GLODOLA

DOE/ET/27005-1

GEOTHERMAL RESERVOIR ASSESSMENT CASE STUDY NORTHERN BASIN AND RANGE PROVINCE LEACH HOT SPRINGS AREA PERSHING COUNTY, NEVADA

FINAL REPORT FOR THE PERIOD APRIL, 1979 THROUGH DECEMBER, 1981

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PREPARED FOR THE U.S. DEPARTMENT OF ENERGY DIVISION OF ENERGY TECHNOLOGY UNDER CONTRACT DE AC 08-79 ET 27005

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ABSTRACT

Aminoil USA, Inc. has conducted a Geothermal Reservoir Assessment Case Study in the Leach Hot Springs Known Geothermal Resource Area of Pershing County, Nevada. The case study included the drilling of twenty-three temperature gradient wells, a magnetotelluric survey, seismic data acquisition and processing, and the drilling of one exploratory well. Existing data from prior investigations, which included water geochemistry, gravity, photogeologic reports and a hydrothermal alteration study, was also provided to the DOE.

The exploratory well was drilled to total depth of 8565' with no significant mud losses or other drilling problems. A maximum temperature of 260°F was recorded at total depth. The relatively low temperature and the lack of permeability (as shown by absence of mud loss) indicated that a current, economic geothermal resource had not been located, and the well was subsequently plugged and abandoned. However, the type and extent of rock alteration found implied that an extensive hot water system had existed in this area at an earlier time.

This report is a synopsis of the case study activities and the data obtained from these activities. Detailed data is on file at the University of Utah Research Institute Earth Science Laboratory (UURI/ESL), Salt Lake City, Utah.

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INTRODUCTION

During 1979, 1980 and 1981, Aminoil USA, Inc., as Contract Operator under Department of Energy (DOE) Contract Number DE-AC08-79ET27005 and working through Field Operator, Sunoco Energy Development Co. (Sunedco), conducted a Geothermal Reservoir Assessment Case Study in the Grass Valley Area of northwestern Nevada (Figure 1). Specific areas of interest were the Leach Hot Springs Known Geothermal Resource Area (KGRA) and the Panther Canyon Area, both in Pershing County, Nevada (Figure 2).

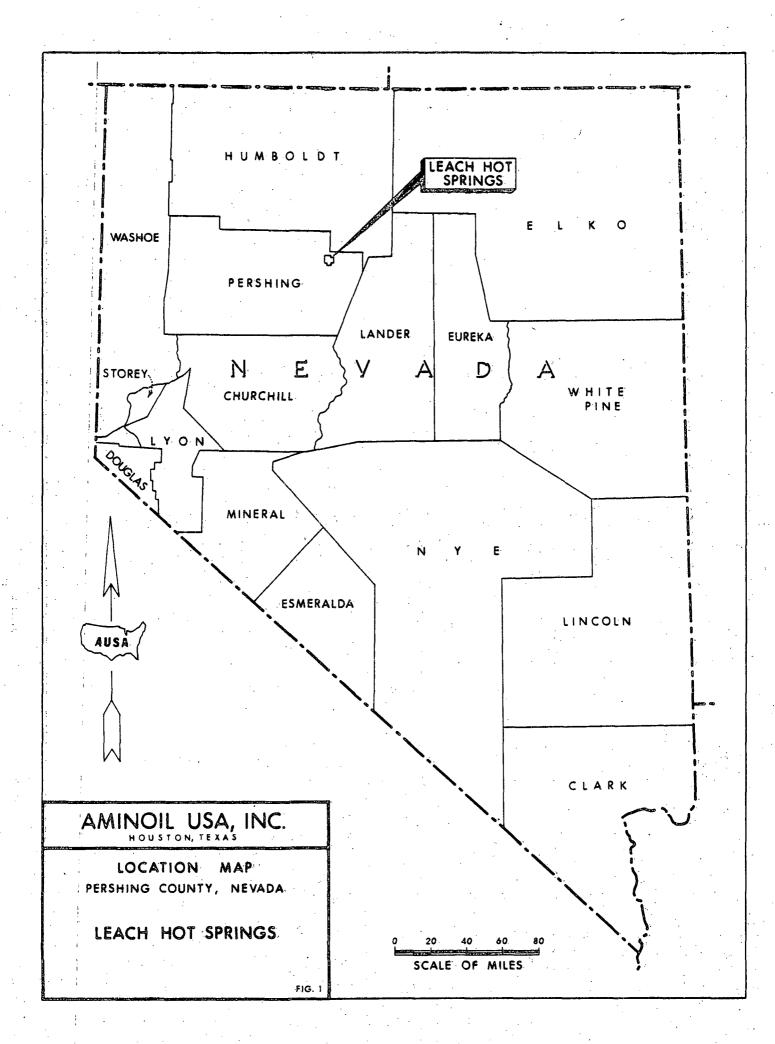
Before beginning the work planned under this contract, existing surface geological data was provided to the DOE which included:

