

ELKO JUNIOR HIGH SCHOOL  
GEOTHERMAL OBSERVATION WELL  
ELKO, NEVADA

August 18, 1986

Project No. 86-392

Prepared for:  
ELKO COUNTY SCHOOL DISTRICT

Prepared by:  
WILLIAM E. NORK, INC.

William E. Nork



**WILLIAM E. NORK, Inc.**

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## 1.0 SUMMARY AND CONCLUSIONS

1. A 239 feet deep Geothermal Observation Well was drilled and tested at the Elko Junior High School, Elko, Nevada.
2. Drill cuttings and an electric log of the 350 feet deep borehole indicated that the portion of the borehole below a depth of approximately 230 feet was not sufficiently permeable to justify completion below this depth. This portion of the borehole was backfilled with drill cuttings and abandoned.
3. Pumping and injection test results indicate that the observation well is capable of accepting between 50 and 60 gallons per minute if it were to be utilized as an injection well. This quantity is roughly equivalent to the off-season and base flow for the district heating system.
4. Test data indicate that the observation well is not fully developed. Additional development procedures are recommended to improve the injectivity of the well. Conversion to and use as an injection well is contingent upon approval by the appropriate regulatory agencies.
5. Injection at an average of approximately 86,400 gallons per day (constant rate of 60 gpm) of thermal effluent at this site will result in minimal impact on the chemical quality of ground water discharged from nearby city wells. Total dissolved solids is expected to increase from approximately 480 to 494 mg/l and iron may increase from 0.01 to 0.16 mg/l.



## 2.0 INTRODUCTION

A Geothermal Observation Well (GOW-1) was drilled at the Elko Junior High School in the NE 1/4 NW 1/4 of Section 11, Township 34 N., Range 55 E. within the storm-water detention impoundment northwest of the school building. Permission to drill the observation well was granted under State of Nevada Department of Minerals Permit No. 83.

The purpose of the observation well was to provide data necessary to assist in a rational evaluation of the feasibility and potential impacts of injecting thermal effluent into the alluvial aquifer beneath the school. The chemical quality of this effluent is good. It meets state and federal drinking water standards with the exception of elevated iron and the presence of detectable concentrations of hydrogen sulfide gas.

The alluvial aquifer in the vicinity of Elko is exploited by the City of Elko as its sole source of water supply. The observation well was conceived to alleviate deficiencies in the available data regarding the nature of the aquifer in this area. The site was selected principally on the driller's description of the formation materials penetrated by the Elko Junior High School production geothermal well drilled at this site. The driller indicated a significant thickness of potentially permeable geologic materials at this site.

The 240 feet deep observation well was drilled by R.D. Reynolds Drilling in the month of July, 1986. It was constructed so as to comply with State of Nevada regulations governing injection wells in the event it was found to be technically feasible to dispose of the thermal effluent in this manner and the disposal alternative was approved by the governing state agencies.

The observation well was subjected to a series of pumping and injection tests which were orchestrated by WILLIAM E. NORK, INC. The results of this investigative effort is summarized in this technical report.



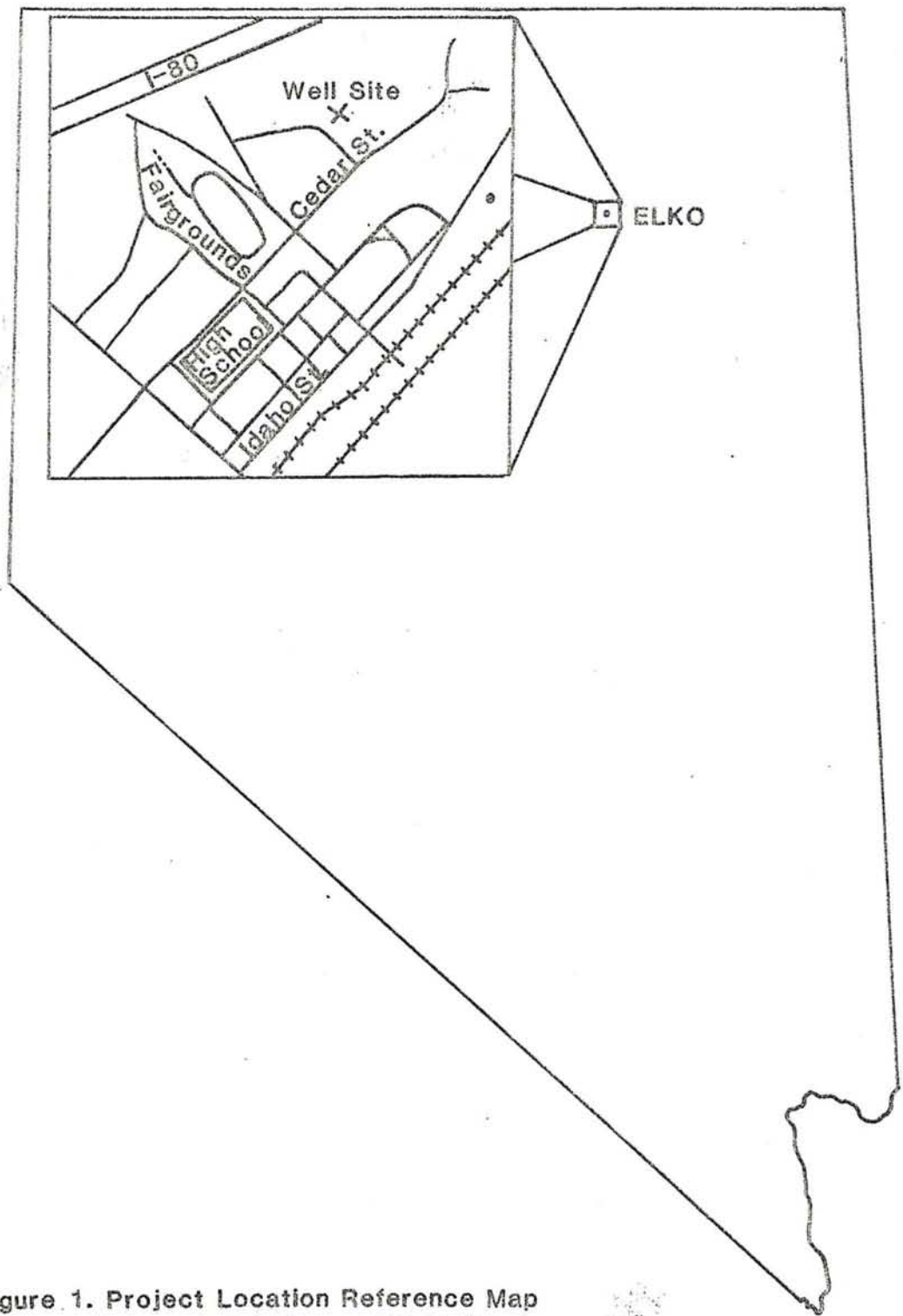


Figure 1. Project Location Reference Map  
Elko Junior High School  
Elko County, Nevada



### 3.0 WELL CONSTRUCTION SUMMARY

A nominal 12-inch diameter borehole was drilled to the target depth of 350 feet between July 15 and 21, 1986. The borehole penetrated alluvial deposits comprising poorly sorted sand, gravel, silt and clay with a few thin sand and gravel beds (Appendix A). On the basis of the lithologic log, it was apparent that the well could not accommodate an average injection rate of 150 gpm necessary to be considered a complete success as a possible injection well. To substantiate this field interpretation, an electric borehole geophysical log was run on July 22 (Appendix B). The log corroborated the preliminary evaluation. As a consequence, the original well design was modified to take advantage of every potentially permeable bed encountered in the well no matter how thin and eliminated geologic materials below a depth of 230 feet which were evaluated as unproductive.

Drilling deeper than the 350 feet target depth was ruled out on the basis of a comparison between the observation well E-log with the E-log of the test hole drilled nearby by Reynolds. To do so would have likely encountered progressively lower permeability deposits as evidenced by the test hole log.

Final well design is illustrated in Figure 2.

Following installation of the well casing, an artificial gravel envelope was emplaced in the annular space between the perforated casing and the formation walls. The well was then developed by jetting and surging with high pressure air. Jetting was followed by swabbing the well with a surge block utilizing a cable-tool rig in an attempt to maximize the hydraulic efficiency of the well. This additional stage of development was added when it became apparent that jetting was insufficiently violent to remove the fines from the formation and that additional development utilizing the relatively small test pump dictated by the probable yield of the well could not adequately surge the well. Development procedures were completed July 30, 1986.

Installation of the cement sanitary seal was delayed until after the completion of the aquifer stress tests. The purpose of this delay was to enable pulling the well casing prior to abandonment of the observation well should it be considered unsuccessful. Testing results (Section 4.0) indicated that the observation well was partially successful. As a result, the seal was emplaced August 12, 1986 by pumping a cement slurry from the top of the gravel pack to land surface (Appendix C), completing all construction activities.



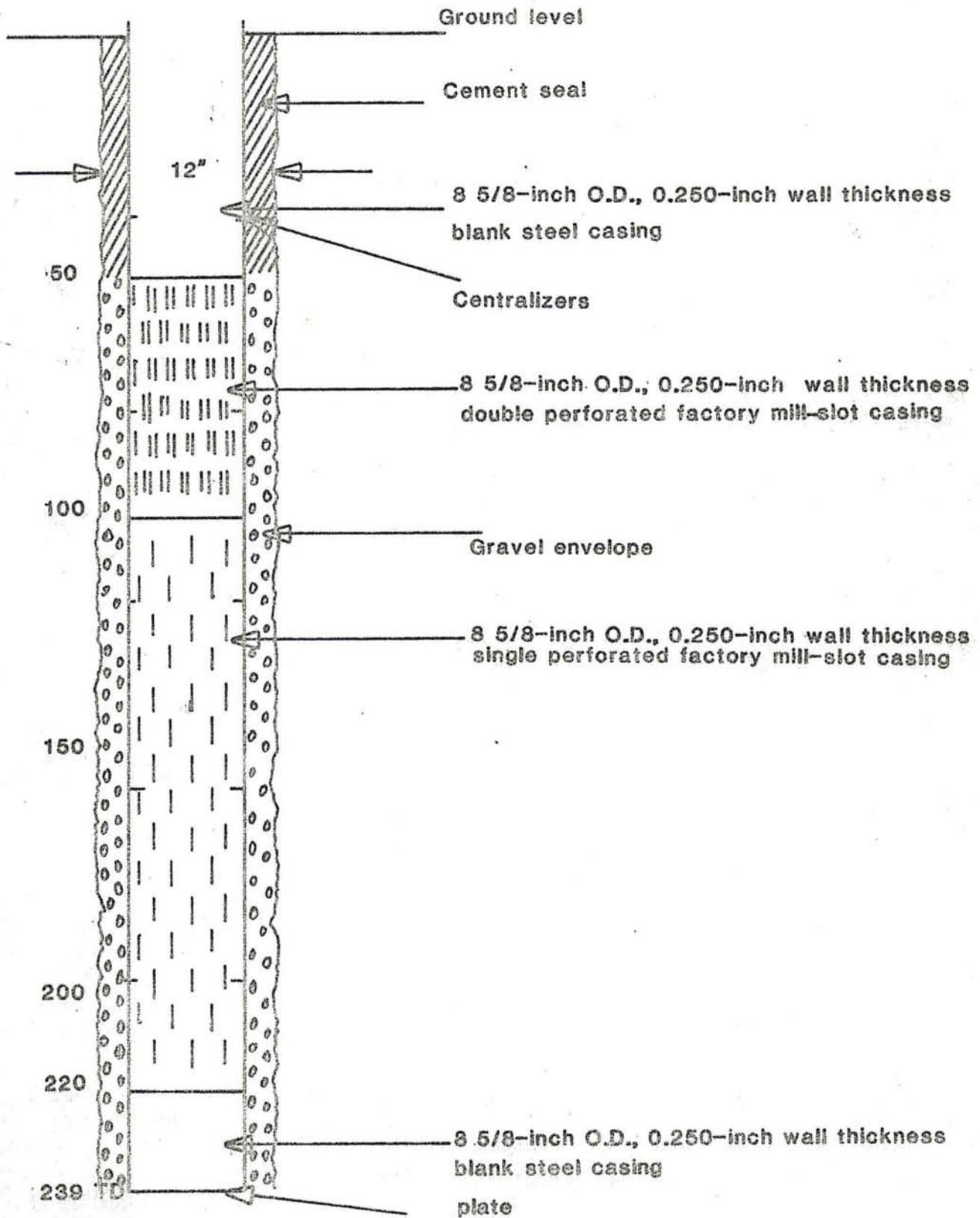


Figure 2. Elko Junior High School Geothermal Observation Well Construction Diagram.



#### 4.0 AQUIFER STRESS TESTS

Immediately upon completion of well development, a five horse-power submersible test pump was installed in the well. The testing sequence comprised a 12-hour step-drawdown test, 24-hour constant-discharge test and a 24-hour injection test, separated by suitable recovery periods. Testing results are summarized below. Field data sheets are provided in Appendix D.

