.3626	2.2599	2.3483
38	AA-SB-P	1.2606	0.9330	1.2571	**********	1.7981	0.8039	1.0443	1.3330	1.1689	1.3668

DU101 CORRELATION ANALYSIS - USGS STATPAC (01/15/82) DATE 7/20/84

ARRAY OF MEANS - CONT.

		21 S-NB	22 S-NI	23 S-PB	24 S-SB	25 S-SC	26 S-SN	27 S-SR	28 S-V	29 S-W	30 S-Y
1	X-COORD.	**********	4.6263	4.6284	4.6301	4.6134	**********	4.6291	4.6276	4.6322	4.6231
2	Y-COORD.	**********	5.6201	5.6201	5.6201	5.6207	**********	5.6200	5.6205	5.6210	5.6207
3	S-FE%	**********	0.1695	-0.1186	-0.2500	0.5880	**********	-0.1843	-0.0489	0.5106	0.1246
4	S-MG%	**********	-0.8724	-1.1996	-1.3993	-1.0000	**********	-1.3514	-1.0265	-1.6990	-1.0627
5	S-CA%	**********	0.1527	-0.0229	-0.0523	-0.2614	**********	0.1151	-0.1145	-0.3389	-0.2422
6	S-TI%	**********	-1.2388	-1.5239	-1.8686	-0.9120	**********	-1.5773	-1.4018	-2.0000	-1.1398
7	S-MN	**********	2.4926	2.7026	3.1168	1.7386	**********	2.6653	2.6477	2.5000	2.7500
8	S-AG	**********	1.3122	1.6673	2.1305	1.0000	**********	1.8379	1.5841	2.2720	1.2663
9	S-AS	**********	2.4602	2.6690	2.5293	3.1990	**********	2.8194	2.6653	**********	2.8860
10	S-AU	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
11	S-B	**********	1.7060	1.4908	1.5359	1.6611	**********	1.5139	1.5205	1.8451	1.4333
12	S-BA	**********	2.4012	2.6403	3.1382	2.3495	**********	2.8807	2.5596	**********	2.5979
13	S-BE	**********	0.8997	1.1773	1.6394	0.1761	**********	1.3364	1.0921	2.0000	0.9274
14	S-BI	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
15	S-CD	**********	1.8891	1.6067	1.6931	1.4771	**********	1.6067	1.7518	**********	1.4771
16	S-CO	**********	0.9889	1.0335	1.3010	1.0000	**********	1.0000	1.0335	**********	1.0608
17	S-CR	**********	1.2755	1.2362	1.0000	2.0000	**********	1.3333	1.2755	**********	1.4924
18	S-CU	**********	1.9701	1.9286	2.0052	2.8266	**********	1.8121	2.0317	1.6761	2.0869
19	S-LA	**********	1.3597	1.4054	1.4399	**********	**********	1.3513	1.4158	1.4771	1.4954
20	S-MO	**********	1.0533	1.2327	1.0595	1.4771	**********	1.4214	1.3242	1.0000	1.2177
21	S-NB	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
22	S-NI	**********	1.1134	1.1134	0.8176	1.6990	**********	1.0608	1.1378	0.8451	1.3592
23	S-PB	**********	2.1357	2.2720	2.5694	2.1990	**********	2.4664	2.2507	2.6611	1.9638
24	S-SB	**********	2.1556	2.1587	2.1676	**********	**********	2.1602	2.1528	2.1505	2.1003
25	S-SC	**********	0.8451	0.7720	**********	0.7720	**********	0.7720	0.7720	**********	0.7720
26	S-SN	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
27	S-SR	**********	2.5000	2.6731	3.0194	2.0000	**********	2.6747	2.7217	3.0000	2.0000
28	S-V	**********	1.5664	1.3803	1.1348	2.1761	**********	1.4734	1.3803	1.1761	1.5706
29	S-W	**********	2.0000	2.0000	2.0000	**********	**********	2.0000	2.0000	2.0000	**********
30	S-Y	**********	1.2704	1.1698	1.0587	1.3495	**********	1.2917	1.1698	**********	1.1698
31	S-ZN	**********	2.7999	2.8155	2.7980	2.6990	**********	2.8138	2.8644	2.5880	2.8746
32	S-ZR	**********	1.6522	1.5963	1.4225	1.7720	**********	1.8108	1.5963	**********	1.5840
33	S-TH	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
34	AA-AU-P	**********	0.6232	-0.0983	-0.3664	-0.5229	**********	-0.6549	-0.0234	**********	-0.5229
35	INST-HG	**********	-0.3834	-0.3009	-0.2289	-0.8328	**********	-0.3560	-0.2966	-0.4257	-0.2169
36	AA-AS-P	**********	1.8439	1.7404	1.8003	2.6021	**********	1.8463	1.7532	2.0769	1.6752
37	AA-ZN-P	**********	2.0946	2.3101	2.4669	2.1761	**********	2.4688	2.2053	2.5792	2.1763
38	AA-SB-P	**********	1.1504	1.2234	1.5362	1.5481	**********	1.3912	1.1807	1.7236	0.9983

ARRAY OF MEANS - CONT.

		31 S-ZN	32 S-ZR	33 S-TH	34 AA-AU-P	35 INST-HG	36 AA-AS-P	37 AA-ZN-P	38 AA-SB-P
1	X-COORD.	4.6280	4.6265	**********	4.6251	4.6285	4.6274	4.6283	4.6289
2	Y-COORD.	5.6201	5.6201	**********	5.6191	5.6201	5.6203	5.6201	5.6201
3	S-FE%	-0.1363	0.1599	**********	-0.2001	-0.1131	-0.1519	-0.0971	-0.1488
4	S-MG%	-1.3463	-0.9112	**********	-1.4005	-1.2044	-1.2785	-1.2193	-1.2146
5	S-CA%	0.1425	-0.3811	**********	0.2644	-0.0229	0.0147	-0.0738	-0.0351
6	S-TI%	-1.6928	-1.1803	**********	-1.8186	-1.5239	-1.6003	-1.5062	-1.5239
7	S-MN	2.8920	2.4176	**********	2.7386	2.7026	2.7449	2.7026	2.7290
8	S-AG	1.9781	0.9713	**********	1.9407	1.6673	1.6985	1.6535	1.7785
9	S-AS	2.7150	2.8997	**********	2.9490	2.7132	2.5579	2.7150	2.6720
10	S-AU	**********	**********	**********	**********	**********	**********	**********	**********
11	S-B	1.5550	1.4863	**********	1.5831	1.4990	1.4999	1.4645	1.4797
12	S-BA	2.7588	2.4483	**********	2.5880	2.6770	2.7368	2.6403	2.6992
13	S-BE	1.4173	0.5403	**********	1.3690	1.1706	1.2427	1.1906	1.2543
14	S-BI	**********	**********	**********	**********	**********	**********	**********	**********
15	S-CD	1.5557	1.4771	**********	1.3597	1.5557	1.5715	1.3891	1.6067
16	S-CO	1.5000	0.9889	**********	1.3010	1.0335	1.0649	1.0335	1.0335
17	S-CR	1.1633	1.3693	**********	**********	1.2362	1.2362	1.2755	1.2462
18	S-CU	2.0927	1.7764	**********	2.0613	1.8652	1.9386	1.9323	1.9286
19	S-LA	1.3262	1.4445	**********	1.3010	1.3967	1.3967	1.4158	1.3967
20	S-MO	0.9908	1.7841	**********	1.2401	1.2679	1.2327	1.2105	1.2812
21	S-NB	**********	**********	**********	**********	**********	**********	**********	**********
22	S-NI	1.1614	1.2817	**********	0.8451	1.1511	1.1077	1.1237	1.1237
23	S-PB	2.6493	1.6850	**********	2.4102	2.2339	2.2720	2.2192	2.2821
24	S-SB	2.1695	2.0000	**********	2.3253	2.1670	2.1676	2.1485	2.1676
25	S-SC	0.6990	0.7720	**********	0.6990	0.7720	0.8451	0.7720	0.7720
26	S-SN	**********	**********	**********	**********	**********	**********	**********	**********
27	S-SR	2.8305	2.0000	**********	2.4247	2.6747	2.7197	2.5999	2.6747
28	S-V	1.3317	1.5738	**********	1.1193	1.3984	1.4095	1.3841	1.3582
29	S-W	2.0000	**********	**********	**********	2.0000	2.0000	2.0000	2.0000
30	S-Y	1.0753	1.2183	**********	1.0000	1.1698	1.1910	1.1698	1.1698
31	S-ZN	2.8253	2.6737	**********	2.8352	2.8253	2.8323	2.7636	2.8155
32	S-ZR	1.7477	1.5963	**********	1.6990	1.5963	1.5330	1.5963	1.5963
33	S-TH	**********	**********	**********	**********	**********	**********	**********	**********
34	AA-AU-P	-0.3993	-0.5229	**********	-0.2486	-0.2486	-0.1937	-0.0983	-0.2486
35	INST-HG	-0.3767	-0.4066	**********	-0.2384	-0.3088	-0.2134	-0.3271	-0.2750
36	AA-AS-P	1.8940	1.5900	**********	2.1810	1.7572	1.7677	1.7180	1.7820
37	AA-ZN-P	2.7139	1.9177	**********	2.4092	2.3220	2.3120	2.3101	2.2873
38	AA-SB-P	1.5119	0.8383	**********	1.6412	1.2217	1.2455	1.1857	1.2456