- 1. Gravity measurements approximately 500 stations.
- 2. Gravity interpretation approximately 900 stations.
- 3. A water geochemical survey.
- 4. A hydrothermal alteration study.
- 5. A surface photogeological study.

The work performed under this contract was divided into three phases as follows:

- Phase I: Drilling and evaluation of sixteen shallow and intermediate depth temperature gradient wells.
- Phase II: A magnetotelluric survey covering thirty-nine sites and twenty-seven line miles of seismic data acquisition and evaluation.
- Phase III: Drilling and evaluation of the Leach Hot Springs USA 11-36 exploratory geothermal well and seven additional shallow temperature gradient wells.

This report is limited to a discussion of the three contract work phases as outlined above.



PHASE I

During the period June through September, 1979, thirteen shallow (282' - 500') and three intermediate (1,185' - 1,500') depth temperature gradient wells were drilled and evaluated in the Grass Valley area of northwestern Nevada.¹ The locations of these wells and of pre-existing temperature gradient wells in the area are shown in Figure 3.

A Gardner - Denver 15 W rig was used to drill the wells with mud used as the circulating medium throughout. Hard drilling and some difficulty with caving were reported for several wells. However, the only problem of any consequence was lost circulation, which resulted in the abandonment of one well at a depth of 80 ' (No. S-GV-79-5) and the subsequent drilling of a replacement well 80 yards away (No. S-GV-79-5A). Since lost circulation was a significant problem in only one well and resulted in little additional cost, no recommendations are made for its prevention.

Bottom hole temperatures measured in these wells ranged from 63 to $93^{\circ}F(17.2 - 33.9^{\circ}C)$ for the shallow wells and from 85 to $201^{\circ}F(29.6 - 94.1^{\circ}C)$ for the intermediate depth wells. Calculated heat flow values ranged as follows:

	Range of Heat Fl	ow Values, HFU ²
	Maximum	Minimum
· .	Porosity Conditions	Porosity Conditions
Shallow Wells	.15 - 5.71	.23 - 8.29
Intermediate Wells	1.54 - 9.6	2.09 - 12.9

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The heat flow values obtained in this study together with previously published values are also shown in Figure 3. The contours shown confirmed the presence of HFU anamolies (greater than 3 HFU) in both the Leach Hot Springs KGRA and the Panther Canyon Area.

¹GeothermEx, Inc., 1979, Temperature - Gradient and Heat - Flow Data, Grass Valley, Nevada: Report for Sunoco Energy Development Co., Dallas, Texas.

 2 HFU = heat flow units, 10^{-6} cal/cm² - sec. Because all holes penetrated unconsolidated alluvium, water saturated conditions were assumed throughout, and heat flow values were calculated using 20% and 40% as the minimum and maximum porosities expected in this setting.

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PHASE II

During April and May, 1979, thirty-nine magnetotelluric (MT) survey sites were occupied by Geotronics Corporation in an attempt to define the potential geothermal source and reservoir in the study area.³ Survey site locations are shown in Figure 4.

Figures 5 and 6 show the resistivity distribution at -4,000' and -12,000', respectively, as interpreted from the MT survey. The conductive anamoly shown along the east side of the survey area is interpreted to be a possible heat source, thus enhancing the potential geothermal productivity of the area.

During July, 1979, twenty-seven line miles of seismic data were obtained as shown in Figure 7. This data was utilized to help in selecting the optimum location for the exploratory well, the Leach Hot Springs USA 11-36. The seismic data confirmed that the Eastern Boundary Fault is a major tectonic element in the area and that the area to the east of the Hot Springs fault is seismically anomalous. Data quality of the seismic was insufficient to detail the structural configuration in the Panther Canyon Area.