##### 4.1 STEP-DRAWDOWN TESTING

A 12-hour duration step-drawdown pumping test comprising three-four-hour steps was conducted July 30-31, 1986.

| Step | Discharge<br>Q<br>(gpm) | Duration<br>t<br>(minutes) | Drawdown<br>s<br>(feet) | Specific Capacity<br>C<br>(gpm <sup>5</sup> /ft) |
|------|-------------------------|----------------------------|-------------------------|--|
| I    | 15                      | 240                        | 6.51                    | 2.3  |
| II   | 30                      | 240                        | 11.34                   | 2.6  |
| III  | 60                      | 240                        | 27.52                   | 2.2  |

Test data are plotted in Figure 3. From the drawdown and specific capacity data (Figure 4) it is apparent that the well was not fully developed by the end of the step-drawdown test. It is recommended that additional development be performed to increase the injectivity of the well, should it be approved as an injection well.

##### 4.2 CONSTANT-DISCHARGE TESTING

Following a recovery period of 12 hours, a 24-hour duration constant-discharge pumping test was initiated. Results are summarized below.

Static water level prior to testing was 94.70 feet below the measuring point (M.P. = top of stilling well). Testing commenced 1800 hrs 7/31/86. Pumping rate was held constant at 50 gpm. Pumping was terminated at 1800 hours 8/1/86. Pumping water level at the conclusion of the test was 109.6 feet below M.P., a drawdown of 14.93 feet. Recovery of water levels in the well were monitored for a period of 12 hours, at which time water levels had recovered 95 percent.

Drawdown and residual drawdown (a.k.a. recovery) data are plotted in Figures 5 and 6. The transmissivity of the aquifer was calculated utilizing the Cooper-Jacob approximation of the Theis equation.





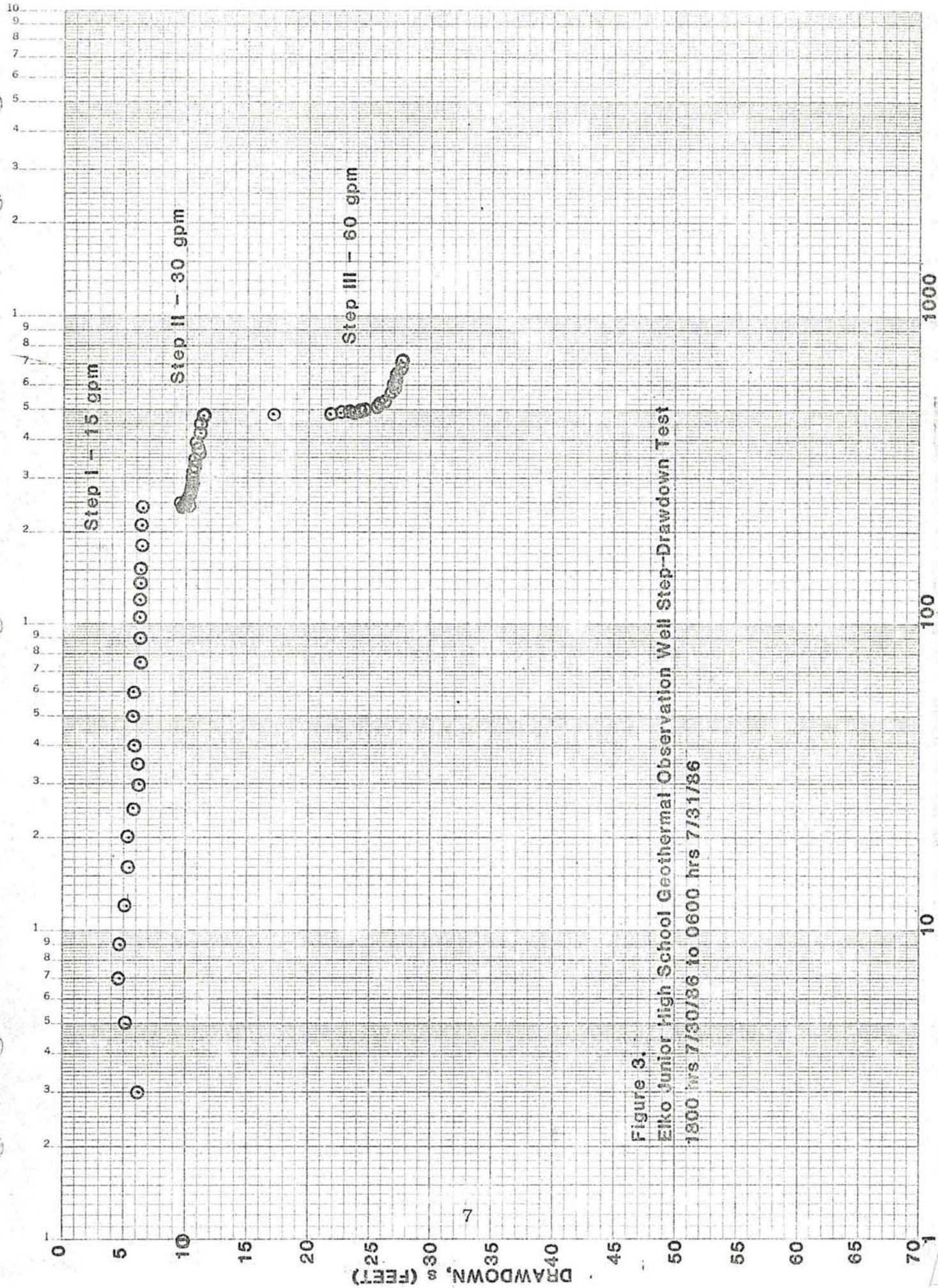


Figure 3.  
Eiko Junior High School Geothermal Observation Well Step-Drawdown Test  
1800 hrs 7/30/86 to 0600 hrs 7/31/86

TIME SINCE PUMPING STARTED, t (MINUTES)

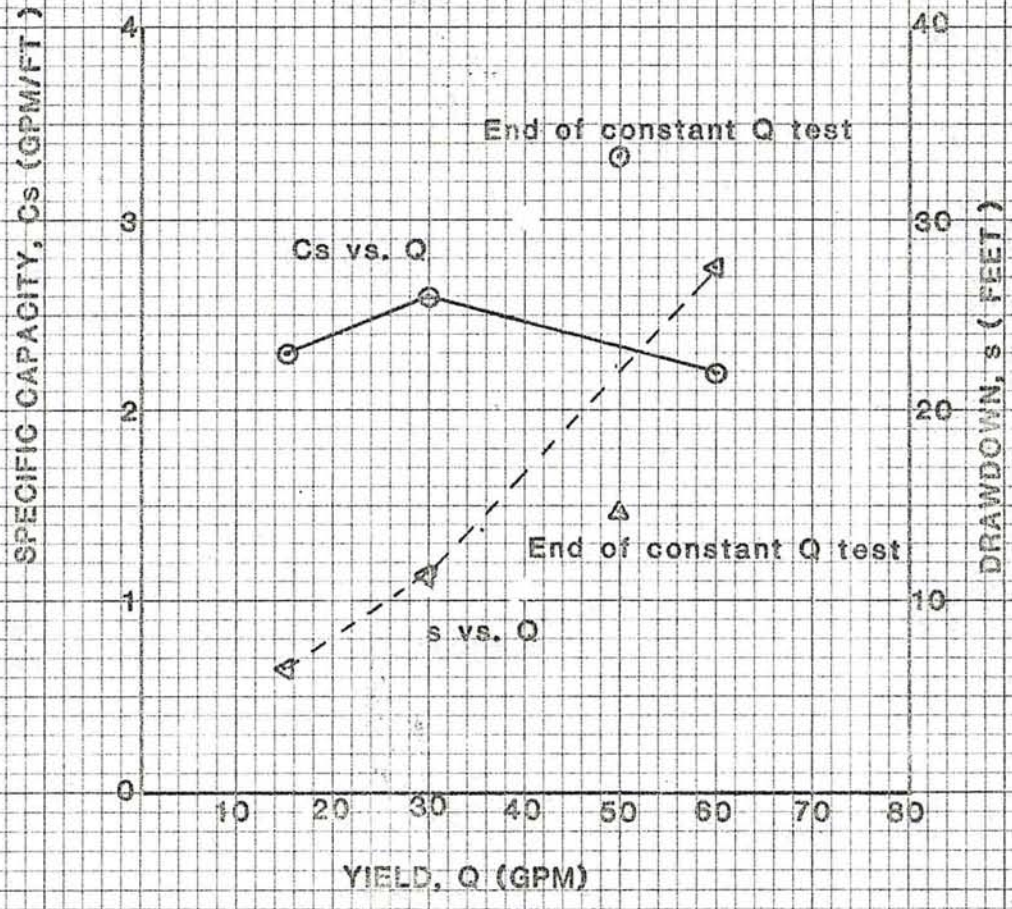
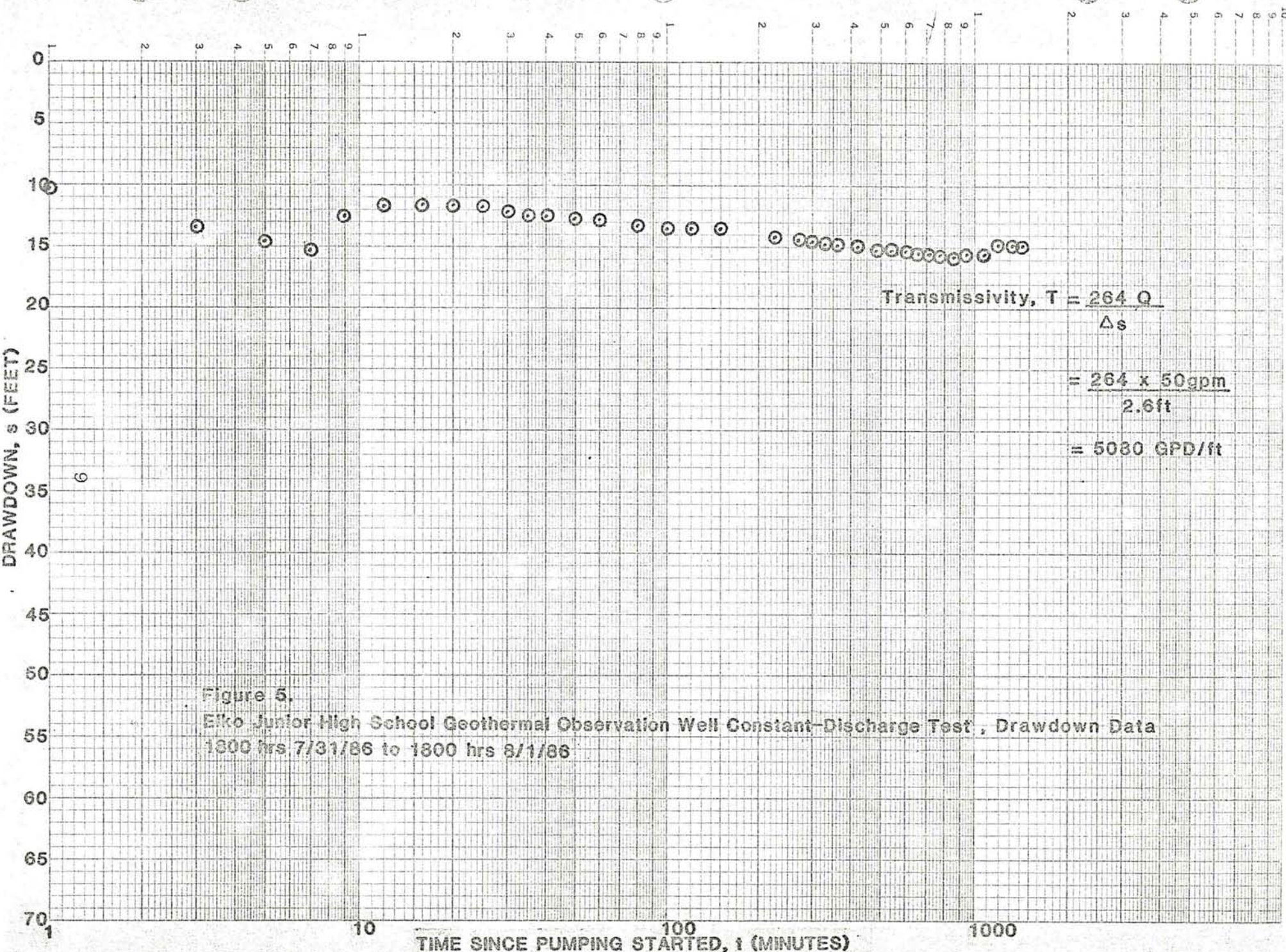


Figure 4. Elko Junior High School Geothermal Observation Well  
Specific Capacity and Drawdown Data