D0101 CORRELATION ANALYSIS - USGS STATPAC (01/15/82) DATE 7/20/84

ARRAY OF VARIANCES -

		1 X-COORD.	2 Y-COORD.	3 S-FE%	4 S-MG%	5 S-CA%	6 S-TI%	7 S-MN	8 S-AG	9 S-AS	10 S-AU
1	X-COORD.	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	**********
2	Y-COORD.	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	**********
3	S-FE%	0.273	0.273	0.273	0.261	0.270	0.368	0.343	0.292	0.317	**********
4	S-MG%	0.269	0.269	0.269	0.269	0.269	0.311	0.303	0.161	0.131	**********
5	S-CA%	0.631	0.631	0.631	0.659	0.631	0.692	0.562	0.640	0.456	**********
6	S-TI%	0.357	0.357	0.357	0.378	0.353	0.357	0.325	0.394	0.385	**********
7	S-MN	0.471	0.471	0.471	0.531	0.480	0.413	0.471	0.508	0.717	**********
8	S-AG	1.034	1.034	1.034	0.988	1.013	1.002	1.317	1.034	1.110	**********
9	S-AS	0.171	0.171	0.171	0.262	0.171	0.327	0.267	0.171	0.171	**********
10	S-AU	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
11	S-B	0.110	0.110	0.110	0.136	0.110	0.103	0.088	0.108	0.076	**********
12	S-BA	0.329	0.329	0.329	0.355	0.332	0.347	0.243	0.276	0.431	**********
13	S-BE	0.546	0.546	0.546	0.547	0.534	0.490	0.640	0.549	0.653	**********
14	S-BI	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
15	S-CD	0.211	0.211	0.211	0.211	0.211	0.319	0.016	0.211	0.319	**********
16	S-CO	0.122	0.122	0.122	0.122	0.122	0.130	0.122	0.159	0.244	**********
17	S-CR	0.145	0.145	0.145	0.145	0.145	0.161	0.178	0.161	0.250	**********
18	S-CU	0.704	0.704	0.704	0.599	0.704	0.655	0.802	0.671	0.628	**********
19	S-LA	0.024	0.024	0.024	0.033	0.026	0.023	0.029	0.017	0.000	**********
20	S-MO	0.342	0.342	0.342	0.105	0.335	0.401	0.457	0.342	0.088	**********
21	S-NB	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
22	S-NI	0.325	0.325	0.325	0.365	0.325	0.394	0.373	0.395	0.684	**********
23	S-PB	0.717	0.717	0.717	0.581	0.696	0.669	0.769	0.687	0.771	**********
24	S-SB	0.041	0.041	0.041	0.053	0.041	0.065	0.023	0.042	0.032	**********
25	S-SC	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.011	**********
26	S-SN	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
27	S-SR	0.439	0.439	0.439	0.323	0.439	0.672	0.582	0.439	0.502	**********
28	S-V	0.277	0.277	0.277	0.387	0.291	0.328	0.323	0.305	0.679	**********
29	S-W	0.000	0.000	0.000	**********	0.000	**********	0.000	0.000	**********	**********
30	S-Y	0.052	0.052	0.052	0.054	0.052	0.056	0.052	0.059	0.110	**********
31	S-ZN	0.148	0.148	0.148	0.146	0.148	0.143	0.111	0.148	0.222	**********
32	S-ZR	0.152	0.152	0.152	0.170	0.152	0.152	0.152	0.103	0.007	**********
33	S-TH	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
34	AA-AU-P	0.439	0.439	0.439	0.068	0.378	0.315	0.468	0.439	0.466	**********
35	INST-HG	0.279	0.279	0.279	0.318	0.265	0.412	0.322	0.228	0.287	**********
36	AA-AS-P	0.381	0.381	0.381	0.396	0.371	0.373	0.306	0.380	0.039	**********
37	AA-ZN-P	0.383	0.383	0.383	0.346	0.327	0.399	0.399	0.321	0.285	**********
38	AA-SB-P	0.395	0.395	0.395	0.365	0.375	0.499	0.335	0.365	0.209	**********

DG101 CORRELATION ANALYSIS - USGS STATPAC (01/15/82) DATE 7/20/84

ARRAY OF VARIANCES - CONT.

		11 S-B	12 S-BA	13 S-BE	14 S-BI	15 S-CD	16 S-CO	17 S-CR	18 S-CU	19 S-LA	20 S-MO
1	X-COORD.	0.000	0.000	0.000	**********	0.000	0.000	0.000	0.000	0.000	0.000
2	Y-COORD.	0.000	0.000	0.000	**********	0.000	0.000	0.000	0.000	0.000	0.000
3	S-FE%	0.283	0.262	0.280	**********	0.345	0.274	0.472	0.278	0.201	0.391
4	S-MG%	0.278	0.312	0.292	**********	0.127	0.402	0.232	0.276	0.129	0.194
5	S-CA%	0.615	0.658	0.639	**********	0.209	0.377	0.777	0.617	0.803	0.630
6	S-TI%	0.378	0.290	0.384	**********	0.297	0.143	0.137	0.374	0.252	0.291
7	S-MN	0.468	0.583	0.483	**********	0.008	0.512	0.299	0.472	0.402	0.452
8	S-AG	1.034	0.765	1.078	**********	1.074	1.742	0.919	1.087	0.923	1.330
9	S-AS	0.171	0.271	0.046	**********	0.356	0.079	0.053	0.171	0.079	0.057
10	S-AU	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
11	S-B	0.110	0.112	0.114	**********	0.188	0.062	0.179	0.086	0.123	0.136
12	S-BA	0.254	0.329	0.193	**********	0.493	0.262	0.305	0.371	0.204	0.171
13	S-BE	0.546	0.514	0.546	**********	0.535	0.621	0.377	0.599	0.433	0.647
14	S-BI	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
15	S-CD	0.211	0.009	0.262	**********	0.211	**********	0.692	0.262	0.402	0.319
16	S-CO	0.139	0.130	0.139	**********	**********	0.122	0.166	0.122	0.181	0.244
17	S-CR	0.161	0.178	0.161	**********	0.016	0.227	0.145	0.145	**********	0.192
18	S-CU	0.683	0.729	0.712	**********	0.196	1.152	0.869	0.704	0.620	0.982
19	S-LA	0.024	0.033	0.024	**********	0.000	0.016	**********	0.020	0.024	0.000
20	S-MO	0.342	0.496	0.342	**********	0.146	0.045	0.135	0.345	0.610	0.342
21	S-NB	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
22	S-NI	0.356	0.443	0.356	**********	0.000	0.527	0.483	0.325	0.030	0.510
23	S-PB	0.696	0.285	0.718	**********	0.502	0.744	0.725	0.728	1.195	0.837
24	S-SB	0.041	0.078	0.041	**********	0.053	**********	0.045	0.042	0.026	0.066
25	S-SC	0.011	0.011	**********	**********	**********	**********	**********	0.011	**********	**********
26	S-SN	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
27	S-SR	0.439	0.083	0.435	**********	0.439	0.163	0.729	0.481	0.522	0.406
28	S-V	0.290	0.366	0.304	**********	0.127	0.670	0.532	0.298	0.021	0.549
29	S-W	0.000	**********	0.000	**********	**********	**********	**********	0.000	**********	**********
30	S-Y	0.052	0.054	0.054	**********	**********	0.061	0.075	0.059	0.009	0.123
31	S-ZN	0.146	0.091	0.155	**********	0.111	0.244	0.335	0.151	0.121	0.252
32	S-ZR	0.147	0.152	0.167	**********	**********	0.185	0.165	0.122	0.195	0.007
33	S-TH	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
34	AA-AU-P	0.439	0.395	0.526	**********	0.101	**********	**********	0.378	0.634	0.312
35	INST-HG	0.290	0.387	0.252	**********	0.569	0.515	0.401	0.294	0.115	0.245
36	AA-AS-P	0.390	0.381	0.390	**********	0.307	0.332	0.499	0.387	0.368	0.291
37	AA-ZN-P	0.345	0.433	0.354	**********	0.043	0.400	0.404	0.297	0.684	0.506
38	AA-SB-P	0.375	0.328	0.374	**********	0.275	0.241	0.413	0.393	0.421	0.406

D0101 CORRELATION ANALYSIS - USGS STATPAC (01/15/82) DATE 7/20/84

ARRAY OF VARIANCES - CONT.