³Geotronics Corporation, 1979, Magnetotelluric Survey of the Leach Hot Springs Area of North Central Nevada: Report for Sunoco Energy Development Co., Dallas, Texas.

PHASE III

Subsequent to the collection and analysis of the data obtained in Phases I and II, the Leach Hot Springs USA 11-36 exploratory geothermal well was spudded on May 15, 1980. Location of the well (Figure 8) was 500 ' FNL and 500 ' FWL of Section 36 - Township 32 North -Range 38 East, Pershing County, Nevada.

The USA 11-36 was drilled to a total depth of 8,565' in just over forty-three days. Mud was used as the circulating medium throughout, and no major problems were encountered during drilling. Logging, evaluation, plugging and abandoning required an additional five days, so that operations were completed in forty-eight days on July 2, 1980. Figure 9 shows the drilling time curve and casing program for the well, and Appendix A is the Daily Drilling Log.

The well was drilled through Tertiary alluvium (characterized as variable mixtures of poorly consolidated clay, sand and gravel) from the surface to a depth of 1,340'. Some silification was noted in the upper 600'. From 1,340' to 2,740', Tertiary mudstone, claystone, sand and gravel were encountered. Tertiary mudstone, claystone, sandstone, siltstone and conglomerate were penetrated from 2,740' to 4,770', with

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tuffaceous sandstone, conglomerate and siltstone predominate in the bottom 400'. An abrupt change to tertiary basalt and andesite occurred at 4,770' and continued to 5,010', where a change to silicic tuffs and tuffaceous sediments, claystone, sandstone and conglomerate was noted. An erosional unconformity between Tertiary and Triassic sediments was found at 5,330'. From 5,330' to 7,170', various forms of altered granite were drilled, while from 7,170' to TD, altered and metamorphosed basalt and granite were penetrated.

The maximum recorded temperature in the well was 260°F, reached some 63 hours after circulation had stopped (see Figure 9 for temperature surveys). This low temperature is the primary indication that the well did not locate a current, economic geothermal resource, although the lithological examination (described more fully in Figure 9) indicated that an extensive hot water system had existed in this area at an earlier time. Additionally, there were no significant mud losses during drilling which indicated that the interval penetrated by the well lacked any appreciable permeability. Due to these very discouraging results, the well was plugged and abandoned.

Initial planning for this case study included the drilling of a second exploratory well in the Panther Canyon Area (Figure 2). The disappoin-

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ting results of the USA 11-36 well prompted reevaluation of these plans. The decision was made to obtain additional temperature gradient/heat flow data in the Panther Canyon Area in an attempt to determine whether the previously mapped anomaly (Figure 3) justified further exploration efforts.

During the period March through June, 1981, six shallow depth (280' - 500') temperature gradient wells were drilled in the Panther Canyon Area.⁴ A seventh well (No. S-GV-81-85) planned as a 1,500' intermediate test was abandoned at 300' after encountering unresolvable drilling problems while trying to cement off a water zone. The locations of these wells and previously drilled temperature gradient wells are shown in Figure 10.

As during Phase I of this study, a Gardner - Denver 15 W rig was used for drilling. Foam was used as the initial circulating medium in most holes, with a switch to mud as caving/circulation problems dictated. Minor problems were encountered in most wells, but as mentioned above, the only major problem occurred in well No. S-GV-81-85, when drill pipe was cemented in the hole while trying to plug a water flow.

Bottom hole temperatures in these wells ranged from 52 to 80°F (11.2 -26.8°C. Several wells (e.g., Nos. S-GV-81-80, S-GV-81-83 and

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S-GV-81-86) had abnormally low bottom hole temperature ($52 - 55^{\circ}$ F), probably because they did not penetrate below the convective effects of shallow, cool groundwater flowing in the area. The intermediate depth test (No. S-GV-81-85) was designed to eliminate these effects, but unfortunately failed as described above. Calculated heat flow values for these wells ranged from 0.77 to 3.30 heat flow units (10^{-6} cal/cm²-sec). These heat flow values, together with previously existing data, are contoured in Figure 10. In summary, an HFU anomaly was confirmed in the Panther Canyon Area, but was judged to be of insufficient size to warrant a deep exploratory test.