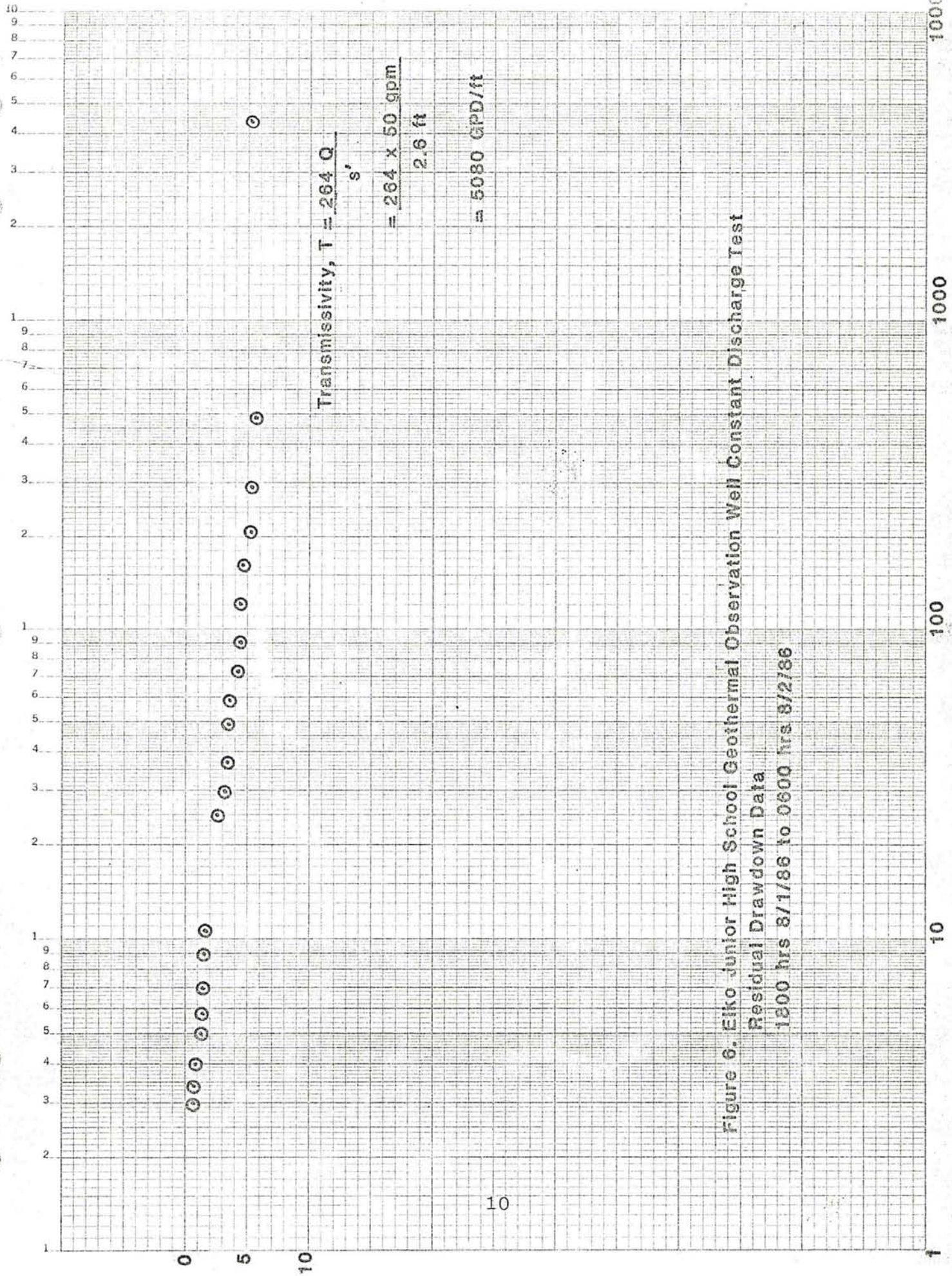


Figure 6. Elko Junior High School Geothermal Observation Well Constant Discharge Test  
Residual Drawdown Data  
1200 hrs 8/1/86 to 0600 hrs 8/2/86

| Data              | Transmissivity<br>(GPD/ft) |
|-------------------|----------------------------|
| Drawdown          | 5,080                      |
| Residual-drawdown | 5,080                      |

This value is consistent with the value of approximately 17,000 GPD/ft for the transmissivity of the alluvial aquifer, a value advanced from available data, when the lesser thickness of the aquifer penetrated by the observation well is taken in account. A value for the coefficient of storage could not be calculated due to the absence of a suitable observation well. It is likely that it is approximately 0.001, a value typical of semi-confined aquifers.

#### 4.3 INJECTION TEST

Following completion of the recovery portion of the constant-discharge test, a 24-hour duration injection test was conducted. The injection rate varied between 37.2 and 114.1 gpm, averaging 60.5 gpm for the entire test. At the conclusion of the test, the water level within the well had risen to within approximately 7.2 feet below land surface. Test data are summarized in Figure 7.



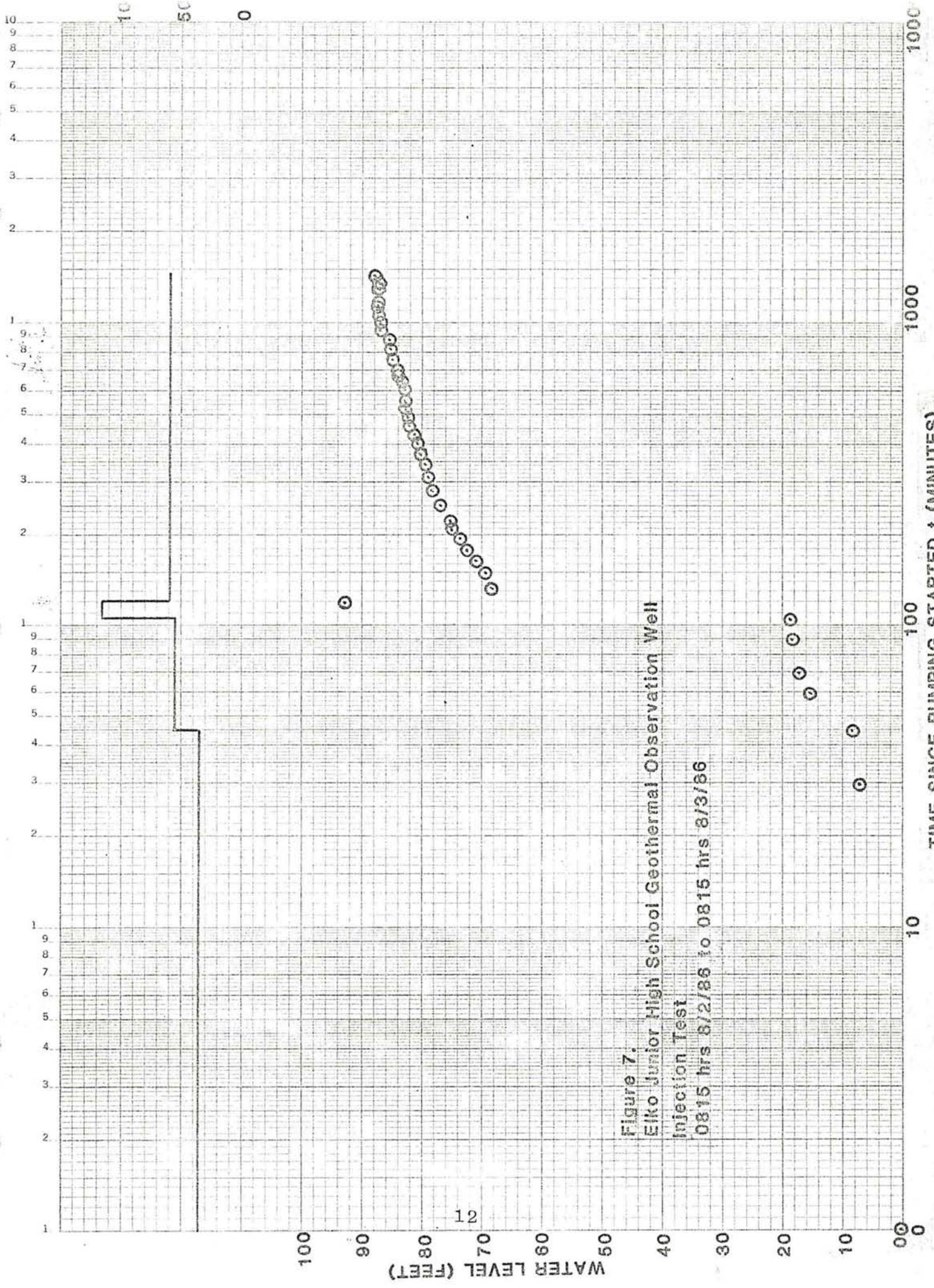


Figure 7.  
Elko Junior High School Geothermal Observation Well  
Injection Test  
0815 hrs 8/2/86 to 0815 hrs 8/3/86

12

## 5.0 WATER CHEMISTRY

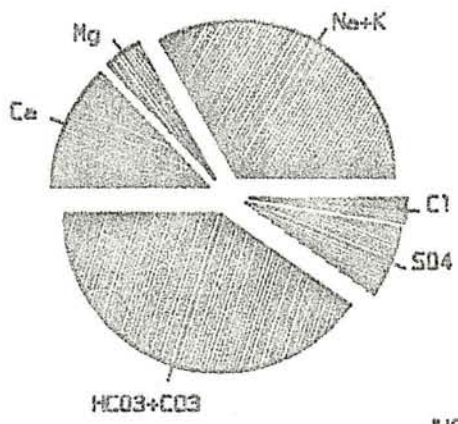
A water sample for chemical analysis was collected at the conclusion of the constant-discharge pumping test. Results of the analysis are listed below and compared with water chemistry data for City Well No. 12 and the Elko Junior High School Geothermal Well.

Table 1. Water chemistry data.

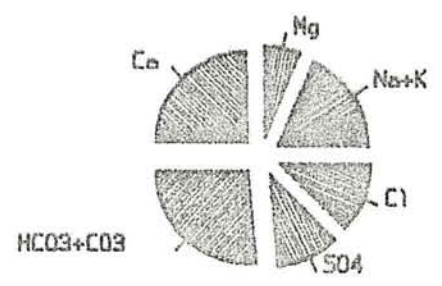
| Sample source    | EJHS Geothermal Well | City Well No. 12 | Geothermal Observation Well | Drinking Water Standard |
|------------------|----------------------|------------------|-----------------------------|-------------------------|
| TDS              | 645                  | 481              | 481                         | 1000                    |
| pH               | 6.45                 | 7.74             | 7.8                         |                         |
| Ca               | 68.9                 | 70               | 3.49 47.0 69                |                         |
| Mg               | 12.5                 | 11               | 0.905 12.9 10               | 150                     |
| Na               | 180                  | 50               | 2.175 30.9 50               |                         |
| K                | 36.5                 | 18               | 0.460 6.3 17                |                         |
|                  |                      |                  | 7.030                       |                         |
| HCO <sub>3</sub> | 500.2                | 210              | 3.442 53.1 194              |                         |
| CO <sub>3</sub>  | <0.01                | 0                | 0                           |                         |
| SO <sub>4</sub>  | 71                   | 70               | 1.457 22.5 57               | 500                     |
| Cl               | 18                   | 56               | 1.537 24.4 75               | 500                     |
| NO <sub>3</sub>  | 0.03                 | 13.6             | 13.7                        | 45                      |
| F                | 1.86                 | 0.25             | 0.2                         | 1.8 0.6                 |
|                  |                      |                  | 6.476                       |                         |
| As               | 0.003                | 0                | 0.005                       | 0.05                    |
| Ba               | 0.25                 | *                | <0.4                        | 1.0                     |
| B                | 0.986                | *                | 0.2                         |                         |
| Cd               | <0.001               | *                | <0.01                       | 0.01                    |
| Cr               | <0.001               | *                | <0.02                       | 0.05                    |
| Cu               | <0.01                | *                | <0.02                       | 1.0                     |
| Pb               | <0.001               | *                | <0.05                       | 0.05                    |
| Fe               | 1.8                  | 0.01             | 0.08                        | 1.8                     |
| Mn               | 0.03                 | 0                | 0.09                        | 0.1                     |
| Hg               | <0.0005              | *                | <0.0005                     | 0.002                   |
| Se               | <0.001               | *                | <0.005                      | 0.01                    |
| Ag               | <0.001               | *                | <0.01                       | 0.05                    |
| Zn               | 0.009                | *                | 0.56                        | 5.0                     |
| SiO <sub>2</sub> | 77.8                 | *                | 75                          |                         |
| H <sub>2</sub> S | 0.6                  |                  |                             |                         |

The gross similarity of the water from the various sources is graphically depicted in Figure 8.

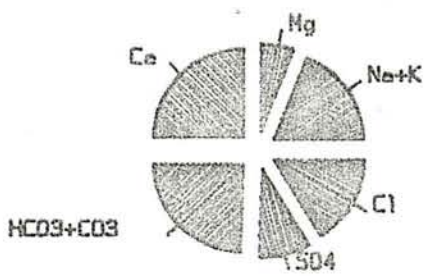




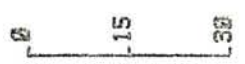
JHS



CITY#12



GOV-1



SCALE OF RADII  
(TOTAL OF EQUIVALENTS  
PER MILLION)

NOTE ERROR (IF ANY) IN CATION/ANION  
BALANCE HAS BEEN REMOVED

PROJECT: ELKO JHS  
FILE: 392  
LOCATION: ELKO NV

PIE DIAGRAMS  
SHOWING WATER QUALITY

WILLIAM E. NORK, INC.

FIGURE: 8



WILLIAM E. NORK, Inc.

Reno, Nevada 89503



## 6.0 IMPACT ON NEARBY WELLS

The City of Elko derives its water supply from numerous wells completed in the alluvial deposits. In the vicinity of the Junior High School they are approximately 400 to 550 feet deep. A total of four wells, numbers 10A, 12, 13 & 14 are located within one-half mile down gradient of the Junior High School site (refer to Figure 9).

Considering the number of wells that have been drilled by the City, there is little readily available data. However, some information regarding the hydrogeologic regime of the alluvial aquifer can be gleaned from the city records. Pumping test data from Well No. 14 suggest an aquifer transmissivity of approximately 17,000 GPD/ft. Specific capacity data from other wells yield similar values and suggests that the aquifer is somewhat uniform in overall character in the vicinity of the Junior High School. The value of transmissivity from the geothermal observation well is reasonably consistent with this value considering the fact that it penetrates less of the aquifer and allowing for some heterogeneity of the alluvial deposits.