		21 S-NB	22 S-NI	23 S-PB	24 S-SB	25 S-SC	26 S-SN	27 S-SR	28 S-V	29 S-W	30 S-Y
1	X-COORD.	**********	0.000	0.000	0.000	0.000	**********	0.000	0.000	0.000	0.000
2	Y-COORD.	**********	0.000	0.000	0.000	0.000	**********	0.000	0.000	0.000	0.000
3	S-FE%	**********	0.260	0.283	0.164	0.025	**********	0.266	0.315	0.224	0.327
4	S-MG%	**********	0.329	0.283	0.108	0.181	**********	0.115	0.295	**********	0.208
5	S-CA%	**********	0.648	0.627	0.678	0.137	**********	0.652	0.582	0.068	0.373
6	S-TI%	**********	0.161	0.357	0.361	0.016	**********	0.540	0.257	**********	0.113
7	S-MN	**********	0.513	0.471	0.234	0.633	**********	0.575	0.492	0.079	0.669
8	S-AG	**********	1.266	1.051	0.551	0.977	**********	0.698	1.265	0.365	1.148
9	S-AS	**********	0.048	0.192	0.039	0.500	**********	0.271	0.220	**********	0.347
10	S-AU	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
11	S-B	**********	0.076	0.112	0.118	0.068	**********	0.131	0.090	0.000	0.079
12	S-BA	**********	0.191	0.323	0.209	0.846	**********	0.333	0.347	**********	0.253
13	S-BE	**********	0.744	0.542	0.200	**********	**********	0.364	0.634	0.000	0.663
14	S-BI	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
15	S-CD	**********	0.692	0.245	0.461	**********	**********	0.245	0.402	**********	**********
16	S-CO	**********	0.130	0.122	**********	**********	**********	0.091	0.122	**********	0.196
17	S-CR	**********	0.161	0.145	0.000	**********	**********	0.333	0.161	**********	0.250
18	S-CU	**********	0.947	0.726	0.580	0.846	**********	0.594	0.768	0.500	0.983
19	S-LA	**********	0.010	0.026	0.035	**********	**********	0.007	0.027	**********	0.040
20	S-MO	**********	0.112	0.342	0.091	**********	**********	0.480	0.418	**********	0.058
21	S-NB	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
22	S-NI	**********	0.325	0.325	0.016	**********	**********	0.196	0.349	**********	0.728
23	S-PB	**********	0.648	0.717	0.643	0.500	**********	0.594	0.879	0.068	0.833
24	S-SB	**********	0.023	0.042	0.041	**********	**********	0.056	0.023	0.045	0.030
25	S-SC	**********	**********	0.011	**********	0.011	**********	0.011	0.011	**********	0.011
26	S-SN	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
27	S-SR	**********	0.659	0.470	0.366	0.000	**********	0.439	0.619	0.977	0.000
28	S-V	**********	0.477	0.277	0.024	2.000	**********	0.431	0.277	**********	0.554
29	S-W	**********	**********	0.000	0.000	**********	**********	0.000	**********	0.000	**********
30	S-Y	**********	0.069	0.052	0.010	0.244	**********	0.132	0.052	**********	0.052
31	S-ZN	**********	0.262	0.154	0.151	**********	**********	0.148	0.188	0.025	0.184
32	S-ZR	**********	0.162	0.152	0.357	0.011	**********	0.021	0.152	**********	0.170
33	S-TH	**********	**********	**********	**********	**********	**********	**********	**********	**********	**********
34	AA-AU-P	**********	**********	0.379	0.497	**********	**********	0.068	0.408	**********	**********
35	INST-HG	**********	0.438	0.288	0.098	0.639	**********	0.172	0.345	0.010	0.331
36	AA-AS-P	**********	0.319	0.375	0.459	**********	**********	0.358	0.387	0.020	0.505
37	AA-ZN-P	**********	0.274	0.383	0.212	0.547	**********	0.259	0.420	0.021	0.389
38	AA-SB-P	**********	0.449	0.396	0.333	0.237	**********	0.379	0.450	0.153	0.220

D0101 CORRELATION ANALYSIS - USGS STATPAC (01/15/82) DATE 7/20/84

ARRAY OF VARIANCES - CONT.

		31 S-ZN	32 S-ZR	33 S-TH	34 AA-AU-P	35 INST-HG	36 AA-AS-P	37 AA-ZN-P	38 AA-SB-P
1	X-COORD.	0.000	0.000	**********	0.000	0.000	0.000	0.000	0.000
2	Y-COORD.	0.000	0.000	**********	0.000	0.000	0.000	0.000	0.000
3	S-FE%	0.320	0.264	**********	0.173	0.283	0.273	0.280	0.248
4	S-MG%	0.698	0.389	**********	0.040	0.269	0.167	0.290	0.281
5	S-CA%	0.615	0.456	**********	0.392	0.627	0.680	0.580	0.601
6	S-TI%	0.397	0.122	**********	0.508	0.357	0.348	0.374	0.380
7	S-MN	0.369	0.499	**********	0.339	0.471	0.503	0.471	0.480
8	S-AG	0.938	0.648	**********	1.271	1.051	1.078	1.092	0.904
9	S-AS	0.198	0.519	**********	0.250	0.173	0.046	0.198	0.171
10	S-AU	**********	**********	**********	**********	**********	**********	**********	**********
11	S-B	0.127	0.066	**********	0.102	0.114	0.119	0.097	0.104
12	S-BA	0.394	0.277	**********	0.605	0.329	0.305	0.323	0.340
13	S-BE	0.392	0.354	**********	0.580	0.529	0.534	0.559	0.507
14	S-BI	**********	**********	**********	**********	**********	**********	**********	**********
15	S-CD	0.211	**********	**********	0.010	0.211	0.262	0.010	0.245
16	S-CO	0.079	0.130	**********	**********	0.122	0.139	0.122	0.122
17	S-CR	0.051	0.227	**********	**********	0.145	0.145	0.161	0.173
18	S-CU	0.425	0.997	**********	0.724	0.681	0.726	0.758	0.726
19	S-LA	0.004	0.036	**********	0.000	0.024	0.024	0.027	0.024
20	S-MO	0.060	0.650	**********	0.331	0.360	0.342	0.370	0.345
21	S-NB	**********	**********	**********	**********	**********	**********	**********	**********
22	S-NI	0.566	0.505	**********	**********	0.338	0.357	0.356	0.356
23	S-PB	0.498	0.331	**********	0.860	0.702	0.759	0.663	0.741
24	S-SB	0.047	0.000	**********	0.082	0.044	0.041	0.044	0.041
25	S-SC	**********	0.011	**********	**********	0.011	**********	0.011	0.011
26	S-SN	**********	**********	**********	**********	**********	**********	**********	**********
27	S-SR	0.406	0.000	**********	0.115	0.439	0.435	0.419	0.439
28	S-V	0.186	0.496	**********	0.022	0.283	0.296	0.291	0.280
29	S-W	0.000	**********	**********	**********	0.000	0.000	0.000	0.000
30	S-Y	0.023	0.056	**********	**********	0.052	0.054	0.052	0.052
31	S-ZN	0.148	0.034	**********	0.119	0.148	0.155	0.112	0.154
32	S-ZR	0.007	0.152	**********	**********	0.152	0.166	0.152	0.152
33	S-TH	**********	**********	**********	**********	**********	**********	**********	**********
34	AA-AU-P	0.578	**********	**********	0.439	0.439	0.526	0.379	0.439
35	INST-HG	0.190	0.487	**********	0.461	0.279	0.167	0.280	0.257
36	AA-AS-P	0.398	0.350	**********	0.460	0.393	0.381	0.377	0.390
37	AA-ZN-P	0.090	0.268	**********	0.720	0.394	0.400	0.383	0.383
38	AA-SB-P	0.289	0.227	**********	0.457	0.394	0.394	0.372	0.395