These activities concluded the case study under the aforementioned DOE contract.

⁴GeothermEx, Inc., 1981. Temperature-Gradient and Heat-Flow Data, Panther Canyon, Nevada: Report for Sunoco Energy Development Co., Dallas, Texas.

APPENDIX A

DAILY DRILLING LOG

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DAILY DRILLING · WORKOVER LOG

WELL		11-36		<u>.</u>			F	Page 1 SPUDDED May 15, 19 80
ELEVAT	IONS: GN	D	· ·		BI	H		DF RDB ASING RECORD
	PIPE SI	75 6	OLE	SEA	T F.C		C/	CEMENTING DATA: Sacks, Kind, etc.
Conduct			012	022				
Surface	······							
Interme	d:							
Oll Strir	ng:							
DATE	DEPTH	FOO	т. D	EGREE	S OFF	M	UD	REMARKS
UAIE	TODAY	AG		EG.	DEPTH	WT	VIS	(Activity) (Formation) (D.S.T.) (Coring) (etc.)
5-15	150	150		<u> </u>		8.4	58.	Rig up, mix mud, rig repairs, drilling to 150'.
5-16	325	175				8.5	. 45	Survey at 150', drilling, circulate, short trip, wait on Howco and casing crew,
								had three flats on Howco and casing crew truck, rig up to run 20" casing, ran three jts. of 20" casing stop, tried to work casing by bridge, POOH
	;,,		_					with casing, stood back and laid down 1 jt., made up 26" bit and TIH to 90'.
5-17 .	325	0		· `		8.5	45	TIH and ream from 80' to 130', circulate and condition mud and wait on stab.,
								POOH, pick up 26" steel stabilizer from 70' to 325', rig up and ran 8 joints of 20" 94# K55, set 320', circulate and rig up Howco and cement with 800 sacks
								Class G with 3% CaCl, cement in place at 9:45 p.m., waiting on cement.
5-18	325	0		0	150	8.8	57	Waiting on cement, cut off 20" and nipple up 20" hydril, test to 200# on hydril
				0	300			and manifold, pick up bottom hole assembly and TIH to 314', tag cement, drilling cement and float shoe, circulate and condition mud, POOH to pick up
								stabilizer.
5-19	1585	1260		0	440	9.1	43	Drilling, ream from 1,536' to 1,576', short trip, circulate and survey.
	• .			1/2	1020			
				1/2	1267			
	•			3/4	1513		ŀ	
5-20	2199	614		3/4	1764	9.0	37	Drilling, trip for bit, survey.
			_	1/4	2039			
5-21	2634	435		1/4	2321	9.0	38	Drilling, survey and short trip.
								· · · · · · · · · · · · · · · · · · ·
5-22	2705	. 71	_			9.0	40	Drilling to depth of 2,705 ¹ , circulate, POOH and TIH, clean up run - no fill, rig
	• •	ļ				•		up to run 13 3/8" 61# casing, running 2,700 ' of 13 3/8" 61# K55 casing, B&W shoe on bottom, float collars at 2 jts. above shoe, circulate, prep. to cement job.
		ļ						
5-23	2705	0	_			9.0	42	Circulate, condition after getting casing to
	·	 				:		bottom, cementing 13 3/8" at 2,701' with 18 bbls. of water ahead followed by 28 bbls. sepolite flush mixed 1,576 sacks of 1:1 pearlite, 40% SSA-1, .5% CFR-2,
								3% gel, .1% HR7, .25# per sack Flocele, tail cement consisting of 185 sacks Class G, 40% SSA-1, .75 CFR2, .1% HR7, 25# per sack of Flocele, displace with
								402 bbls. mud, bumped plug, recover 25% of the 100% excess to surface, cement did not fall back, in place at 4:00 a.m., waiting on cement, cut off 13 3/8" cas-

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DAILY DRILLING - WORKOVER LOG