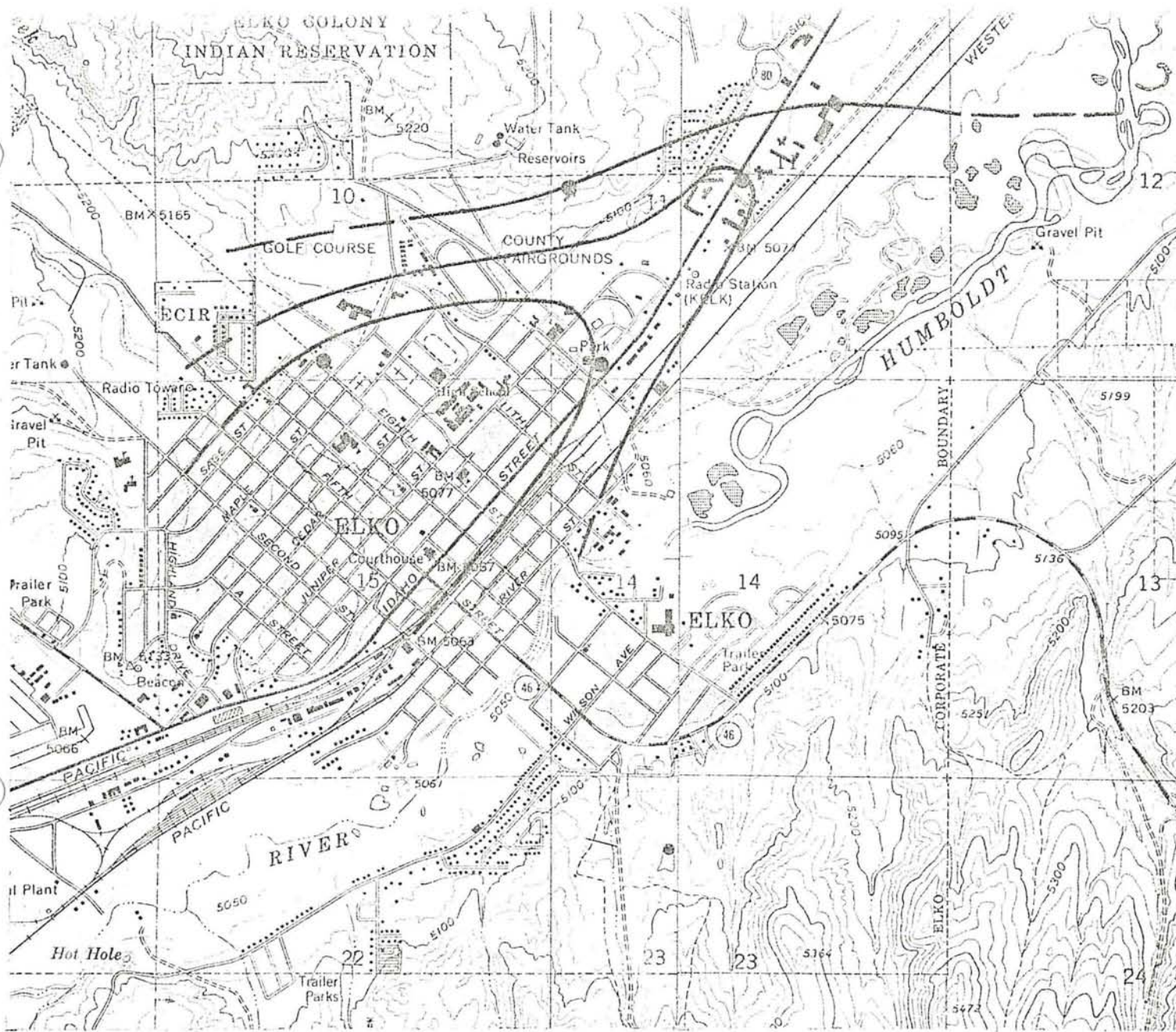
Water level information suggest a southerly to southeasterly direction of ground water flow immediately beneath the site (Figure 9). These data indicate a well defined trough of depression beneath Elko caused by the withdrawals by the city wells. Moreover, they suggest a hydraulic connection with the Humboldt River. That is, unless there is a source of recharge to the aquifer such as the river, drawdowns experienced by city wells should be much greater than that allowed by the available data.

To test these hypotheses, drawdowns in the aquifer were simulated utilizing average monthly discharges from the city wells (for 1985), the transmissivity from the Well No. 14 test (17,000 GPD/ft), and a recharge boundary coincidental with the Humboldt River in the analytical model VARFLOW (IDO, 1984). Input for the model are listed in Appendix E. The general shape of drawdown contours (Figure 10) agreed with those drawn from the available information and appears to support the model of the aquifer suggested by the available data.

It follows then, that any thermal effluent injected into the alluvial aquifer tapped by the city wells will ultimately flow toward these nearby wells. To examine the impact on the chemical quality of the ground water discharged by the city wells, consider the following:

1. Wells No. 12 and 14 discharged an average of 1,066,406





Scale

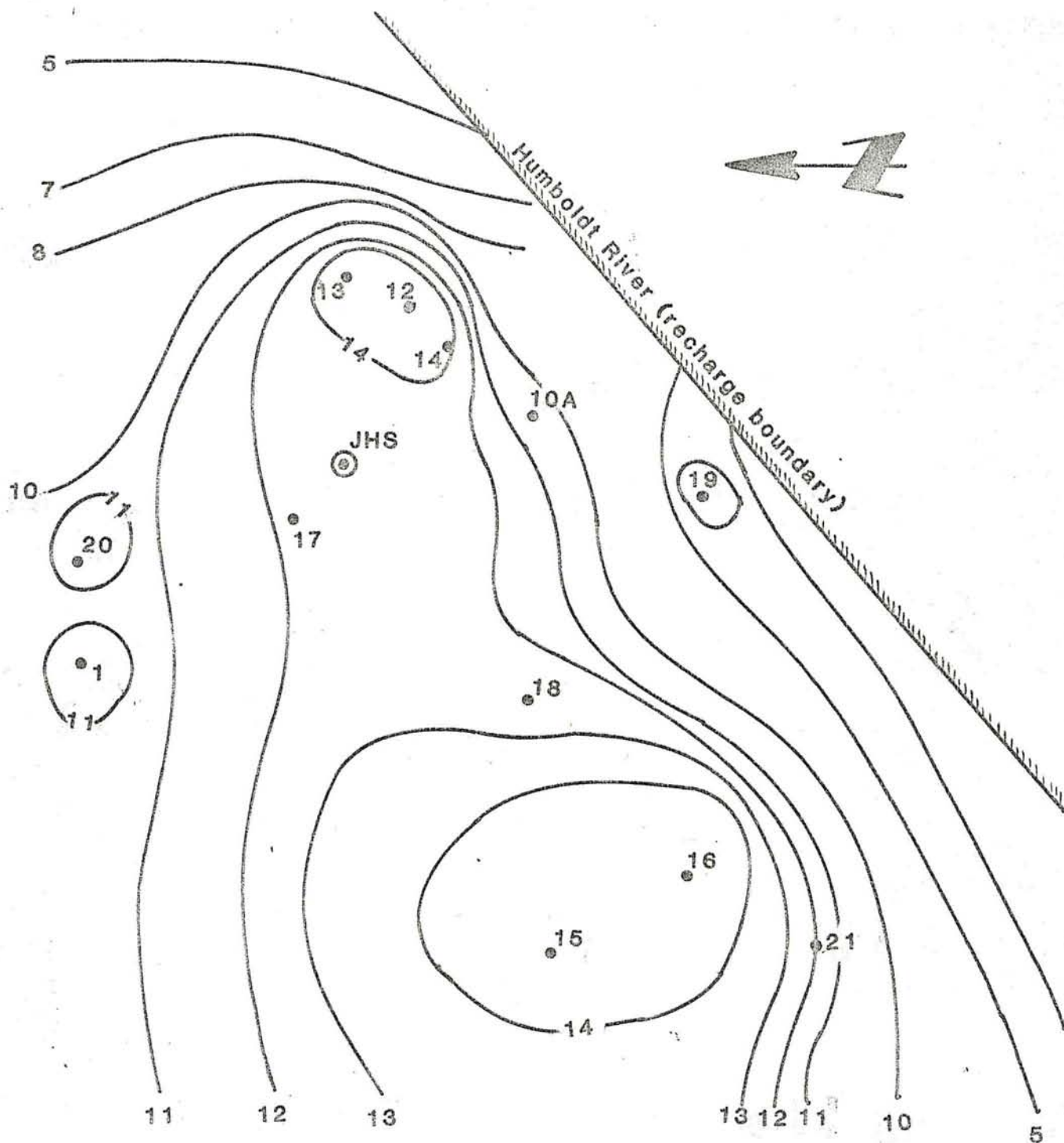
1 : 24,000

EXPLANATION

- Well (water level reported)
- water level contour ( feet above-sea level )

Figure 9. Well site locations and water level elevations in the vicinity of the Elko Junior High School!





Scale  
1 inch 2000 feet

14 • City well

Figure 10. Computed drawdown due to city pumpage in the vicinity of the Elko Junior High School



gallons per day (GPD) in 1985.

2. The injectivity of the Geothermal Observation Well is 86,400 GPD.
3. The concentration of iron in the discharge of Wells No. 12 and 14 is 0.01 mg/l.
4. The concentration of iron in the thermal effluent is 1.8 mg/l.

Assuming that no dispersion or mixing takes place in the aquifer, the concentration of iron in the discharge of Wells No. 12 and 14 may approach

$$C = \frac{(86,400 \text{ GPD} \times 1.8 \text{ mg/l}) + (980,000 \times 0.01 \text{ mg/l})}{1,066,406 \text{ GPD}}$$
$$= 0.16 \text{ mg/l}$$

which is well below the drinking water standard.

The Total Dissolved Solids can likewise be evaluated, assuming

1. TDS of city water is approximately 480 mg/l.
2. TDS of effluent is 650 mg/l.

Substituting this value into the mixing equation yields a concentration,

$$C = \frac{(86,400 \text{ GPD} \times 650 \text{ mg/l}) + (980,000 \text{ GPD} \times 480 \text{ mg/l})}{1,066,406 \text{ GPD}}$$
$$= 494 \text{ mg/l}$$

which is a very insignificant increase. Since the chemical nature of the alluvial and thermal waters is similar, no noticeable change in the character of the drinking water will occur (WEN, INC., 1985).

Because the thermal effluent will disperse and the plume will be spread out further by other city wells, any increase in TDS and iron will be less than that predicted above.



The need for a more rigorous analysis such as two- or three-dimensional numerical computer modelling is not warranted due to the small potential impact suggested by the worst-case discussed above.



## 7.0 SOURCES OF INFORMATION

IDO, 1982. Low-to-moderate temperature hydrothermal reservoir engineering handbook; U.S. Department of Energy Idaho operations Office, IDO-10099, Vol. II.

Nork, William E. Inc., 1985. Junior High School geothermal well; private consulting report prepared for the Elko County School District.

### Other sources:

City of Elko; well logs, pumping test and water chemistry data, and monthly pumpage records for city wells.



APPENDIX A  
LITHOLOGIC LOG



**WILLIAM E. NORK, Inc.**

*Reno, Nevada 89503*

LOG OF BOREHOLE

BOREHOLE ELKO JUNIOR High G.O.W. #1

PAGE 1 of 5

|   |                              |   |                            |
|---|------------------------------|---|----------------------------|
| LOC. or COORDS. <u>ELKO JR. High School</u> | DRILLER <u>Ray Reynolds</u>  | START DATE <u>7-15-86</u>   | FINISH DATE <u>7-21-86</u> |
| GROUND ELEV. <u>5140'</u>                   | <u>Drilling Co.</u>          | TIME <u>9:30 am</u>   | <u>5:00 pm</u>             |
| TOTAL DEPTH <u>239'</u>                     | RIG <u>Scharmon, T-64 HB</u> | GEOPHYS LOG <input checked="" type="checkbox"/> YES <input type="checkbox"/> NO | HOW LEFT _____             |
| BOREHOLE DIAM. <u>12"</u>                   | BIT(S) <u>12"</u>            | FLUID <u>MUD ROTARY</u>   |                            |