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COLUMN	VERSUS COLUMN	CORRELATION COEFFICIENT	NO. OF PAIRS
1 (X-COORD.)	2 (Y-COORD.)	-0.3529	29
1 (X-COORD.)	3 (S-FE%)	-0.2707	29
1 (X-COORD.)	4 (S-MG%)	0.3161	21
1 (X-COORD.)	5 (S-CA%)	-0.0628	28
1 (X-COORD.)	6 (S-TI%)	0.0230	18
1 (X-COORD.)	7 (S-MN)	0.2323	21
1 (X-COORD.)	8 (S-AG)	0.5237	26
1 (X-COORD.)	9 (S-AS)	-0.3867	10
1 (X-COORD.)	10 (S-AU)	********	0
1 (X-COORD.)	11 (S-B)	-0.2547	28
1 (X-COORD.)	12 (S-BA)	0.3339	18
1 (X-COORD.)	13 (S-BE)	0.1779	27
1 (X-COORD.)	14 (S-BI)	********	0
1 (X-COORD.)	15 (S-CD)	0.2118	6
1 (X-COORD.)	16 (S-CO)	-0.2579	7
1 (X-COORD.)	17 (S-CR)	-0.4054	7
1 (X-COORD.)	18 (S-CU)	-0.2715	25
1 (X-COORD.)	19 (S-LA)	-0.3861	12
1 (X-COORD.)	20 (S-MO)	0.1934	12
1 (X-COORD.)	21 (S-NB)	********	0
1 (X-COORD.)	22 (S-NI)	-0.2269	12
1 (X-COORD.)	23 (S-PB)	0.1577	28
1 (X-COORD.)	24 (S-SB)	-0.3291	16
1 (X-COORD.)	25 (S-SC)	1.0000	2
1 (X-COORD.)	26 (S-SN)	********	0
1 (X-COORD.)	27 (S-SR)	0.4135	16
1 (X-COORD.)	28 (S-V)	-0.4565	22
1 (X-COORD.)	29 (S-W)	********	2
1 (X-COORD.)	30 (S-Y)	-0.4861	9
1 (X-COORD.)	31 (S-ZN)	0.2415	19
1 (X-COORD.)	32 (S-ZR)	0.4340	10
1 (X-COORD.)	33 (S-TH)	********	0
1 (X-COORD.)	34 (AA-AU-P)	-0.3426	6
1 (X-COORD.)	35 (INST-HG)	-0.3263	28
1 (X-COORD.)	36 (AA-AS-P)	-0.1076	27
1 (X-COORD.)	37 (AA-ZN-P)	0.0504	27
1 (X-COORD.)	38 (AA-SB-P)	-0.0874	28
2 (Y-COORD.)	3 (S-FE%)	-0.0898	29
2 (Y-COORD.)	4 (S-MG%)	-0.1216	21
2 (Y-COORD.)	5 (S-CA%)	-0.1961	28
2 (Y-COORD.)	6 (S-TI%)	0.0932	18
2 (Y-COORD.)	7 (S-MN)	0.1476	21
2 (Y-COORD.)	8 (S-AG)	0.1956	26
2 (Y-COORD.)	9 (S-AS)	0.0207	10
2 (Y-COORD.)	10 (S-AU)	********	0
2 (Y-COORD.)	11 (S-B)	-0.2553	28
2 (Y-COORD.)	12 (S-BA)	-0.1972	18
2 (Y-COORD.)	13 (S-BE)	0.2230	27
2 (Y-COORD.)	14 (S-BI)	********	0
2 (Y-COORD.)	15 (S-CD)	0.3389	6

D0101 CORRELATION ANALYSIS - USGS STATPAC (01/15/82) DATE 7/20/84

COLUMN	VERSUS	COLUMN	CORRELATION COEFFICIENT	NO. OF PAIRS
2 (Y-COORD.)	16	(S-CO)	0.2011	7
2 (Y-COORD.)	17	(S-CR)	-0.3073	7
2 (Y-COORD.)	18	(S-CU)	0.3043	25
2 (Y-COORD.)	19	(S-LA)	0.2319	12
2 (Y-COORD.)	20	(S-MO)	0.0706	12
2 (Y-COORD.)	21	(S-NB)	********	0
2 (Y-COORD.)	22	(S-NI)	-0.1497	12
2 (Y-COORD.)	23	(S-PB)	0.1197	28
2 (Y-COORD.)	24	(S-SB)	-0.6662	16
2 (Y-COORD.)	25	(S-SC)	-1.0000	2
2 (Y-COORD.)	26	(S-SN)	********	0
2 (Y-COORD.)	27	(S-SR)	0.1479	16
2 (Y-COORD.)	28	(S-V)	-0.0142	22
2 (Y-COORD.)	29	(S-W)	********	2
2 (Y-COORD.)	30	(S-Y)	-0.7590	9
2 (Y-COORD.)	31	(S-ZN)	-0.0643	19
2 (Y-COORD.)	32	(S-ZR)	-0.3894	10
2 (Y-COORD.)	33	(S-TH)	********	0
2 (Y-COORD.)	34	(AA-AU-P)	0.1821	6
2 (Y-COORD.)	35	(INST-HG)	0.0872	28
2 (Y-COORD.)	36	(AA-AS-P)	-0.2772	27
2 (Y-COORD.)	37	(AA-ZN-P)	-0.1261	27
2 (Y-COORD.)	38	(AA-SB-P)	-0.1351	28
3 (S-FE%)	4	(S-MG%)	0.4318	21
3 (S-FE%)	5	(S-CA%)	0.0185	28
3 (S-FE%)	6	(S-TI%)	0.3453	18
3 (S-FE%)	7	(S-MN)	-0.5519	21
3 (S-FE%)	8	(S-AG)	-0.5066	26
3 (S-FE%)	9	(S-AS)	0.1677	10
3 (S-FE%)	10	(S-AU)	********	0
3 (S-FE%)	11	(S-B)	0.4888	28
3 (S-FE%)	12	(S-BA)	-0.2229	18
3 (S-FE%)	13	(S-BE)	-0.3623	27
3 (S-FE%)	14	(S-BI)	********	0
3 (S-FE%)	15	(S-CD)	-0.6044	6
3 (S-FE%)	16	(S-CO)	0.3506	7
3 (S-FE%)	17	(S-CR)	0.5975	7
3 (S-FE%)	18	(S-CU)	0.0386	25
3 (S-FE%)	19	(S-LA)	0.2966	12
3 (S-FE%)	20	(S-MO)	-0.2666	12
3 (S-FE%)	21	(S-NB)	********	0
3 (S-FE%)	22	(S-NI)	0.6643	12
3 (S-FE%)	23	(S-PB)	-0.3089	28
3 (S-FE%)	24	(S-SB)	0.3215	16
3 (S-FE%)	25	(S-SC)	1.0000	2
3 (S-FE%)	26	(S-SN)	********	0
3 (S-FE%)	27	(S-SR)	-0.2922	16
3 (S-FE%)	28	(S-V)	0.5549	22
3 (S-FE%)	29	(S-W)	********	2
3 (S-FE%)	30	(S-Y)	0.5691	9

D0101 CORRELATION ANALYSIS - USGS STATPAC (01/15/82) DATE 7/20/84

COLUMN	VERSUS	COLUMN	CORRELATION COEFFICIENT	NO. OF PAIRS
3 (S-FE%)	31	(S-ZN)	-0.2874	19
3 (S-FE%)	32	(S-ZR)	0.2481	10
3 (S-FE%)	33	(S-TH)	********	0
3 (S-FE%)	34	(AA-AU-P)	-0.4806	6
3 (S-FE%)	35	(INST-HG)	-0.3396	28
3 (S-FE%)	36	(AA-AS-P)	0.1679	27
3 (S-FE%)	37	(AA-ZN-P)	-0.0041	27
3 (S-FE%)	38	(AA-SB-P)	-0.0314	28
4 (S-MG%)	5	(S-CA%)	0.0246	21
4 (S-MG%)	6	(S-TI%)	0.5777	14
4 (S-MG%)	7	(S-MN)	-0.2937	15
4 (S-MG%)	8	(S-AG)	-0.3392	18
4 (S-MG%)	9	(S-AS)	-0.2980	6
4 (S-MG%)	10	(S-AU)	********	0
4 (S-MG%)	11	(S-B)	0.2990	20
4 (S-MG%)	12	(S-BA)	-0.2192	16
4 (S-MG%)	13	(S-BE)	-0.5604	19
4 (S-MG%)	14	(S-BI)	********	0
4 (S-MG%)	15	(S-CD)	0.6052	6
4 (S-MG%)	16	(S-CO)	-0.3549	7
4 (S-MG%)	17	(S-CR)	0.2499	7
4 (S-MG%)	18	(S-CU)	0.1575	18
4 (S-MG%)	19	(S-LA)	-0.4881	8
4 (S-MG%)	20	(S-MO)	0.5461	7
4 (S-MG%)	21	(S-NB)	********	0
4 (S-MG%)	22	(S-NI)	-0.0001	10
4 (S-MG%)	23	(S-PB)	0.0008	20
4 (S-MG%)	24	(S-SB)	-0.0581	11
4 (S-MG%)	25	(S-SC)	1.0000	2
4 (S-MG%)	26	(S-SN)	********	0
4 (S-MG%)	27	(S-SR)	0.1401	13
4 (S-MG%)	28	(S-V)	0.0881	14
4 (S-MG%)	29	(S-W)	********	1
4 (S-MG%)	30	(S-Y)	0.3490	8
4 (S-MG%)	31	(S-ZN)	0.4432	14
4 (S-MG%)	32	(S-ZR)	0.4021	9
4 (S-MG%)	33	(S-TH)	********	0
4 (S-MG%)	34	(AA-AU-P)	-0.6563	4
4 (S-MG%)	35	(INST-HG)	-0.2125	21
4 (S-MG%)	36	(AA-AS-P)	0.1282	19
4 (S-MG%)	37	(AA-ZN-P)	-0.2469	19
4 (S-MG%)	38	(AA-SB-P)	-0.1145	20
5 (S-CA%)	6	(S-TI%)	0.1290	17
5 (S-CA%)	7	(S-MN)	0.1445	20
5 (S-CA%)	8	(S-AG)	-0.1125	25
5 (S-CA%)	9	(S-AS)	-0.2140	10
5 (S-CA%)	10	(S-AU)	********	0
5 (S-CA%)	11	(S-B)	0.1658	27
5 (S-CA%)	12	(S-BA)	0.1802	17
5 (S-CA%)	13	(S-BE)	-0.1566	26