CI E1/4-	IONE- ON	<u> </u>						Page 2 SPUDDED May 15, 19 80
LEVAT	IONS: GN	U			BI	H		DF RDB ASING RECORD
	PIPE SI	76	HOLE	SE/	T F.C	~ [C	CEMENTING DATA: Sacks, Kind, etc.
Conduct			HOLL					
Surface				-				
nterme					·	-+-		
Dil Strir								
	DEPTH	FOC	от. I		ES OFF	M	UD	REMARKS
DATE	TODAY	AG	••	DEG.	DEPTH	wτ	VIS	(Activity) (Formation) (D.S.T.) (Coring) (etc.)
:								
5-23								ing, set out 20" hydril, load out same, break cement sheath, orange peel 20" and 30", dress top of 13 3/8" casing, set on WKM.
5-24	2701	0				8.6	45	Weld on casing head and nipple up, change ram blocks in H&H gate as they
	· · · · · · · · · · · · · · · · · · ·							were upside down, rebuild kill line and manifold line, run in test plug, test blind rams to 1,000 psi for 30 minutes in presence of USGS man at midnight.
5-25	3136	430	6	1/2	296 1	8.8	42	TIH to 2,603 ', tag cement, test pipe rams to 1,000# OK by USGS man, drill out
								shoe at 2,701', drilling, POOH after survey to change BHA, Change BHA, TIH to 2,798', ream from 2,798' to 3,085' because of addition of stabilizers.
5-26	3683	546	6	1/4	3222	9.0	41	Drilling, survey.
				1/2	3467			
5-27	3891	208	8	3/4	3716	[~] 9.0	39	Drilling, survey & POOH, TIH to 2,778', reaming from 2,778' to 3,068', cir- culate and condition hole and mud, ream from 3,068' to 3,192'.
5-28	4185	294	•	1 1/4	3966	8.9	39	Ream and circulate 3,195 ' to 3,891 ', drilling, circulate and survey.
		ļ		1 1/4	4025			
				1 3/4	4149			
5-29	4294	109	9	1 1/2	4254	9.0	40	Drilling to 4,254', POOH, tight spot 3,590' to 2,860', TIH with new bit to 2,876', reaming from 2,876' to 4,254', drilling.
	· ·							
5-30	4630	340	0 ·	1 3/4	4521	9.1	40	Drilling, reaming after short trip, short trip.
5-31	4957	327	7	2	4647		•	Drilling, trip, circulate and survey.
6-1	5300	343	3	4	5300	8.9	45	Drilling, short trips, circulate and survey.
	· · · · · · · · · · · · · · · · · · ·							·
6-2	5526	226	5	3 1/2	5420	8.9	40	Drilling, trip time, POOH and TIH for bit #8, reaming from 5,260' to 5,300', circulate and survey.
	<u></u>							
6-3	5832	300	6	3 1/4	5545	9.0	40	Drilling, circulate and survey, short trips.
		ļ		3	5669			
6-4	5976	144	4	3 1/4	5887	8.9	39	Drilling and survey with bit #8, POOH with bit #8, change stabilizers, dress
								reamer with new cutters, check jars and shock sub, pick up bit #9, TIH, drilling twisted off, POOH, left 12 ¼ " reamer and bit in hole due to failure of bit sub
1.1		1						washed out, TIH to screw into fish at midnight.

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DAILY DRILLING - WORKOVER LOG