PROJECT ELKO JUNIOR High School G.O.W. #1 LOCATION ELKO JUNIOR High

LOGGED BY JKS

| DEPTH | PENE-TRATE | CIRC. RET. LOSS |      | A-LIFT (gpm) | MATERIAL | SYM BOL | DESCRIPTION AND COMMENTS   |
|-------|------------|-----------------|------|--------------|----------|---------|--|
|       |            | RET.            | LOSS |              |          |         |  |
| - 5'  | 60'/hr     |                 |      |              |          |         | whole drilled to depth of 45' BEFORE my arrival - (no samples taken)   |
| - 10' |            |                 |      |              |          |         | Sample Taken from flushing hole - gravels & clays 50/50 too mixed to id. correctly   |
| - 15' |            |                 |      |              |          |         | Sample at 45'  |
| - 20' |            |                 |      |              |          |         |  |
| - 25' |            |                 |      |              |          |         |  |
| - 30' |            |                 |      |              |          |         |  |
| - 35' |            |                 |      |              |          |         |  |
| - 40' |            |                 |      |              |          |         |  |
| - 45' | 60'/hr     |                 |      |              |          |         | Sample shows minor amounts of gravel intermixed with clays - hole may yet be showing cuttings from 1st 45' Rock chips are angular up to 0.5cm long - 50% clays UP (further it appears to be a mudstone or siltstone) |
| - 50' |            |                 |      |              |          |         | Mudstone - minor gravels -   |
| - 55' |            |                 |      |              |          |         | Mudstone - minor gravels, clays  |
| - 60' |            |                 |      |              |          |         | clays, more gravels, bits of black shale   |
| - 62' |            |                 |      |              |          |         | <u>- 62' hit gravels</u> Some fluid losses   |
| - 65' |            |                 |      |              |          |         | gravel, fine grained, well sorted, angular minor amounts of clays  |
| - 70' |            |                 |      |              |          |         | down to 70' @ 1125'/hr - gravels, $\leq 1/8"$ well sorted, gtz, shale, FOS/PS, fine gravel   |



|  |                             |   |                            |
|--|-----------------------------|---|----------------------------|
| LOC. OF COORDS. <u>ELKO JUNIOR HIGH SCHOOL</u> | DRILLER <u>Ray Reynolds</u> | START DATE <u>7-15-86</u>   | FINISH DATE <u>7-21-86</u> |
| GROUND ELEV. <u>5140</u>                       | RIG <u>Schaumm T-64-HB</u>  | TIME <u>9:30am</u>  | <u>5:00pm</u>              |
| TOTAL DEPTH <u>350'</u>                        | BIT(S) <u>12"</u>           | GEOPHYS LOG <input checked="" type="checkbox"/> YES <input type="checkbox"/> NO |                            |
| BOREHOLE DIAM. <u>12"</u>                      | FLUID <u>MUD, water</u>     | HOW LEFT _____  |                            |

LOCATION LOGGED BY

PROJECT

| DEPTH | PENE-TRATE | CIRC. RET. LOSS | A-LIFT (gpm) | MATERIAL                | SYM BOL | DESCRIPTION AND COMMENTS  |
|-------|------------|-----------------|--------------|-------------------------|---------|---|
| 75'   | 60'/hr     | 10 gpm          |              | gravels                 | 0       | gravels, $\leq 1/8"$ well sorted, angular - fine grained<br>Heavy Fluid losses - (R.R.) - "5-10 gpm"  |
| 80'   |            |                 |              |                         | 0       | gravels - getting coarser $\leq 1/4"$ , minor clays   |
| 85'   | 50'/hr     |                 |              |                         | 0       | gravels - $\leq 1/4"$ angular to rounded, more clay<br>rig penetration slowing a little   |
| 90'   | 60'/hr     |                 |              | GRAVELS                 | 0       | gravels - finer graind again $\leq 1/8"$ minor clays.<br>ADDED 1 BAG MUD * 12:00 noon   |
| 95'   | 60'/hr     |                 |              |                         | 0       | gravel, minor clays - no change - Fluid loss negligible   |
| 100'  |            |                 |              |                         | 0       | gravel - no apparent $\Delta$ , Fluid loss now negligible   |
| 105'  |            |                 |              |                         | 0       | gravel, coarser $\leq 1/4"$ , minor clays, & bits to well rounded.<br>moderate fluid loss again -   |
| 110'  | 30'/hr     |                 |              |                         | 0       | gravel size seems to be increasing w/ depth<br>quit for lunch - 12:15 pm ADD 1 BAG MUD -<br>gravel, some clays - penetration slowed here: poss<br>indication of clay beds                                   |
| 115'  |            |                 |              | INCREASING CLAY content | 0       | gravel, coarse $\leq 1/4"$ , clays - (40% $\pm$ )   |
| 120'  |            |                 |              |                         | 0       | clays, coarse gravels (40% $\pm$ ) penetration<br>still @ 30'/hr or less, gravels slightly finer  |
| 125'  |            | Loss of 3 gpm   |              | gravel                  | 0       | 122' static change - Fluid loss minor to negligible, Fluid loss $\approx$ 3-4 gpm est.<br>gravel - coarse grained $\leq 1/4"$ 30% clays; decreasing<br>angular shape. most grains $\approx 1/8"$ to $1/16"$ |
| 130'  | 30'/hr     | 5-6 gpm         |              | gravel                  | 0       | gravel - medium grained $1/8"$ or less angular to sub-rounded. minor amounts of clay<br>Fluid loss increasing 5-6 gpm est.  |
| 135'  |            |                 |              |                         | 0       | gravel, angular to sub rounded - minor clays<br>fluid loss $\approx$ 4-5 gpm  |
| 140'  |            |                 |              |                         | 0       | gravels, upto $1/4"$ , angular to sub rounded, clays<br>increasing - upto $\approx$ 30%<br>NOTE: clays are reddish brown; silty -   |

LOG OF BOREHOLE

BOREHOLE ELKO THS.

PAGE 3 of 5

|                                  |                             |   |                            |
|----------------------------------|-----------------------------|---|----------------------------|
| LOC. or COORDS. <u>ELKO THS.</u> | DRILLER <u>Ray Reynolds</u> | START DATE <u>7-15-86</u>   | FINISH DATE <u>7-21-86</u> |
| GROUND ELEV. <u>5140</u>         |                             | TIME <u>9:30am</u>  | <u>5:00pm</u>              |
| TOTAL DEPTH <u>350'</u>          | RIG <u>Scheuch T-64 HB</u>  | GEOPHYS LOG <input checked="" type="checkbox"/> YES <input type="checkbox"/> NO |                            |
| BOREHOLE DIAM. <u>12"</u>        | BIT(S) <u>12"</u>           | HOW LEFT _____  |                            |
|                                  | FLUID <u>MUD Rotary</u>     |   |                            |

LOCATION LOGGED BY

PROJECT

| DEPTH | PENE-TRATE | CIRC. RET. LOSS     | A-LIFT (gpm) | MATERIAL                    | SYM-BOL | DESCRIPTION AND COMMENTS   |
|-------|------------|---------------------|--------------|-----------------------------|---------|--|
| 145'  | 30'/hr.    |                     |              | gravels                     | ○       | ADD 1/2 BAG mud - penetration may be slower due to type of bit and fact that pressure from mud is pushing bit up?? No major lithological changes since 62' depth. gravel, angular, up to 1/4", 30% clays or less, fluid loss negligible. |
| 150'  |            | 3 to 4 gpm          |              | gravels; clays              | ○       | 148' - 1/2 BAG mud ADDED - gravel, angular up to 1/4", 50% clays ±, fluid loss minor, 3 to 4 gpm.  |
| 155'  |            | 3 to 4 gpm          |              | gravels; clays              | ○       | gravels, angular to subrounded, up to 3/8", 50% clays, minor fluid loss  |
| 160'  |            | 5-6 gpm             |              |                             | ○       | gravels, & to subrounded, minor clays, 20% or less. penetration up slightly. Fluid loss 5-6 gpm EST.   |
| 165'  |            |                     |              | gravels minor clays         | ○       | gravels, & to subrounded, minor amounts of clay ≈ 20% NOTE: clays are reddish brown silty clays (NOT bentonite)  |
| 170'  | 30'/hr.    | 2-3 gpm             |              | gravels minor clays         | ○       | gravels & to subrounded, minor amounts of clay ≤ 20%   |
| 175'  |            | 2-3 gpm             |              | gravel; reddish brown clays | ○       | gravels ANGULAR TO SUBROUNDED, up to 25% clays very little lithological change. Penetration slowed. Fluid loss 2-3 gpm   |
| 180'  | 20'/hr.    | 2-3 gpm             |              |                             | ○       | gravels - angular to subrounded, fluid loss 2-3 gpm, clays in minor amounts 10-15%   |
| 185'  | 20'/hr.    | 3-4 gpm             |              | gravel / clay mix           | ○       | gravels & to subrounded - clays 50% press clay stringers in between gravel beds however no penetration changes occurring to suggest this   |
| 190'  |            |                     |              |                             | ○       | gravels - fine grained - bentonite showing up sample not particularly representative   |
| 195'  |            | ≤ 1 gpm (*measured) |              |                             | ○       | gravels, & to subrounded, minor amounts red silty clays  |
| 200'  | 60'/hr.    |                     |              |                             | ○       | gravels, & to subrounded 1/8" or less, 20% clays   |
| 205'  |            | ≤ 1 gpm             |              |                             | ○       | gravels, fine grained 1/16" or less, less clays ≈ 10%  |
| 210'  |            |                     |              |                             | ○       | gravels - 1/8" or less, & to sub (clays 15% ±)   |
| 215'  |            | 2+ gpm              |              |                             | ○       | gravels - " no change.   |

LOG OF BOREHOLE

BOREHOLE JHS-ELKO

PAGE 4 of 5

|   |                             |   |                            |
|---|-----------------------------|---|----------------------------|
| LOC. or COORDS. <u>ELKO</u><br><u>JHS</u> | DRILLER <u>Ray Reynolds</u> | START DATE <u>7-15-86</u>   | FINISH DATE <u>7-21-86</u> |
| GROUND ELEV. <u>5140</u>                  |                             | TIME <u>9:30am</u>  | <u>5:00pm</u>              |
| TOTAL DEPTH <u>350'</u>                   | RIG <u>Schramm T-64-HB</u>  | GEOPHYS LOG <input checked="" type="checkbox"/> YES <input type="checkbox"/> NO |                            |
| BOREHOLE DIAM. <u>12"</u>                 | BIT(S) <u>12"</u>           | HOW LEFT _____  |                            |
|   | FLUID <u>MUD</u>            |   |                            |

LOCATION LOGGED BY

PROJECT

| DEPTH | PENE-TRATE | CIRC. RET. LOSS | A-LIFT (gpm) | MATERIAL        | SYM-BOI. | DESCRIPTION AND COMMENTS  |
|-------|------------|-----------------|--------------|-----------------|----------|---|
| 220'  | 60'/hr     | 2 gpm           |              | gravels         | 0-0      | Gravels, 1/8" or less, & to subrounded - 20% clays. at 218 rig indicated poss clay. back for 3-4" poss indication of separate lithologies - |
| 225'  | ↓          | 2 gpm           |              | "               | 0-0      | gravels, 1/8" or less, & to subr. 10-15% clays. no penetration rate change - no Δ in fluid losses   |
| 230'  | ↓          |                 |              | "               | 0-0      | gravels, 1/8" =, & to subrounded, 10% clays - NO Δ.   |
| 235'  | 50'/hr     | 19 gpm          |              |                 | 0-0      | gravels, 1/8" & to subrounded, clays up to 30% ± penetration down a little, fluid loss = 19 gpm   |
| 240'  | ↓          | 1+ gpm          |              | gravels & clays | 0-0      | gravels ≤ 1/8" 35-40% clays, no Δ in penetration or fluid losses  |
| 245'  | 30'/hr     | 2-3 gpm         |              |                 | 0-0      | Mud getting thick again - Penetration decrease NOT due to lithological changes - fluid losses increasing due to cleaning of mud tanks.      |
| 250'  | 30'/hr     | 2 gpm           |              | gravels         | 0-0      | 245 - gravel ≤ 1/8", silty clays 20% ±, clays still reddish brown w/in, var amounts of sand size particles                                  |
| 255'  | 30'/hr     | 1-2 gpm         |              | gravels         | 0-0      | gravel ≤ 1/8" & to subrounded, 10-15% clays, reddish brown silty clays (sticky)   |
| 260'  | 30'/hr     | 2 gpm           |              |                 | 0-0      | gravels, ≤ 1/8" & to subrounded, 10% clays, NO Δ in penetration or fluid losses   |
| 265'  | ↓          | 1-2 gpm         |              |                 | 0-0      | gravels ≤ 1/8" & to subrounded, 15% clays - no changes  |
| 270'  | ↓          | 2 gpm           |              | gravels         | 0-0      | gravels, slightly larger ≤ 3/16", 5-10% clays.  |
| 275'  | ↓          |                 |              |                 | 0-0      | no change (Office call during this period)  |
| 280'  | ↓          |                 |              |                 | 0-0      | gravels, 20% clays  |
| 285'  | ↓          | 2 gpm           |              |                 | 0-0      | gravels, ≤ 1/4" & to subrounded, 15% clays no penetration or fluid Δ's.   |
| 290'  | ↓          | 1-2 gpm         |              |                 | 0-0      | gravels ≤ 3/16", 20% clays, No changes  |

|  |  |   |                            |
|--|--|---|----------------------------|
| LOC. or COORDS. <u>ELKO JUNIOR HIGH School</u> | DRILLER <u>Ray Reynolds Drilling Co.</u> | START DATE <u>7-15-86</u>   | FINISH DATE <u>7-21-86</u> |
| GROUND ELEV. <u>5140</u>                       | RIG <u>Schramm T-64 HB</u>               | TIME <u>9:30am</u>  | <u>5:00pm</u>              |
| TOTAL DEPTH <u>350'</u>                        | BIT(S) <u>12"</u>                        | GEOPHYS LOG <input checked="" type="checkbox"/> YES <input type="checkbox"/> NO |                            |
| BOREHOLE DIAM. <u>12"</u>                      | FLUID <u>mud (Bentonite/water)</u>       | HOW LEFT _____  |                            |