00101 CORRELATION ANALYSIS - USGS STATPAC (01/15/82) DATE 7/20/84

COLUMN	VERSUS	COLUMN	CORRELATION COEFFICIENT	NO. OF PAIRS
5 (S-CA%)	14	(S-BI)	********	0
5 (S-CA%)	15	(S-CD)	0.4181	6
5 (S-CA%)	16	(S-CO)	-0.2687	7
5 (S-CA%)	17	(S-CR)	-0.4517	7
5 (S-CA%)	18	(S-CU)	-0.0239	25
5 (S-CA%)	19	(S-LA)	-0.3005	11
5 (S-CA%)	20	(S-MO)	-0.6950	11
5 (S-CA%)	21	(S-NB)	********	0
5 (S-CA%)	22	(S-NI)	-0.1910	12
5 (S-CA%)	23	(S-PB)	0.1810	27
5 (S-CA%)	24	(S-SB)	0.3657	16
5 (S-CA%)	25	(S-SC)	-1.0000	2
5 (S-CA%)	26	(S-SN)	********	0
5 (S-CA%)	27	(S-SR)	-0.0013	16
5 (S-CA%)	28	(S-V)	-0.0042	21
5 (S-CA%)	29	(S-W)	********	2
5 (S-CA%)	30	(S-Y)	0.0378	9
5 (S-CA%)	31	(S-ZN)	0.1721	19
5 (S-CA%)	32	(S-ZR)	-0.0070	10
5 (S-CA%)	33	(S-TH)	********	0
5 (S-CA%)	34	(AA-AU-P)	0.1238	5
5 (S-CA%)	35	(INST-HG)	-0.0600	27
5 (S-CA%)	36	(AA-AS-P)	0.1123	26
5 (S-CA%)	37	(AA-ZN-P)	0.2576	26
5 (S-CA%)	38	(AA-SB-P)	0.2401	27
6 (S-TI%)	7	(S-MN)	0.0133	15
6 (S-TI%)	8	(S-AG)	-0.1821	15
6 (S-TI%)	9	(S-AS)	0.3348	5
6 (S-TI%)	10	(S-AU)	********	0
6 (S-TI%)	11	(S-B)	-0.0475	17
6 (S-TI%)	12	(S-BA)	-0.2982	14
6 (S-TI%)	13	(S-BE)	-0.3983	16
6 (S-TI%)	14	(S-BI)	********	0
6 (S-TI%)	15	(S-CD)	-0.0800	4
6 (S-TI%)	16	(S-CO)	-0.1128	6
6 (S-TI%)	17	(S-CR)	0.8775	6
6 (S-TI%)	18	(S-CU)	0.1514	16
6 (S-TI%)	19	(S-LA)	0.0547	7
6 (S-TI%)	20	(S-MO)	0.0852	7
6 (S-TI%)	21	(S-NB)	********	0
6 (S-TI%)	22	(S-NI)	0.1797	9
6 (S-TI%)	23	(S-PB)	-0.1207	18
6 (S-TI%)	24	(S-SB)	-0.3053	8
6 (S-TI%)	25	(S-SC)	1.0000	2
6 (S-TI%)	26	(S-SN)	********	0
6 (S-TI%)	27	(S-SR)	-0.4586	10
6 (S-TI%)	28	(S-V)	0.2269	16
6 (S-TI%)	29	(S-W)	********	1
6 (S-TI%)	30	(S-Y)	0.3486	7
6 (S-TI%)	31	(S-ZN)	-0.0388	10

DC101 CORRELATION ANALYSIS - USGS STATPAC (01/15/82) DATE 7/20/84

COLUMN	VERSUS	COLUMN	CORRELATION COEFFICIENT	NO. OF PAIRS
6 (S-TI%)	32	(S-ZR)	0.8185	10
6 (S-TI%)	33	(S-TH)	********	0
6 (S-TI%)	34	(AA-AU-P)	-0.5077	3
6 (S-TI%)	35	(INST-HG)	-0.4366	18
6 (S-TI%)	36	(AA-AS-P)	0.1380	16
6 (S-TI%)	37	(AA-ZN-P)	-0.1035	17
6 (S-TI%)	38	(AA-SB-P)	-0.1639	17
7 (S-MN)	8	(S-AG)	0.5891	18
7 (S-MN)	9	(S-AS)	0.1138	5
7 (S-MN)	10	(S-AU)	********	0
7 (S-MN)	11	(S-B)	-0.5388	20
7 (S-MN)	12	(S-BA)	0.2442	14
7 (S-MN)	13	(S-BE)	0.6697	19
7 (S-MN)	14	(S-BI)	********	0
7 (S-MN)	15	(S-CD)	1.0000	2
7 (S-MN)	16	(S-CO)	-0.0980	7
7 (S-MN)	17	(S-CR)	-0.8769	5
7 (S-MN)	18	(S-CU)	-0.0181	18
7 (S-MN)	19	(S-LA)	0.2749	9
7 (S-MN)	20	(S-MO)	-0.4678	8
7 (S-MN)	21	(S-NB)	********	0
7 (S-MN)	22	(S-NI)	-0.6205	10
7 (S-MN)	23	(S-PB)	0.4345	21
7 (S-MN)	24	(S-SB)	-0.0900	9
7 (S-MN)	25	(S-SC)	-1.0000	2
7 (S-MN)	26	(S-SN)	********	0
7 (S-MN)	27	(S-SR)	0.3042	10
7 (S-MN)	28	(S-V)	-0.6940	18
7 (S-MN)	29	(S-W)	********	2
7 (S-MN)	30	(S-Y)	-0.8390	9
7 (S-MN)	31	(S-ZN)	0.1203	12
7 (S-MN)	32	(S-ZR)	-0.0965	10
7 (S-MN)	33	(S-TH)	********	0
7 (S-MN)	34	(AA-AU-P)	-0.1473	4
7 (S-MN)	35	(INST-HG)	0.1209	21
7 (S-MN)	36	(AA-AS-P)	-0.2320	19
7 (S-MN)	37	(AA-ZN-P)	0.3781	21
7 (S-MN)	38	(AA-SB-P)	0.2208	20
8 (S-AG)	9	(S-AS)	0.0750	10
8 (S-AG)	10	(S-AU)	********	0
8 (S-AG)	11	(S-B)	-0.1897	26
8 (S-AG)	12	(S-BA)	0.1321	15
8 (S-AG)	13	(S-BE)	0.8280	25
8 (S-AG)	14	(S-BI)	********	0
8 (S-AG)	15	(S-CD)	0.3227	6
8 (S-AG)	16	(S-CO)	0.0686	5
8 (S-AG)	17	(S-CR)	-0.4472	6
8 (S-AG)	18	(S-CU)	0.3667	23
8 (S-AG)	19	(S-LA)	-0.3157	11
8 (S-AG)	20	(S-MO)	-0.3520	12

D0101 CORRELATION ANALYSIS - USGS STATPAC (01/15/82) DATE 7/20/84

COLUMN	VERSUS	COLUMN	CORRELATION COEFFICIENT	NO. OF PAIRS
8 (S-AG)	21	(S-NB)	********	0
8 (S-AG)	22	(S-NI)	-0.5600	10
8 (S-AG)	23	(S-PB)	0.8207	25
8 (S-AG)	24	(S-SB)	-0.3182	15
8 (S-AG)	25	(S-SC)	-1.0000	2
8 (S-AG)	26	(S-SN)	********	0
8 (S-AG)	27	(S-SR)	0.5993	16
8 (S-AG)	28	(S-V)	-0.6645	19
8 (S-AG)	29	(S-W)	********	2
8 (S-AG)	30	(S-Y)	-0.6528	8
8 (S-AG)	31	(S-ZN)	0.2193	19
8 (S-AG)	32	(S-ZR)	0.4035	7
8 (S-AG)	33	(S-TH)	********	0
8 (S-AG)	34	(AA-AU-P)	-0.2947	6
8 (S-AG)	35	(INST-HG)	-0.0965	25
8 (S-AG)	36	(AA-AS-P)	0.3254	25
8 (S-AG)	37	(AA-ZN-P)	0.4977	24
8 (S-AG)	38	(AA-SB-P)	0.6016	25
9 (S-AS)	10	(S-AU)	********	0
9 (S-AS)	11	(S-B)	-0.3761	10
9 (S-AS)	12	(S-BA)	-0.6801	5
9 (S-AS)	13	(S-BE)	0.1652	9
9 (S-AS)	14	(S-BI)	********	0
9 (S-AS)	15	(S-CD)	-0.4901	4
9 (S-AS)	16	(S-CO)	-1.0000	2
9 (S-AS)	17	(S-CR)	0.8789	3
9 (S-AS)	18	(S-CU)	-0.1461	10
9 (S-AS)	19	(S-LA)	********	3
9 (S-AS)	20	(S-MO)	-0.1676	7
9 (S-AS)	21	(S-NB)	********	0
9 (S-AS)	22	(S-NI)	-0.1285	5
9 (S-AS)	23	(S-PB)	0.0134	9
9 (S-AS)	24	(S-SB)	0.5434	6
9 (S-AS)	25	(S-SC)	-1.0000	2
9 (S-AS)	26	(S-SN)	********	0
9 (S-AS)	27	(S-SR)	-0.6778	5
9 (S-AS)	28	(S-V)	-0.1335	8
9 (S-AS)	29	(S-W)	********	0
9 (S-AS)	30	(S-Y)	-0.5245	4
9 (S-AS)	31	(S-ZN)	-0.2016	8
9 (S-AS)	32	(S-ZR)	-0.2413	3
9 (S-AS)	33	(S-TH)	********	0
9 (S-AS)	34	(AA-AU-P)	-0.1938	4
9 (S-AS)	35	(INST-HG)	-0.7513	9
9 (S-AS)	36	(AA-AS-P)	0.8808	9
9 (S-AS)	37	(AA-ZN-P)	0.2590	8
9 (S-AS)	38	(AA-SB-P)	0.1120	10
10 (S-AU)	11	(S-B)	********	0
10 (S-AU)	12	(S-BA)	********	0
10 (S-AU)	13	(S-BE)	********	0