WELL	USA	A 11-3	36				P	age 3	SPUDDED	May 15,	19 80	
ELEVAT	IONS: GN	D			BI	н	DF RDB					
	2405						CA	SING RECORD	TINO DATA Osaka V			
Conduct	PIPE SI	IZE	HOLE	SE/	AT F.(<u>. </u>		CEMEN	TING DATA: Sacks, K	1na, etc.		
Surface							<u> </u>	······································			· · · · · · · · · · · · · · · · · · ·	
nterme	· · · · · · · · · · · · · · · · · · ·							· · ·	······		· · · · · · · · · · · · · · · · · · ·	
Dii Strin	-		<u> </u>	+			<u></u>	·····			· ·	
	DEPTH	F	DOT-	DEGRE	ES OFF	M	D		REMARKS			
DATE	TODAY		GE	DEG.	DEPTH	WT	VIS	(Activity)	(Formation) (D.S.		(etc.)	
	· · · · · · · · · · · · · · · · · · ·	+								<u> </u>		
6-5	6001		25			9.0	40	Fishing, TIH, circulate	at fish, screw into fish,	established circul	ation, pumped	
								fish free, chain out, lay	down fish, Magna-Flux	drill collars and	subs, picked up	
						ŀ		new BHA, TIH, checki reamed to TD, drilling,				
	· · · ·	.						to electrical short not a	ble to run optimum hyd	raulics.		
,									· · ·		• •	
6-6	6062		61			8.9	39	Drilling with one mud	pump due to electrical f	ailure, POOH on	even stands,	
				<u></u>				dressed near bit reamer				
·	<u></u>	+		<u>,.</u>		ľ		night.	· <u>·····</u>		<u></u>	
	• •								· · · · ·			
. 6-7	6160		98	1 1/2	6098	8.9	45	TIH to 6,002', ream to 4.9' /Hr.	6,062', circulate and s	urvey, drilling wi	th bit #10 average	
											· · ·	
6-8	6280		120	NG	6280	9.0	45	Drilling, trip, circulate	and survey.			
								· · · · · · · · · · · · · · · · · · ·	······································	······································		
6-9	6395		115			9.0	40	Trip for bit, ream after	trip 6,240 ' to 6,280 ', o	drilling.		
				·····				· ·				
6-10	6528		103	1 1/2	6528	8.9	39	Drilling survey POOH	I for bit and reamer cut	ter change	·	
				- /-				<i></i>				
6-11	. 6630		02			.9.0	38	TIH to 6,452', reaming	after trip drilling	<u></u>		
				<u></u>		. 9.0	30	1. 1.			·······	
6-12	6755	+ .	25			·		Drilling with bit #12.	, 		· · ·	
0-12	0/35	+ •	2.5			9.0	37	Drining with bit #12.		· · · ·		
6-13	6857	<u> </u>	02	2 1/2	6809	9.0	37	Drilling to 6,809', surv break circulation, wash	ey and POOH, TIH wit	h bit #13, stoppe	d at 6,793',	
								orcak cuculation, wash	eu out 1111 10 0,809 , dr	innag to 0,857/ 2	mianight.	
6-14	7056	<u>,</u>	99			9.0	42	Drilling with bit #13 an	d ana nu			
·	•	+					-7 6 0	Drining with oit #15 an	a one pump.			
6-15	7205	+ 	49	3 1/4	7121	8.9	42	Drilling with hit #12	OOH to change bit, sur			
	· · · · · · · · · · · · · · · · · · ·	+	<u> </u>	J /4	- 14-1		-74	while out #13, F				
6-16	7312	<u>† </u>	07			9.0		Finish POOL charge	bit, RIH 11 ' fill, drillin	na with his 414		
		1	<u> </u>		L	7.0	36		KALLI III, UIIIII	5 mill 011 #14.		

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DAILY DRILLING - WORKOVER LOG

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ELEVAT	IONS: GN	D.			B	н		age 4 SPUDDED May 15, 19 80 DF RDB
						-	C	ASING RECORD
	PIPE SI	ZE	HOLE	SEA	T F.C	2.		CEMENTING DATA: Sacks, Kind, etc.
Conduct				+				
Surface	•			+				an en antico de la competencia de la co La competencia de la c
Interme	d:			1			<u>.</u>	
Oil Strin	ng:		· · · ·					
	DEPTH	FOO	т. С	EGREE	SOFF	M	JD	REMARKS
DATE	TODAY	AG		DEG.	DEPTH	WT	VIS	(Activity) (Formation) (D.S.T.) (Coring) (etc.)
	•							
6-17	7438	126	;	4 ¾	7363	9.0	37	Drilling with bit #14, survey for direction.
	· · · · · · · · · · · · · · · · · · ·	. 						Drilling with bit #14, survey, POOH, change bit reamers and stabilizer, RIH - no
6-18	7519	81		5 1/4	7546	. 8.9	38	fill, drilling with bit #15.
	• •	<u> </u>						
6-19	7635	146	5	5 1/4	7550	9.0	40	Drilling, survey.
6-20	7737	102	2	4 3/4	7643	9.0	38	Drilling, survey.
				5	7733			
6-21	7809	72				9.0	35	Drilling, trip for bit #16, POOH and TIH - no problems, cut off drilling line.
6-22	7924	115		5 1/4	7859	8.9	38	Drilling with bit #16, survey at 7,859'.
6-23	8022	98		5 1/4	7952	8.9	39	Drilling with bit #16, directional Wireline survey.
				5 1/2	8044			
6-24	8144	122	· .	5 1/2	8044	9.0	39	Drilling with bit #16, survey.
		ļ		5 1/2	8137			
6-25	8258	114	•		·	9.06	46	Drilling, POOH for bit change, drop junk sub, pick up bit #17, TIH to 8,161', circulate for trip.
6-26	8421	163	3	5 1/2	8258	9.0	38	Drilling, survey.
				5 3/4	8352	· .		
6-27	8565	144		5 1/2	8444	8.9	32	Drilling, circulate and condition hole, survey dev.
		<u> </u>		5 1/2	8565			
6-28	8565	0				9.0	37	POOH, short trip, TIH 35' fill, circulate and condition hole and mud, POOH to
								log, set back drill collars, run temp. surveys, stuck same on second run at 5,700', pulled line in two at key seat, making up four-prong spear to fish wireline and
								instruments at midnight.
6-2 9	8565	0	_			. 9.0	40	TIH with spear, picking up wireline to 8,397 ' at 6:00, circulate, POOH,
		ļ						recovered all of fish, attempt to run electric logs - failed, repairing short in log line of Dresser Atlas, running DI, FL, BHC, AL, Cal at midnight.
6-30	0.445	<u> </u>						Finish electric log Dresser Atlas, CDL GR logs, running Pruitt Wireline Services,
0-30	8565	0				9.0	46	temp. surveys, both stops, and travers charts at midnight.