LOCATION LOGGED BY

PROJECT

| DEPTH | PENE-TRATE | CIRC. RET. LOSS | A-LIFT (gpm) | MATERIAL | SYM BOL | DESCRIPTION AND COMMENTS  |
|-------|------------|-----------------|--------------|----------|---------|---|
| 295'  | 30"/hr     | 2 gpm           |              |          |         | gravels $\leq 1/4"$ , 15-20% clays, fluid loss slightly increased. penetration unchanged          |
| 300'  | ↓          | 2 gpm           |              |          |         | gravels $\leq 1/4"$ , 25% clays, gravels are $\&$ to subrounded - increasing clay content         |
| 305'  | ↓          | 2 gpm           |              |          |         | gravels $\leq 1/8"$ 25% clays - (red silty)   |
| 310'  | ↓          | 1-2 gpm         |              |          |         | gravel, $\leq 3/16"$ 20% clays - RED BROWN SILTY clays, NO MAJOR LITHOLOGICAL CHANGES -           |
| 315'  | ↓          |                 |              |          |         | gravels $\leq 1/8"$ 15% clays - Red brown   |
| 320'  | ↓          |                 |              |          |         | Fine gravels ALMOST A SAND  |
| 325'  | ↓          |                 |              |          |         | Gravels, coarse $\leq 1/8"$ ,   |
| 330'  | ↓          |                 |              |          |         | gravels, 20% clays no change from 300 area  |
| 335'  | ↓          |                 |              |          |         | gravels, $\leq 1/8"$ , $\&$ to subrounded, 15% clays.   |
| 340'  | ↓          |                 |              |          |         | gravels " Appears to be sandier, less silty, less cohesive  |
| 345'  | ↓          |                 |              |          |         | gravels - no apparent s, 15% clays.   |
| 350'  | ↓          |                 |              |          |         | " " No change in lithologies -  |
| 360'  |            |                 |              |          |         | gravels, 15-20% clays -   |
| 370'  |            |                 |              |          |         | gravels, $\leq 1/8"$ , clays - 10% reddish brown, not as cohesive or prominent but still present. |
| 374'  |            |                 |              |          |         |   |

APPENDIX B  
GEOPHYSICAL LOG



**WILLIAM E. NORK, Inc.**

*Reno, Nevada 89503*



APPENDIX C  
CONSTRUCTION SUMMARY



**WILLIAM E. NORK, Inc.**

*Reno, Nevada 89503*

LOCATION OR COORDS: ELKO JR. High

ELEVATION: GROUND LEVEL \_\_\_\_\_

TOP OF CASING \_\_\_\_\_

DRILLING SUMMARY:

TOTAL DEPTH 239'

BOREHOLE DIAMETER 12"

DRILLER Ray Reynolds

RIG Schramm T-64-HB

BIT(S) 1 1/4"

DRILLING FLUID MUD, water,  
(Rotary)

SURFACE CASING \_\_\_\_\_

WELL DESIGN:

BASIS: GEOLOGIC LOG YES GEOPHYSICAL LOG YES

CASING STRING(S): C=CASING S=SCREEN

|             |             |           |  |  |
|-------------|-------------|-----------|--|--|
| <u>2.5'</u> | <u>50'</u>  | <u>C1</u> |  |  |
| <u>50'</u>  | <u>100'</u> | <u>S1</u> |  |  |
| <u>100'</u> | <u>220'</u> | <u>S2</u> |  |  |
| <u>220'</u> | <u>239'</u> | <u>C2</u> |  |  |

CASING: C1 8 1/2" O.D. x 0.250

C2 8 5/8" O.D x 0.250

C3 \_\_\_\_\_

C4 \_\_\_\_\_

S1 Double perf 8 7/8" O.D. x 0.250"

S2 Single per 8 7/8" O.D. x 0.250"

S3 \_\_\_\_\_

S4 \_\_\_\_\_

CENTRALIZERS Every 2 lengths of casing  
N 40' apart

FILTER MATERIAL gravel,  $\geq 1/4"$  no shales  
OR carbonates.

CEMENT NEAT CEMENT & BENTONITE

OTHER \_\_\_\_\_

CONSTRUCTION TIME LOG:

| TASK | START |      | FINISH |      |
|------|-------|------|--------|------|
|      | DATE  | TIME | DATE   | TIME |

DRILLING:

|                        |             |                |             |                |
|------------------------|-------------|----------------|-------------|----------------|
| <u>12.25" DIAMETER</u> | <u>7-15</u> | <u>9:30 AM</u> | <u>7-21</u> | <u>5:00 PM</u> |
|------------------------|-------------|----------------|-------------|----------------|

|                   |             |                 |             |                |
|-------------------|-------------|-----------------|-------------|----------------|
| GEOPHYS. LOGGING: | <u>7-22</u> | <u>11:00 AM</u> | <u>7-22</u> | <u>1:00 PM</u> |
|-------------------|-------------|-----------------|-------------|----------------|

CASING:

|                           |             |                 |             |                |
|---------------------------|-------------|-----------------|-------------|----------------|
| <u>8 5/8" O.D. 0.250"</u> | <u>7-25</u> | <u>11:00 AM</u> | <u>7-25</u> | <u>5:00 PM</u> |
|---------------------------|-------------|-----------------|-------------|----------------|

WALL THICKNESS \_\_\_\_\_

FILTER PLACEMENT:

|   |             |                |             |                |
|---|-------------|----------------|-------------|----------------|
| { | <u>7-25</u> | <u>5:00 PM</u> | <u>7-25</u> | <u>6:00 PM</u> |
|   | <u>7-26</u> | <u>9:30 PM</u> | <u>7-26</u> | <u>2:00 PM</u> |

CEMENTING: \_\_\_\_\_

|              |             |                |             |                |
|--------------|-------------|----------------|-------------|----------------|
| DEVELOPMENT: | <u>7-25</u> | <u>5:00 PM</u> | <u>7-30</u> | <u>5:00 PM</u> |
|--------------|-------------|----------------|-------------|----------------|

OTHER: \_\_\_\_\_

WELL DEVELOPMENT:

7-25-86 1 hr  
7-26-86 5 hrs - press. air  
7-29-86 Surge Block 8 hrs.

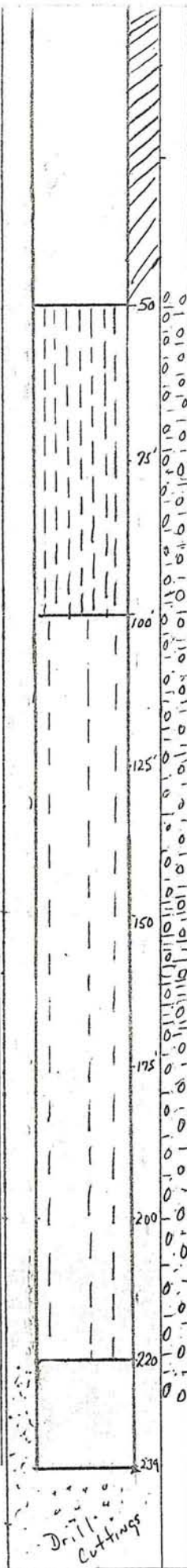
COMMENTS:

Borehole drilled to 350 feet  
BACK FILLED to 239 feet.  
Blank casing from 239 to 220'  
Single perforated casing from  
220 to 100 feet. Double per-  
forated casing from 100 to  
50' Blank casing from 50  
feet to +1.5' ABOVE LAND  
SURFACE.

LOCATION Elko Jr. High School

PERSONNEL TKG

PROJECT 86





APPENDIX D  
FIELD DATA SHEETS



**WILLIAM E. NORK, Inc.**

*Reno, Nevada 89503*

TYPE OF PUMPING TEST STEP-DRAWDOWN

PUMPING/RECOVERY DATA

M.P. FOR WATER LEVELS TOP OF STILLING WELL (+1.58')

DISTANCE FROM PUMPING WELL \_\_\_\_\_

LOCATION ELKO JUNIOR HIGH SCHOOL

PUMPING/OBSERVATION WELL \_\_\_\_\_

OTHER OBSERVATION WELL(S) \_\_\_\_\_

PUMP ON: DATE 7-30 TIME 1800PUMP OFF: DATE 7-31 TIME 0600

| CLOCK TIME | ELAPSED TIME (minutes) |    | t/t' | WATER LEVEL MEASUREMENT (feet) |         | PUMPING RATE (gpm) |   | REMARKS                          |
|------------|------------------------|----|------|--------------------------------|---------|--------------------|---|----------------------------------|
|            | t                      | t' |      | 92.65                          | ⊕ or s' | 15gpm              | Q |                                  |
| 1800       | 0                      |    |      | 92.65                          |         | 40                 |   | 40gpm MURKY WATER ADJUST FLOW    |
| 1801       | 1                      |    |      | 102.20                         | 9.55    | 15                 |   | ADJUST FLOW                      |
| 1803       | 3                      |    |      | 98.70                          | 6.05    | "                  |   | MURKY                            |
| 1805       | 5                      |    |      | 97.70                          | 5.05    | "                  |   |                                  |
| 1807       | 7                      |    |      | 97.59                          | 4.94    | "                  |   | WATER CLEARING                   |
| 1809       | 9                      |    |      | 97.51                          | 4.86    | "                  |   |                                  |
| 1812       | 12                     |    |      | 97.69                          | 5.04    | "                  |   | ADJUST FLOW, WATER CLEARING      |
| 1816       | 16                     |    |      | 98.11                          | 5.46    | "                  |   |                                  |
| 1820       | 20                     |    |      | 98.10                          | 5.45    | "                  |   | ADJUST FLOW                      |
| 1825       | 25                     |    |      | 98.56                          | 5.91    | "                  |   | WATER CLEAR 64°F                 |
| 1830       | 30                     |    |      | 98.67                          | 6.02    |                    |   | EC = 600 ppm                     |
| 1835       | 35                     |    |      | 98.65                          | 6.00    |                    |   | ADJUST FLOW                      |
| 1840       | 40                     |    |      | 98.56                          | 5.91    | 15gpm              |   | T = 63°F, CLEAR                  |
| 1850       | 50                     |    |      | 98.50                          | 5.85    |                    |   |                                  |
| 1900       | 60                     |    |      | 98.57                          | 5.92    |                    |   |                                  |
| 1915       | 75                     |    |      | 98.69                          | 6.04    |                    |   | WATER CLEAR, (600 ppm = EC)      |
| 1930       | 90                     |    |      | 98.74                          | 6.09    |                    |   | WATER CLEAR, 64°F, EC = 600 ppm. |
| 1945       | 105                    |    |      | 98.81                          | 6.16    |                    |   | clear                            |
| 2000       | 120                    |    |      | 98.86                          | 6.21    |                    |   |                                  |
| 2015       | 135                    |    |      | 98.94                          | 6.29    |                    |   | T = 65°F, 600 ppm = EC.          |
| 2030       | 150                    |    |      | 98.95                          | 6.30    |                    |   |                                  |
| 2100       | 180                    |    |      | 99.01                          | 6.36    |                    |   | EC = 600 ppm, T = 65°F           |
| 2130       | 210                    |    |      | 99.07                          | 6.42    |                    |   |                                  |
| 2200       | 240                    |    |      | 99.16                          | 6.51    | 30gpm              |   | Pump INCREASED to 30 GPM.        |

TYPE OF PUMPING TEST STEP DRAWDOWN  
PUMPING/RECOVERY DATA  
 M.P. FOR WATER LEVELS TOP OF STILLING WELL  
 DISTANCE FROM PUMPING WELL \_\_\_\_\_  
 LOCATION ELKO JUNIOR HIGH SCHOOL

PUMPING/OBSERVATION WELL \_\_\_\_\_  
 OTHER OBSERVATION WELL(S) \_\_\_\_\_  
 PUMP ON: DATE 7-30 TIME 1800  
 PUMP OFF: DATE 7-31 TIME 0600

| CLOCK TIME | ELAPSED TIME (minutes) |     | t/t' | WATER LEVEL MEASUREMENT (feet) |          | PUMPING RATE (gpm) |   | REMARKS                                    |
|------------|------------------------|-----|------|--------------------------------|----------|--------------------|---|--|
|            | t                      | t'  |      | 92.65                          | s. or s' |                    | Q |  |
| 2201       | 1                      | 241 |      | 103.00                         | 10.35    | 30 gpm             |   |  |
| 2203       | 3                      | 243 |      | 102.45                         | 9.80     | "                  |   |  |
| 2205       | 5                      | 245 |      | 102.42                         | 9.77     | "                  |   | clear                                      |
| 2207       | 7                      | 247 |      | 102.43                         | 9.78     | "                  |   |  |
| 2209       | 9                      | 249 |      | 102.56                         | 9.91     | "                  |   |  |
| 2212       | 12                     | 252 |      | 102.65                         | 10.00    | "                  |   |  |
| 2215       | 15                     | 255 |      | 102.66                         | 10.01    | "                  |   | clear                                      |
| 2218       | 18                     | 258 |      | 102.75                         | 10.10    | "                  |   |  |
| 2221       | 21                     | 261 |      | 102.83                         | 10.18    | "                  |   |  |
| 2225       | 25                     | 265 |      | 102.93                         | 10.28    | "                  |   | T=62°F, E.C.=500 ppm                       |
| 2230       | 30                     | 270 |      | 102.98                         | 10.33    | "                  |   |  |
| 2235       | 35                     | 275 |      | 103.07                         | 10.42    | "                  |   |  |
| 2240       | 40                     | 280 |      | 103.08                         | 10.43    | "                  |   | clear                                      |
| 2250       | 50                     | 290 |      | 103.16                         | 10.51    | "                  |   |  |
| 2300       | 60                     | 300 |      | 103.27                         | 10.62    | "                  |   |  |
| 2315       | 75                     | 315 |      | 103.39                         | 10.74    | "                  |   |  |
| 2330       | 90                     | 330 |      | 103.51                         | 10.86    | "                  |   | clear                                      |
| 2345       | 105                    | 345 |      | 103.56                         | 10.91    | "                  |   |  |
| 2400       | 120                    | 360 |      | 103.68                         | 11.03    | "                  |   | T=62°F E.C.=600 ppm                        |
| 0015       | 135                    | 375 |      | 103.63                         | 10.98    | "                  |   | clear                                      |
| 0030       | 150                    | 390 |      | 103.83                         | 11.18    | "                  |   |  |
| 0100       | 180                    | 420 |      | 103.88                         | 11.23    | "                  |   |  |
| 0130       | 210                    | 450 |      | 103.99                         | 11.34    | "                  |   | T=62°F E.C.=600 ppm<br>METALS SAMPLE TAKEN |