D01U1 CORRELATION ANALYSIS - USGS STATPAC (01/15/82) DATE 7/20/84

COLUMN	VERSUS	COLUMN	CORRELATION COEFFICIENT	NO. OF PAIRS
10 (S-AU)	14	(S-BI)	********	0
10 (S-AU)	15	(S-CD)	********	0
10 (S-AU)	16	(S-CO)	********	0
10 (S-AU)	17	(S-CR)	********	0
10 (S-AU)	18	(S-CU)	********	0
10 (S-AU)	19	(S-LA)	********	0
10 (S-AU)	20	(S-MO)	********	0
10 (S-AU)	21	(S-NB)	********	0
10 (S-AU)	22	(S-NI)	********	0
10 (S-AU)	23	(S-PB)	********	0
10 (S-AU)	24	(S-SB)	********	0
10 (S-AU)	25	(S-SC)	********	0
10 (S-AU)	26	(S-SN)	********	0
10 (S-AU)	27	(S-SR)	********	0
10 (S-AU)	28	(S-V)	********	0
10 (S-AU)	29	(S-W)	********	0
10 (S-AU)	30	(S-Y)	********	0
10 (S-AU)	31	(S-ZN)	********	0
10 (S-AU)	32	(S-ZR)	********	0
10 (S-AU)	33	(S-TH)	********	0
10 (S-AU)	34	(AA-AU-P)	********	0
10 (S-AU)	35	(INST-HG)	********	0
10 (S-AU)	36	(AA-AS-P)	********	0
10 (S-AU)	37	(AA-ZN-P)	********	0
10 (S-AU)	38	(AA-SB-P)	********	0
11 (S-B)	12	(S-BA)	-0.1322	17
11 (S-B)	13	(S-BE)	-0.1859	27
11 (S-B)	14	(S-BI)	********	0
11 (S-B)	15	(S-CD)	0.3595	6
11 (S-B)	16	(S-CO)	0.5028	6
11 (S-B)	17	(S-CR)	0.2685	6
11 (S-B)	18	(S-CU)	0.1628	24
11 (S-B)	19	(S-LA)	-0.3315	12
11 (S-B)	20	(S-MO)	-0.1008	12
11 (S-B)	21	(S-NB)	********	0
11 (S-B)	22	(S-NI)	0.3104	11
11 (S-B)	23	(S-PB)	0.1908	27
11 (S-B)	24	(S-SB)	0.5909	16
11 (S-B)	25	(S-SC)	1.0000	2
11 (S-B)	26	(S-SN)	********	0
11 (S-B)	27	(S-SR)	0.2700	16
11 (S-B)	28	(S-V)	0.4357	21
11 (S-B)	29	(S-W)	********	2
11 (S-B)	30	(S-Y)	0.6255	9
11 (S-B)	31	(S-ZN)	0.1693	19
11 (S-B)	32	(S-ZR)	0.4303	9
11 (S-B)	33	(S-TH)	********	0
11 (S-B)	34	(AA-AU-P)	-0.0675	6
11 (S-B)	35	(INST-HG)	-0.0016	27
11 (S-B)	36	(AA-AS-P)	0.6045	26

DC1U1 CORRELATION ANALYSIS - USGS STATPAC (01/15/82) DATE 7/20/84

COLUMN	VERSUS	COLUMN	CORRELATION COEFFICIENT	NO. OF PAIRS
11 (S-B)	37	(AA-ZN-P)	0.1797	26
11 (S-B)	38	(AA-SB-P)	0.5850	27
12 (S-BA)	13	(S-BE)	0.5320	16
12 (S-BA)	14	(S-BI)	********	0
12 (S-BA)	15	(S-CD)	-0.3812	5
12 (S-BA)	16	(S-CO)	0.1274	6
12 (S-BA)	17	(S-CR)	0.7598	5
12 (S-BA)	18	(S-CU)	-0.0244	14
12 (S-BA)	19	(S-LA)	0.4060	8
12 (S-BA)	20	(S-MO)	-0.1842	7
12 (S-BA)	21	(S-NB)	********	0
12 (S-BA)	22	(S-NI)	0.2981	8
12 (S-BA)	23	(S-PB)	-0.0112	17
12 (S-BA)	24	(S-SB)	0.1364	6
12 (S-BA)	25	(S-SC)	1.0000	2
12 (S-BA)	26	(S-SN)	********	0
12 (S-BA)	27	(S-SR)	0.7459	9
12 (S-BA)	28	(S-V)	0.0958	14
12 (S-BA)	29	(S-W)	********	0
12 (S-BA)	30	(S-Y)	0.3704	8
12 (S-BA)	31	(S-ZN)	-0.0100	9
12 (S-BA)	32	(S-ZR)	0.0662	10
12 (S-BA)	33	(S-TH)	********	0
12 (S-BA)	34	(AA-AL-P)	-0.4705	4
12 (S-BA)	35	(INST-HG)	0.2039	18
12 (S-BA)	36	(AA-AS-P)	0.1535	16
12 (S-BA)	37	(AA-ZN-P)	0.2124	17
12 (S-BA)	38	(AA-SB-P)	0.1233	17
13 (S-BE)	14	(S-BI)	********	0
13 (S-BE)	15	(S-CD)	-0.0847	5
13 (S-BE)	16	(S-CO)	0.0197	6
13 (S-BE)	17	(S-CR)	-0.4161	6
13 (S-BE)	18	(S-CU)	0.1679	23
13 (S-BE)	19	(S-LA)	0.1153	12
13 (S-BE)	20	(S-MO)	-0.4787	12
13 (S-BE)	21	(S-NB)	********	0
13 (S-BE)	22	(S-NI)	-0.6004	11
13 (S-BE)	23	(S-PB)	0.6109	26
13 (S-BE)	24	(S-SB)	-0.2168	16
13 (S-BE)	25	(S-SC)	********	1
13 (S-BE)	26	(S-SN)	********	0
13 (S-BE)	27	(S-SR)	0.4578	15
13 (S-BE)	28	(S-V)	-0.5980	20
13 (S-BE)	29	(S-W)	********	2
13 (S-BE)	30	(S-Y)	-0.7299	8
13 (S-BE)	31	(S-ZN)	-0.0768	18
13 (S-BE)	32	(S-ZR)	0.2039	8
13 (S-BE)	33	(S-TH)	********	0
13 (S-BE)	34	(AA-AL-P)	-0.5421	5
13 (S-BE)	35	(INST-HG)	-0.0418	26