TYPE OF PUMPING TEST STEP-DRAWDOWNPUMPING RECOVERY DATAM.P. FOR WATER LEVELS TOP OF STILLING WELL

DISTANCE FROM PUMPING WELL \_\_\_\_\_

LOCATION ELKO INSPUMPING OBSERVATION WELL  
OTHER OBSERVATION WELL(S) \_\_\_\_\_PUMP ON: DATE 7-30 TIME 1800PUMP OFF: DATE 7-31 TIME 0600

| CLOCK TIME | ELAPSED TIME (minutes) |     | t/t' | WATER LEVEL MEASUREMENT (feet) |          | PUMPING RATE (gpm) |   | REMARKS                  |
|------------|------------------------|-----|------|--------------------------------|----------|--------------------|---|--------------------------|
|            | t                      | t'  |      | 92.65                          | s. or s' |                    | Q |                          |
| 0200       | 240                    | 480 |      | 103.99                         | 11.34    |                    |   | clear                    |
| 0201       | 1                      | 481 |      | 109.80                         | 17.15    | 50                 |   | Δ FLOW RATE 50-60 gpm    |
| 0203       | 3                      | 483 |      | 113.83                         | 21.18    | 60                 |   | MURKY WATER.             |
| 0205       | 5                      | 485 |      | 115.20                         | 22.55    |                    |   |                          |
| 0207       | 7                      | 487 |      | 115.81                         | 23.16    | 60                 |   |                          |
| 0209       | 9                      | 489 |      | 116.28                         | 23.63    |                    |   |                          |
| 0212       | 12                     | 492 |      | 116.68                         | 24.03    |                    |   | cloudy water             |
| 0216       | 16                     | 496 |      | 117.11                         | 24.46    | 60                 |   |                          |
| 0220       | 20                     | 500 |      | 117.42                         | 24.77    |                    |   | slightly clouded         |
| 0225       | 25                     | 505 |      | 117.72                         | 25.07    |                    |   | clear                    |
| 0230       | 30                     | 510 |      | 118.30                         | 25.65    |                    |   |                          |
| 0240       | 40                     | 520 |      | 118.48                         | 25.83    |                    |   | clear                    |
| 0250       | 50                     | 530 |      | 118.88                         | 26.23    |                    |   |                          |
| 0300       | 60                     | 540 |      | 119.11                         | 26.46    |                    |   | T = 61°F, E.C. = 500 ppm |
| 0315       | 75                     | 555 |      | 119.23                         | 26.58    |                    |   | clear                    |
| 0330       | 90                     | 570 |      | 119.44                         | 26.79    |                    |   |                          |
| 0345       | 105                    | 585 |      | 119.62                         | 26.97    |                    |   |                          |
| 0400       | 120                    | 600 |      | 119.57                         | 26.92    |                    |   |                          |
| 0415       | 135                    | 615 |      | 119.82                         | 27.17    |                    |   | 61°F, E.C. = 500 ppm     |
| 0430       | 150                    | 630 |      | 119.63                         | 26.98    |                    |   |                          |
| 0500       | 180                    | 660 |      | 120.01                         | 27.36    |                    |   | clear                    |
| 0530       | 210                    | 690 |      | 120.29                         | 27.52    |                    |   |                          |
| 0600       | 240                    | 720 |      | 120.17                         | 27.52    |                    |   | PUMP OFF!                |

**PUMPING TEST DATA**

WELL NO. ELKO JHS G.O.W. #1

TYPE OF PUMPING TEST STEP-DRAWDOWN  
 PUMPING/RECOVERY DATA  
 M.P. FOR WATER LEVELS TOP OF STILLING WELL  
 DISTANCE FROM PUMPING WELL \_\_\_\_\_  
 LOCATION ELKO JUNIOR HIGH SCHOOL

PUMPING/OBSERVATION WELL \_\_\_\_\_  
 OTHER OBSERVATION WELL(S) \_\_\_\_\_  
 PUMP ON: DATE 7-31 TIME 0600  
 PUMP OFF: DATE 7-31 TIME \_\_\_\_\_

| CLOCK TIME | ELAPSED TIME (minutes) |    | t/t' | WATER LEVEL MEASUREMENT (feet) |          | PUMPING RATE (gpm) |   | REMARKS          |
|------------|------------------------|----|------|--------------------------------|----------|--------------------|---|------------------|
|            | t                      | t' |      |                                | s. or s' |                    | Q |                  |
| 0605       | 5                      | 5  |      | 101.85                         |          |                    |   | 66.6% RECOVERED  |
|            | 725                    |    |      |                                |          |                    |   |                  |
| 0610       | 10                     |    |      | 100.92                         |          |                    |   | 70.0%            |
|            | 730                    |    |      |                                |          |                    |   |                  |
| 0615       | 15                     |    |      | 100.17                         |          |                    |   | 72.7%            |
|            | 735                    |    |      |                                |          |                    |   |                  |
| 0620       | 20                     |    |      | 99.65                          |          |                    |   | 74.6%            |
|            | 740                    |    |      |                                |          |                    |   |                  |
| 0630       | 30                     |    |      | 98.87                          |          |                    |   | 77.4%            |
|            | 750                    |    |      |                                |          |                    |   |                  |
| 0645       | 45                     |    |      | 98.13                          |          |                    |   | 80.1%            |
|            | 765                    |    |      |                                |          |                    |   |                  |
| 0700       | 60                     |    |      | 97.61                          |          |                    |   | 82.0%            |
|            | 780                    |    |      |                                |          |                    |   |                  |
| 0730       | 90                     |    |      | 95.11                          |          |                    |   | 91.1%            |
|            | 810                    |    |      |                                |          |                    |   |                  |
| 0800       | 120                    |    |      | 94.70                          |          |                    |   | 92.5% RECOVERED  |
|            | 840                    |    |      |                                |          |                    |   |                  |
| 1800       |                        |    |      | 94.70                          |          |                    |   | 92.5% RECOVERED. |

TYPE OF PUMPING TEST CONSTANT DISCHARGE~~PUMPING/RECOVERY DATA~~M.P. FOR WATER LEVELS TOD OF STILLING WELL (+1.58')

DISTANCE FROM PUMPING WELL \_\_\_\_\_

LOCATION ELKO JUNIOR HIGH SCHOOL~~PUMPING/OBSERVATION WELL~~

OTHER OBSERVATION WELL(S) \_\_\_\_\_

PUMP ON: DATE 7-31 TIME 1800PUMP OFF: DATE 8-1 TIME 1800

| CLOCK TIME | ELAPSED TIME (minutes) |    | t/t' | WATER LEVEL MEASUREMENT (feet) |           | PUMPING RATE (gpm) |   | REMARKS                         |
|------------|------------------------|----|------|--------------------------------|-----------|--------------------|---|---------------------------------|
|            | t                      | t' |      | 94.70                          | (s) or s' | 50                 | Q |                                 |
| 1800       | 1                      |    |      | 105.00                         | 10.3      | 60                 |   | 60 gpm - ADJUST FLOW            |
| 1803       | 3                      |    |      | 108.08                         | 13.38     | 60                 |   | ADJUST FLOW (DECREASE)          |
| 1805       | 5                      |    |      | 109.37                         | 14.67     | 60                 |   | " " "                           |
| 1807       | 7                      |    |      | 109.91                         | 15.21     | 60                 |   | " " "                           |
| 1809       | 9                      |    |      | 107.03                         | 12.33     | 50                 |   | FLOW CLEAR                      |
| 1812       | 12                     |    |      | 106.42                         | 11.72     |                    |   |                                 |
| 1816       | 16                     |    |      | 106.32                         | 11.62     | 50                 |   | CLEAR                           |
| 1820       | 20                     |    |      | 106.36                         | 11.66     |                    |   |                                 |
| 1825       | 25                     |    |      | 106.61                         | 11.91     | 50                 |   | T=62°F, E.C.=750 mhos           |
| 1830       | 30                     |    |      | 106.78                         | 12.08     |                    |   |                                 |
| 1835       | 35                     |    |      | 107.08                         | 12.38     |                    |   |                                 |
| 1840       | 40                     |    |      | 107.09                         | 12.39     |                    |   | CLEAR                           |
| 1850       | 50                     |    |      | 107.41                         | 12.71     |                    |   |                                 |
| 1900       | 60                     |    |      | 107.57                         | 12.87     |                    |   |                                 |
| 1920       | 80                     |    |      | 107.91                         | 13.21     |                    |   |                                 |
| 1940       | 100                    |    |      | 108.19                         | 13.49     |                    |   |                                 |
| 2000       | 120                    |    |      | 108.24                         | 13.54     | 50                 |   | T=62°F, E.C.=750 mhos           |
| 2030       | 150                    |    |      | 108.30                         | 13.60     |                    |   |                                 |
| 2100       | 180                    |    |      |                                |           |                    |   |                                 |
| 2147       | 227                    |    |      | 108.86                         | 14.16     |                    |   | clear                           |
| 2200       | 240                    |    |      |                                |           |                    |   |                                 |
| 2230       | 270                    |    |      | 109.08                         | 14.38     |                    |   | T=61°F, E.C.=800 mhos           |
| 2300       | 300                    |    |      | 109.38                         | 14.68     |                    |   |                                 |
| 2330       | 330                    |    |      | 109.55                         | 14.85     | 50                 |   |                                 |
| 2400       | 360                    |    |      | 109.61                         | 14.91     | 50                 |   | T=63°F, E.C.=800 μmhos, pH=7.29 |



WELL NO. ELKO JHS G.O.W. #1

TYPE OF PUMPING TEST CONSTANT DISCHARGE  
 PUMPING/RECOVERY DATA  
 M.P. FOR WATER LEVELS TOP OF STILLING WELL  
 DISTANCE FROM PUMPING WELL \_\_\_\_\_  
 LOCATION ELKO JUNIOR HIGH SCHOOL

PUMPING/OBSERVATION WELL \_\_\_\_\_  
 OTHER OBSERVATION WELL(S) \_\_\_\_\_

PUMP ON: DATE 8-1 TIME 1800  
 PUMP OFF: DATE 8-2 TIME 0600

| CLOCK TIME | ELAPSED TIME (minutes) |      | t/t' | WATER LEVEL MEASUREMENT (feet) |          | PUMPING RATE (gpm) |   | REMARKS |
|------------|------------------------|------|------|--------------------------------|----------|--------------------|---|---------|
|            | t                      | t'   |      | 94.7                           | s. or s' |                    | Q |         |
| 1801       | 1                      | 1441 | 1    | 1441                           | 99.80    | 5.1                |   |         |
| 1803       | 3                      | 1443 | 3    | 481                            | 100.29   | 5.59               |   |         |
| 1805       | 5                      | 1445 | 5    | 289                            | 100.09   | 5.39               |   |         |
| 1807       | 7                      | 1447 | 7    | 207                            | 99.79    | 5.09               |   |         |
| 1809       | 9                      | 1449 | 9    | 161                            | 99.62    | 4.92               |   |         |
| 1812       | 12                     | 1452 | 12   | 121                            | 99.32    | 4.62               |   |         |
| 1816       | 16                     | 1456 | 16   | 91                             | 99.07    | 4.37               |   |         |
| 1820       | 20                     | 1460 | 20   | 73                             | 98.77    | 4.07               |   |         |
| 1825       | 25                     | 1465 | 25   | 59                             | 98.37    | 3.67               |   |         |
| 1830       | 30                     | 1470 | 30   | 49                             | 98.37    | 3.67               |   |         |
| 1840       | 40                     | 1480 | 40   | 37                             | 97.98    | 3.28               |   |         |
| 1850       | 50                     | 1490 | 50   | 30                             | 97.80    | 3.10               |   |         |
| 1900       | 60                     | 1500 | 60   | 25                             | 97.29    | 2.59               |   |         |
| 1915       | 75                     | 1515 | 75   | 20                             |          |                    |   |         |
| 1930       | 90                     | 1530 | 90   | 17                             |          |                    |   |         |
| 1945       | 105                    | 1545 | 105  | 14.7                           |          |                    |   |         |
| 2000       | 120                    | 1560 | 120  | 13                             |          |                    |   |         |
| 2030       | 150                    | 1590 | 150  | 10.6                           | 96.39    | 1.69               |   |         |
| 2100       | 180                    | 1620 | 180  | 9                              | 96.33    | 1.63               |   |         |
| 2130       | 210                    | 1650 | 210  | 7.8                            |          |                    |   |         |
| 2200       | 240                    | 1680 | 240  | 7                              | 96.07    | 1.37               |   |         |
| 2300       | 300                    | 1740 | 300  | 5.8                            | 95.94    | 1.24               |   |         |
| 2400       | 360                    | 1800 | 360  | 5                              | 95.83    | 1.13               |   |         |
| 0200       | 480                    | 1920 | 480  | 4                              | 95.67    | .97                |   |         |
| 0615       | 735                    | 2175 | 735  | 3.0                            | 95.48    | .78                |   |         |



PUMPING TEST DATA

WELL NO. ELKO JHS GOW #1

TYPE OF PUMPING TEST INJECTION  
 (PUMPING) RECOVERY DATA  
 M.P. FOR WATER LEVELS TOP OF STILLING WELL  
 DISTANCE FROM PUMPING WELL \_\_\_\_\_  
 LOCATION ELKO JHS

~~PUMPING~~/OBSERVATION WELL  
 OTHER OBSERVATION WELL(S) \_\_\_\_\_  
 PUMP ON: DATE 8-2-86 TIME 0815  
 PUMP OFF: DATE 8-3-86 TIME 0815

| CLOCK TIME | ELAPSED TIME (minutes) |    | t/t' | WATER LEVEL MEASUREMENT (feet) |          | PUMPING RATE (gpm) |   | REMARKS             |
|------------|------------------------|----|------|--------------------------------|----------|--------------------|---|---------------------|
|            | t                      | t' |      | 95.00                          | s. or s' | 60                 | Q |                     |
| 0815       | 0                      |    |      | 95.00                          | 0        |                    |   |                     |
| 0840       | 25                     |    |      | 87.50                          |          |                    |   |                     |
| 0845       | 30                     |    |      | 87.34                          | 7.66'    | 37.2               |   |                     |
| 0900       | 45                     |    |      | 86.83                          | 8.17     | 34.1               |   | ΔQ (increased flow) |
| 0915       | 60                     |    |      | 79.30                          | 15.7     | 70.5               |   |                     |
| 0930       | 75                     |    |      | 77.70                          | 17.3     | 51.6               |   |                     |
| 0945       | 90                     |    |      | 76.90                          | 18.1     | 56.4               |   |                     |
| 1000       | 105                    |    |      | 76.29                          | 18.71    | 53.8               |   | ΔQ (increased flow) |
| 1015       | 120                    |    |      | 1.9                            | 93.1     | 114.07             |   | ΔQ (decreased flow) |
| 1030       | 135                    |    |      | 26.35                          | 68.6     | 65.25              |   |                     |
| 1045       | 150                    |    |      | 25.71                          | 69.3     | 63.03              |   |                     |
| 1100       | 165                    |    |      | 23.58                          | 71.4     | 62.33              |   |                     |
| 1115       | 180                    |    |      | 22.26                          | 72.7     | 66.82              |   |                     |
| 1130       | 195                    |    |      | 21.09                          | 73.9     | 62.03              |   |                     |
| 1145       | 210                    |    |      | 20.02                          | 75       | 61.43              |   |                     |
| 1200       | 225                    |    |      | 19.21                          | 75.8     | 61.14              |   |                     |
| 1230       | 255                    |    |      | 17.80                          | 77.2     | 60.8               |   |                     |
| 1300       | 285                    |    |      | 16.69                          | 78.3     | 58.5               |   |                     |
| 1330       | 315                    |    |      | 15.87                          | 79.1     | 60.4               |   |                     |
| 1400       | 345                    |    |      | 15.35                          | 79.6     | 59.9               |   |                     |
| 1430       | 375                    |    |      | 14.82                          | 80.2     | 60.1               |   |                     |
| 1500       | 405                    |    |      | 14.21                          | 80.8     | 60.3               |   |                     |
| 1530       | 435                    |    |      | 13.35                          | 81.65    | 60.7               |   |                     |
| 1600       | 465                    |    |      | 12.71                          | 82.29    | 61.5               |   |                     |
| 1630       | 495                    |    |      | 12.46                          | 82.5     | 60.9               |   |                     |
| 1700       | 525                    |    |      | 12.25                          | 82.75    | 61.0               |   |                     |
| 1730       | 555                    |    |      | 11.99                          | 83.0     | 61.0               |   |                     |



APPENDIX E  
INPUT FOR VAREFLOW MODEL



**WILLIAM E. NORK, Inc.**

*Reno, Nevada 89503*

Number of discharging wells = 9

| City of Elko<br>Well Number | Coordinates |       |
|-----------------------------|-------------|-------|
|                             | X           | Y     |
| 1                           | 200         | 5400  |
| 20                          | 100         | 6700  |
| 13                          | 3700        | 1050  |
| 12                          | 4500        | 10500 |
| 10A                         | 6100        | 8700  |
| 19                          | 8300        | 7600  |
| 18                          | 6100        | 4900  |
| 15                          | 6400        | 1500  |
| 16                          | 8200        | 2500  |

Transmissivity =  $2,273 \text{ FT}^2/\text{day}$

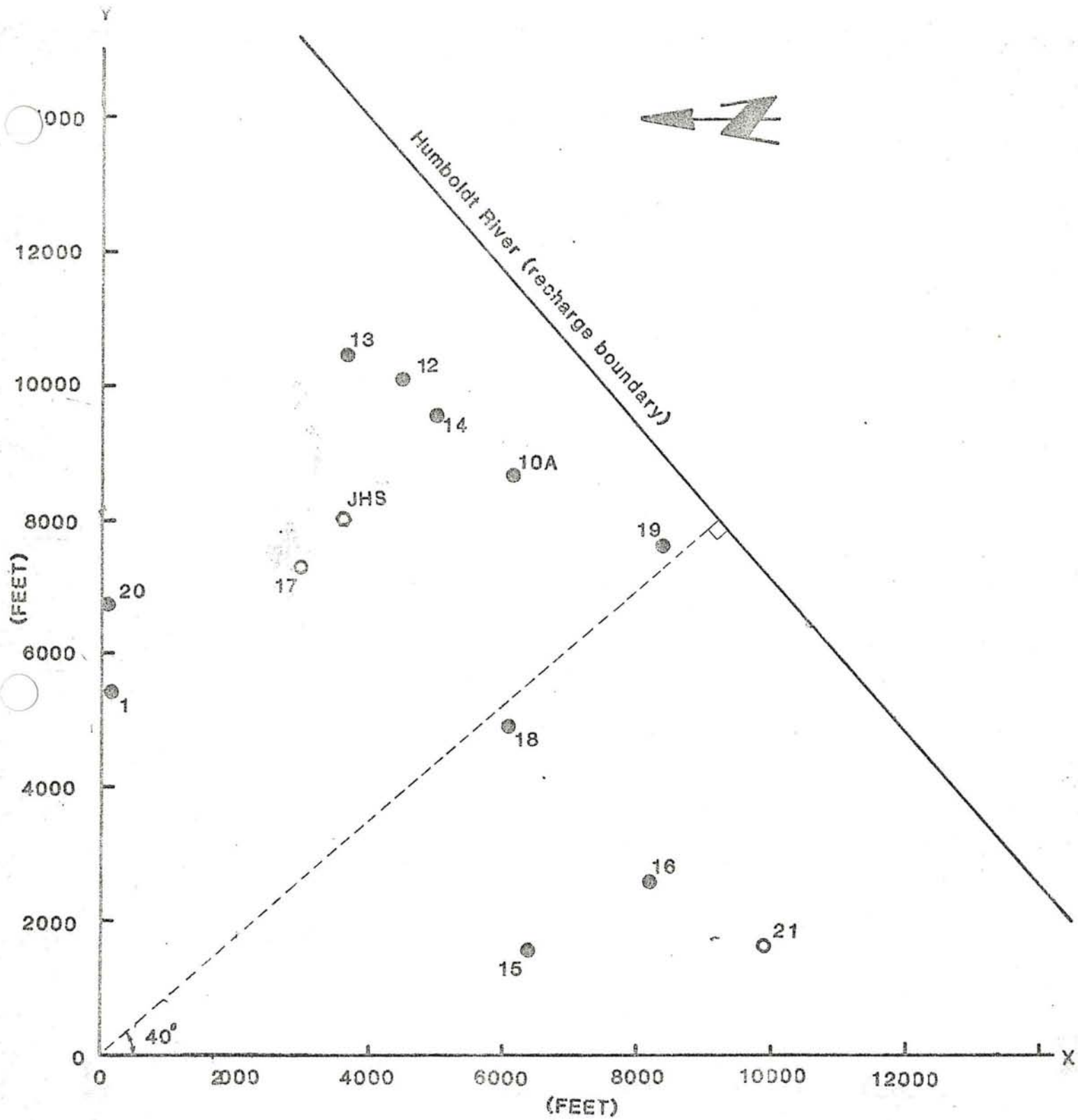
Coefficient of Storage = 0.001

Recharge boundary located 12,200 feet from origin

Angle between X-axis and normal to boundary = 40 degrees



**WILLIAM E. NORK, Inc.**



VARFLOW Model Layout

● City Well used in simulation



WILLIAM E. NORK, Inc.

Reno, Nevada 89503

Pumping Schedule

| Time since simulation started (days) | Discharge rate (cubic feet/day) |
|--------------------------------------|---------------------------------|
|--------------------------------------|---------------------------------|

City Well No. 1

|           |        |
|-----------|--------|
| 0 - 90    | 0      |
| 90 - 120  | 10,415 |
| 120 - 150 | 19,025 |
| 150 - 180 | 26,728 |
| 180 - 210 | 30,458 |
| 210 - 240 | 33,822 |
| 240 - 270 | 4,335  |
| 270 - 300 | 8,198  |
| 300 - 360 | 0      |

City Well No. 20

|           |         |
|-----------|---------|
| 0 - 60    | 0       |
| 60 - 90   | 1,128   |
| 90 - 120  | 32,618  |
| 120 - 150 | 50,578  |
| 150 - 180 | 111,992 |
| 180 - 210 | 88,516  |
| 210 - 240 | 116,738 |
| 240 - 270 | 35,856  |
| 270 - 300 | 2,161   |
| 300 - 360 | 0       |

City Well No. 13

|           |        |
|-----------|--------|
| 0 - 150   | 0      |
| 150 - 180 | 94,770 |
| 180 - 210 | 91,933 |
| 210 - 240 | 90,956 |
| 240 - 270 | 31,186 |
| 270 - 360 | 0      |

City Well No. 12

|         |         |
|---------|---------|
| 0 - 30  | 105,808 |
| 30 - 60 | 95,439  |
| 60 - 90 | 91,655  |



|           |         |
|-----------|---------|
| 90 - 120  | 101,230 |
| 120 - 150 | 102,296 |
| 150 - 180 | 95,861  |
| 180 - 210 | 97,231  |
| 210 - 240 | 96,817  |
| 240 - 270 | 95,914  |
| 270 - 300 | 101,529 |
| 300 - 330 | 97,978  |
| 330 - 360 | 101,604 |

City Well No. 10A

|           |        |
|-----------|--------|
| 0 - 30    | 20,495 |
| 30 - 60   | 20,132 |
| 60 - 90   | 21,265 |
| 90 - 120  | 46,375 |
| 120 - 150 | 55,755 |
| 150 - 180 | 53,379 |
| 180 - 210 | 38,780 |
| 210 - 240 | 34,509 |
| 240 - 270 | 48,523 |
| 270 - 300 | 41,837 |
| 300 - 330 | 36,183 |
| 330 - 360 | 22,323 |

City Well No. 19

|           |         |
|-----------|---------|
| 0 - 30    | 83,873  |
| 30 - 60   | 82,450  |
| 60 - 90   | 111,298 |
| 90 - 120  | 136,978 |
| 120 - 150 | 155,597 |
| 150 - 180 | 147,473 |
| 180 - 210 | 149,894 |
| 210 - 240 | 26,597  |
| 240 - 270 | 0       |
| 270 - 300 | 988     |
| 300 - 330 | 0       |
| 330 - 360 | 0       |

City Well No. 18

|           |         |
|-----------|---------|
| 0 - 150   | 0       |
| 150 - 180 | 38,298  |
| 180 - 210 | 104,608 |
| 210 - 240 | 9,886   |
| 240 - 360 | 0       |



City Well No. 15

|           |        |
|-----------|--------|
| 0 - 30    | 54,401 |
| 30 - 60   | 72,281 |
| 60 - 90   | 52,528 |
| 90 - 120  | 78,428 |
| 120 - 150 | 83,343 |
| 150 - 180 | 83,611 |
| 180 - 210 | 61,856 |
| 240 - 270 | 60,476 |
| 270 - 300 | 38,387 |
| 300 - 330 | 31,720 |
| 330 - 360 | 24,698 |

City Well No. 16

|           |        |
|-----------|--------|
| 0 - 150   | 0      |
| 150 - 180 | 21,271 |
| 180 - 210 | 83,099 |
| 210 - 240 | 80,388 |
| 240 - 270 | 83,261 |
| 270 - 300 | 83,924 |
| 300 - 330 | 81,681 |
| 330 - 360 | 84,800 |







**WILLIAM E. NORK, Inc.**

*Reno, Nevada 89503*