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COLUMN	VERSUS	COLUMN	CORRELATION COEFFICIENT	NO. OF PAIRS
13 (S-BE)	36	(AA-AS-P)	0.1373	26
13 (S-BE)	37	(AA-ZN-P)	0.4297	25
13 (S-BE)	38	(AA-SB-P)	0.5120	26
14 (S-BI)	15	(S-CD)	********	0
14 (S-BI)	16	(S-CO)	********	0
14 (S-BI)	17	(S-CR)	********	0
14 (S-BI)	18	(S-CU)	********	0
14 (S-BI)	19	(S-LA)	********	0
14 (S-BI)	20	(S-MO)	********	0
14 (S-BI)	21	(S-NB)	********	0
14 (S-BI)	22	(S-NI)	********	0
14 (S-BI)	23	(S-PB)	********	0
14 (S-BI)	24	(S-SB)	********	0
14 (S-BI)	25	(S-SC)	********	0
14 (S-BI)	26	(S-SN)	********	0
14 (S-BI)	27	(S-SR)	********	0
14 (S-BI)	28	(S-V)	********	0
14 (S-BI)	29	(S-W)	********	0
14 (S-BI)	30	(S-Y)	********	0
14 (S-BI)	31	(S-ZN)	********	0
14 (S-BI)	32	(S-ZR)	********	0
14 (S-BI)	33	(S-TH)	********	0
14 (S-BI)	34	(AA-AL-P)	********	0
14 (S-BI)	35	(INST-HG)	********	0
14 (S-BI)	36	(AA-AS-P)	********	0
14 (S-BI)	37	(AA-ZN-P)	********	0
14 (S-BI)	38	(AA-SB-P)	********	0
15 (S-CD)	16	(S-CO)	********	0
15 (S-CD)	17	(S-CR)	-1.0000	2
15 (S-CD)	18	(S-CU)	0.4377	5
15 (S-CD)	19	(S-LA)	********	3
15 (S-CD)	20	(S-MO)	0.7570	4
15 (S-CD)	21	(S-NB)	********	0
15 (S-CD)	22	(S-NI)	********	2
15 (S-CD)	23	(S-PB)	0.9626	5
15 (S-CD)	24	(S-SB)	-0.5000	3
15 (S-CD)	25	(S-SC)	********	1
15 (S-CD)	26	(S-SN)	********	0
15 (S-CD)	27	(S-SR)	0.8654	5
15 (S-CD)	28	(S-V)	-0.4674	3
15 (S-CD)	29	(S-W)	********	0
15 (S-CD)	30	(S-Y)	********	1
15 (S-CD)	31	(S-ZN)	0.8539	6
15 (S-CD)	32	(S-ZR)	********	1
15 (S-CD)	33	(S-TH)	********	0
15 (S-CD)	34	(AA-AL-P)	0.3200	3
15 (S-CD)	35	(INST-HG)	0.4902	6
15 (S-CD)	36	(AA-AS-P)	0.1474	5
15 (S-CD)	37	(AA-ZN-P)	0.0636	4
15 (S-CD)	38	(AA-SB-P)	0.3247	5

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COLUMN	VERSUS	COLUMN	CORRELATION COEFFICIENT	NO. OF PAIRS
16 (S-CO)	17	(S-CR)	0.3254	4
16 (S-CO)	18	(S-CU)	0.6799	7
16 (S-CO)	19	(S-LA)	-1.0000	2
16 (S-CO)	20	(S-MO)	-1.0000	2
16 (S-CO)	21	(S-NB)	********	0
16 (S-CO)	22	(S-NI)	0.9747	6
16 (S-CO)	23	(S-PB)	0.2526	7
16 (S-CO)	24	(S-SB)	********	1
16 (S-CO)	25	(S-SC)	********	1
16 (S-CO)	26	(S-SN)	********	0
16 (S-CO)	27	(S-SR)	0.8660	3
16 (S-CO)	28	(S-V)	0.3666	7
16 (S-CO)	29	(S-W)	********	0
16 (S-CO)	30	(S-Y)	0.1457	4
16 (S-CO)	31	(S-ZN)	-1.0000	2
16 (S-CO)	32	(S-ZR)	0.0602	6
16 (S-CO)	33	(S-TH)	********	0
16 (S-CO)	34	(AA-AU-P)	********	1
16 (S-CO)	35	(INST-HG)	0.1061	7
16 (S-CO)	36	(AA-AS-P)	0.6398	6
16 (S-CO)	37	(AA-ZN-P)	0.6982	7
16 (S-CO)	38	(AA-SB-P)	0.4903	7
17 (S-CR)	18	(S-CU)	0.9219	7
17 (S-CR)	19	(S-LA)	********	1
17 (S-CR)	20	(S-MO)	0.3426	4
17 (S-CR)	21	(S-NB)	********	0
17 (S-CR)	22	(S-NI)	0.6093	6
17 (S-CR)	23	(S-PB)	-0.2290	7
17 (S-CR)	24	(S-SB)	********	2
17 (S-CR)	25	(S-SC)	********	1
17 (S-CR)	26	(S-SN)	********	0
17 (S-CR)	27	(S-SR)	-0.8106	3
17 (S-CR)	28	(S-V)	0.9882	6
17 (S-CR)	29	(S-W)	********	0
17 (S-CR)	30	(S-Y)	0.9647	3
17 (S-CR)	31	(S-ZN)	-0.4934	4
17 (S-CR)	32	(S-ZR)	0.9360	4
17 (S-CR)	33	(S-TH)	********	0
17 (S-CR)	34	(AA-AU-P)	********	0
17 (S-CR)	35	(INST-HG)	-0.1905	7
17 (S-CR)	36	(AA-AS-P)	0.7079	7
17 (S-CR)	37	(AA-ZN-P)	-0.1124	6
17 (S-CR)	38	(AA-SB-P)	0.0246	6
18 (S-CU)	19	(S-LA)	-0.5482	9
18 (S-CU)	20	(S-MO)	-0.3926	10
18 (S-CU)	21	(S-NB)	********	0
18 (S-CU)	22	(S-NI)	0.3577	12
18 (S-CU)	23	(S-PB)	0.5437	24
18 (S-CU)	24	(S-SB)	-0.2364	15
18 (S-CU)	25	(S-SC)	1.0000	2

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COLUMN	VERSUS	COLUMN	CORRELATION COEFFICIENT	NO. OF PAIRS
18 (S-CU)	26	(S-SN)	********	0
18 (S-CU)	27	(S-SR)	0.3104	14
18 (S-CU)	28	(S-V)	0.2243	20
18 (S-CU)	29	(S-W)	********	2
18 (S-CU)	30	(S-Y)	0.5185	8
18 (S-CU)	31	(S-ZN)	-0.0286	17
18 (S-CU)	32	(S-ZR)	0.1912	9
18 (S-CU)	33	(S-TH)	********	0
18 (S-CU)	34	(AA-AU-P)	0.6455	5
18 (S-CU)	35	(INST-HG)	0.0310	24
18 (S-CU)	36	(AA-AS-P)	0.4730	23
18 (S-CU)	37	(AA-ZN-P)	0.3541	23
18 (S-CU)	38	(AA-SB-P)	0.4613	24
19 (S-LA)	20	(S-MO)	********	5
19 (S-LA)	21	(S-NB)	********	0
19 (S-LA)	22	(S-NI)	-0.5000	3
19 (S-LA)	23	(S-PB)	-0.5210	11
19 (S-LA)	24	(S-SB)	0.0308	7
19 (S-LA)	25	(S-SC)	********	0
19 (S-LA)	26	(S-SN)	********	0
19 (S-LA)	27	(S-SR)	0.1148	7
19 (S-LA)	28	(S-V)	-0.3945	10
19 (S-LA)	29	(S-W)	********	1
19 (S-LA)	30	(S-Y)	0.4244	5
19 (S-LA)	31	(S-ZN)	-0.5746	7
19 (S-LA)	32	(S-ZR)	-0.7557	4
19 (S-LA)	33	(S-TH)	********	0
19 (S-LA)	34	(AA-AU-P)	********	3
19 (S-LA)	35	(INST-HG)	-0.0167	12
19 (S-LA)	36	(AA-AS-P)	-0.4500	12
19 (S-LA)	37	(AA-ZN-P)	-0.4185	10
19 (S-LA)	38	(AA-SB-P)	-0.3027	12
20 (S-MO)	21	(S-NB)	********	0
20 (S-MO)	22	(S-NI)	0.4401	7
20 (S-MO)	23	(S-PB)	-0.4430	12
20 (S-MO)	24	(S-SB)	0.2912	5
20 (S-MO)	25	(S-SC)	********	1
20 (S-MO)	26	(S-SN)	********	0
20 (S-MO)	27	(S-SR)	-0.1466	6
20 (S-MO)	28	(S-V)	0.1011	9
20 (S-MO)	29	(S-W)	********	1
20 (S-MO)	30	(S-Y)	0.9975	3
20 (S-MO)	31	(S-ZN)	0.3974	8
20 (S-MO)	32	(S-ZR)	-0.3296	3
20 (S-MO)	33	(S-TH)	********	0
20 (S-MO)	34	(AA-AU-P)	-0.0095	3
20 (S-MO)	35	(INST-HG)	0.5141	11
20 (S-MO)	36	(AA-AS-P)	-0.2290	12
20 (S-MO)	37	(AA-ZN-P)	-0.6480	11
20 (S-MO)	38	(AA-SB-P)	-0.4479	11

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COLUMN	VERSUS COLUMN	CORRELATION COEFFICIENT	NO. OF PAIRS
21 (S-NB)	22 (S-NI)	********	0
21 (S-NB)	23 (S-PB)	********	0
21 (S-NB)	24 (S-SB)	********	0
21 (S-NB)	25 (S-SC)	********	0
21 (S-NB)	26 (S-SN)	********	0
21 (S-NB)	27 (S-SR)	********	0
21 (S-NB)	28 (S-V)	********	0
21 (S-NB)	29 (S-W)	********	0
21 (S-NB)	30 (S-Y)	********	0
21 (S-NB)	31 (S-ZN)	********	0
21 (S-NB)	32 (S-ZR)	********	0
21 (S-NB)	33 (S-TH)	********	0
21 (S-NB)	34 (AA-AU-P)	********	0
21 (S-NB)	35 (INST-HG)	********	0
21 (S-NB)	36 (AA-AS-P)	********	0
21 (S-NB)	37 (AA-ZN-P)	********	0
21 (S-NB)	38 (AA-SB-P)	********	0
22 (S-NI)	23 (S-PB)	-0.4364	12
22 (S-NI)	24 (S-SB)	0.5582	5
22 (S-NI)	25 (S-SC)	********	1
22 (S-NI)	26 (S-SN)	********	0
22 (S-NI)	27 (S-SR)	-0.1559	4
22 (S-NI)	28 (S-V)	0.7419	11
22 (S-NI)	29 (S-W)	********	1
22 (S-NI)	30 (S-Y)	0.5151	5
22 (S-NI)	31 (S-ZN)	-0.2261	6
22 (S-NI)	32 (S-ZR)	0.0658	7
22 (S-NI)	33 (S-TH)	********	0
22 (S-NI)	34 (AA-AU-P)	********	1
22 (S-NI)	35 (INST-HG)	0.0018	11
22 (S-NI)	36 (AA-AS-P)	0.4337	11
22 (S-NI)	37 (AA-ZN-P)	0.0383	11
22 (S-NI)	38 (AA-SB-P)	-0.2089	11
23 (S-PB)	24 (S-SB)	-0.0953	15
23 (S-PB)	25 (S-SC)	-1.0000	2
23 (S-PB)	26 (S-SN)	********	0
23 (S-PB)	27 (S-SR)	0.7137	15
23 (S-PB)	28 (S-V)	-0.3665	22
23 (S-PB)	29 (S-W)	********	2
23 (S-PB)	30 (S-Y)	-0.4190	9
23 (S-PB)	31 (S-ZN)	0.6094	18
23 (S-PB)	32 (S-ZR)	0.4469	10
23 (S-PB)	33 (S-TH)	********	0
23 (S-PB)	34 (AA-AU-P)	-0.6439	5
23 (S-PB)	35 (INST-HG)	-0.0812	27
23 (S-PB)	36 (AA-AS-P)	0.4770	26
23 (S-PB)	37 (AA-ZN-P)	0.7173	27
23 (S-PB)	38 (AA-SB-P)	0.7539	27
24 (S-SB)	25 (S-SC)	********	0
24 (S-SB)	26 (S-SN)	********	0

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COLUMN	VERSUS	COLUMN	CORRELATION COEFFICIENT	NO. OF PAIRS
24 (S-SB)	27	(S-SR)	-0.1471	10
24 (S-SB)	28	(S-V)	-0.1276	11
24 (S-SB)	29	(S-W)	********	2
24 (S-SB)	30	(S-Y)	-0.5000	3
24 (S-SB)	31	(S-ZN)	0.3500	13
24 (S-SB)	32	(S-ZR)	********	2
24 (S-SB)	33	(S-TH)	********	0
24 (S-SB)	34	(AA-AU-P)	0.1446	4
24 (S-SB)	35	(INST-HG)	0.6224	15
24 (S-SB)	36	(AA-AS-P)	0.6433	16
24 (S-SB)	37	(AA-ZN-P)	0.1942	14
24 (S-SB)	38	(AA-SB-P)	0.5602	16
25 (S-SC)	26	(S-SN)	********	0
25 (S-SC)	27	(S-SR)	********	2
25 (S-SC)	28	(S-V)	1.0000	2
25 (S-SC)	29	(S-W)	********	0
25 (S-SC)	30	(S-Y)	1.0000	2
25 (S-SC)	31	(S-ZN)	********	1
25 (S-SC)	32	(S-ZR)	1.0000	2
25 (S-SC)	33	(S-TH)	********	0
25 (S-SC)	34	(AA-AU-P)	********	1
25 (S-SC)	35	(INST-HG)	1.0000	2
25 (S-SC)	36	(AA-AS-P)	********	1
25 (S-SC)	37	(AA-ZN-P)	-1.0000	2
25 (S-SC)	38	(AA-SB-P)	-1.0000	2
26 (S-SN)	27	(S-SR)	********	0
26 (S-SN)	28	(S-V)	********	0
26 (S-SN)	29	(S-W)	********	0
26 (S-SN)	30	(S-Y)	********	0
26 (S-SN)	31	(S-ZN)	********	0
26 (S-SN)	32	(S-ZR)	********	0
26 (S-SN)	33	(S-TH)	********	0
26 (S-SN)	34	(AA-AU-P)	********	0
26 (S-SN)	35	(INST-HG)	********	0
26 (S-SN)	36	(AA-AS-P)	********	0
26 (S-SN)	37	(AA-ZN-P)	********	0
26 (S-SN)	38	(AA-SB-P)	********	0
27 (S-SR)	28	(S-V)	-0.3949	9
27 (S-SR)	29	(S-W)	********	2
27 (S-SR)	30	(S-Y)	********	3
27 (S-SR)	31	(S-ZN)	0.2277	13
27 (S-SR)	32	(S-ZR)	********	4
27 (S-SR)	33	(S-TH)	********	0
27 (S-SR)	34	(AA-AU-P)	-0.7314	4
27 (S-SR)	35	(INST-HG)	0.1878	16
27 (S-SR)	36	(AA-AS-P)	0.0236	15
27 (S-SR)	37	(AA-ZN-P)	0.3552	14
27 (S-SR)	38	(AA-SB-P)	0.5074	16
28 (S-V)	29	(S-W)	********	1
28 (S-V)	30	(S-Y)	0.9103	9

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COLUMN	VERSUS	COLUMN	CORRELATION COEFFICIENT	NO. OF PAIRS
28 (S-V)	31	(S-ZN)	-0.2223	12
28 (S-V)	32	(S-ZR)	0.1782	10
28 (S-V)	33	(S-TH)	********	0
28 (S-V)	34	(AA-AU-P)	0.2360	4
28 (S-V)	35	(INST-HG)	0.0204	21
28 (S-V)	36	(AA-AS-P)	0.1948	20
28 (S-V)	37	(AA-ZN-P)	-0.1635	21
28 (S-V)	38	(AA-SB-P)	-0.2290	21
29 (S-W)	30	(S-Y)	********	0
29 (S-W)	31	(S-ZN)	********	2
29 (S-W)	32	(S-ZR)	********	0
29 (S-W)	33	(S-TH)	********	0
29 (S-W)	34	(AA-AU-P)	********	0
29 (S-W)	35	(INST-HG)	********	2
29 (S-W)	36	(AA-AS-P)	********	2
29 (S-W)	37	(AA-ZN-P)	********	2
29 (S-W)	38	(AA-SB-P)	********	2
30 (S-Y)	31	(S-ZN)	-0.6173	4
30 (S-Y)	32	(S-ZR)	0.1442	7
30 (S-Y)	33	(S-TH)	********	0
30 (S-Y)	34	(AA-AU-P)	********	1
30 (S-Y)	35	(INST-HG)	0.0948	9
30 (S-Y)	36	(AA-AS-P)	0.5229	8
30 (S-Y)	37	(AA-ZN-P)	-0.5075	9
30 (S-Y)	38	(AA-SB-P)	-0.1805	9
31 (S-ZN)	32	(S-ZR)	0.8010	3
31 (S-ZN)	33	(S-TH)	********	0
31 (S-ZN)	34	(AA-AU-P)	-0.8624	5
31 (S-ZN)	35	(INST-HG)	0.3858	19
31 (S-ZN)	36	(AA-AS-P)	0.4006	18
31 (S-ZN)	37	(AA-ZN-P)	0.9723	17
31 (S-ZN)	38	(AA-SB-P)	0.3926	18
32 (S-ZR)	33	(S-TH)	********	0
32 (S-ZR)	34	(AA-AU-P)	********	1
32 (S-ZR)	35	(INST-HG)	-0.6195	10
32 (S-ZR)	36	(AA-AS-P)	0.5036	8
32 (S-ZR)	37	(AA-ZN-P)	0.3903	10
32 (S-ZR)	38	(AA-SB-P)	0.2117	10
33 (S-TH)	34	(AA-AU-P)	********	0
33 (S-TH)	35	(INST-HG)	********	0
33 (S-TH)	36	(AA-AS-P)	********	0
33 (S-TH)	37	(AA-ZN-P)	********	0
33 (S-TH)	38	(AA-SB-P)	********	0
34 (AA-AU-P)	35	(INST-HG)	0.4369	6
34 (AA-AU-P)	36	(AA-AS-P)	-0.4519	5
34 (AA-AU-P)	37	(AA-ZN-P)	-0.7917	5
34 (AA-AU-P)	38	(AA-SB-P)	-0.4487	6
35 (INST-HG)	36	(AA-AS-P)	0.0761	26
35 (INST-HG)	37	(AA-ZN-P)	-0.2136	26
35 (INST-HG)	38	(AA-SB-P)	-0.0051	27