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DAILY DRILLING · WORKOVER LOG

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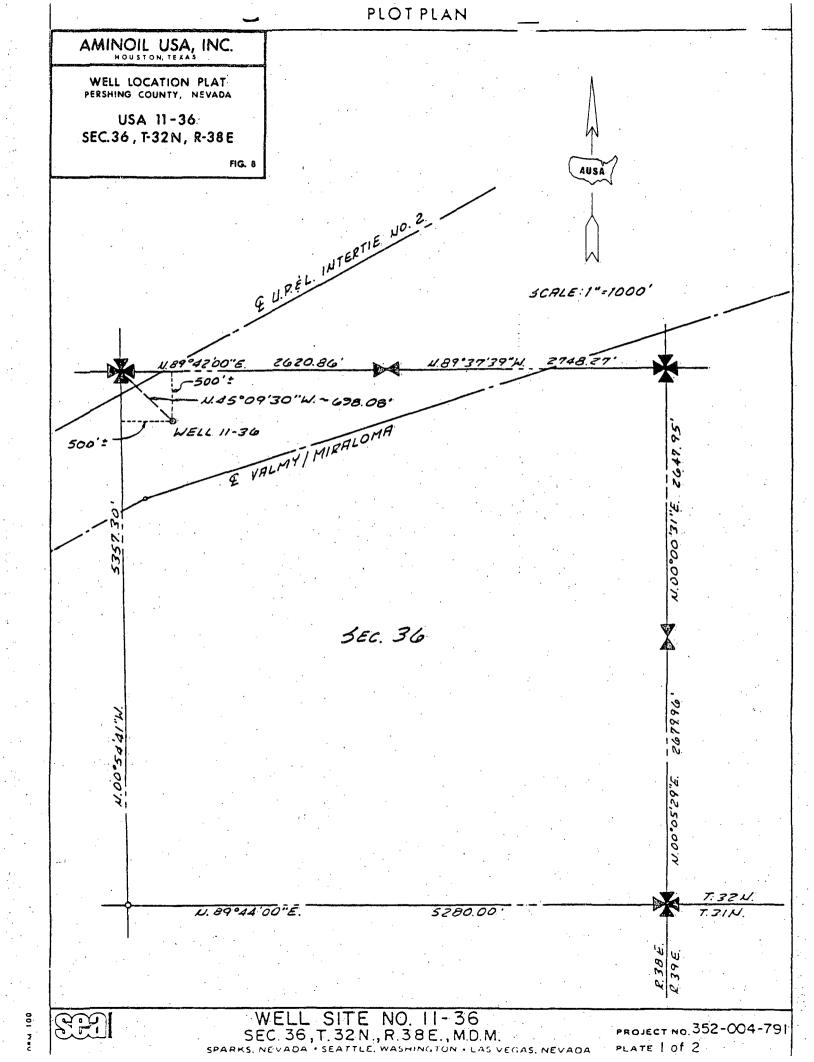
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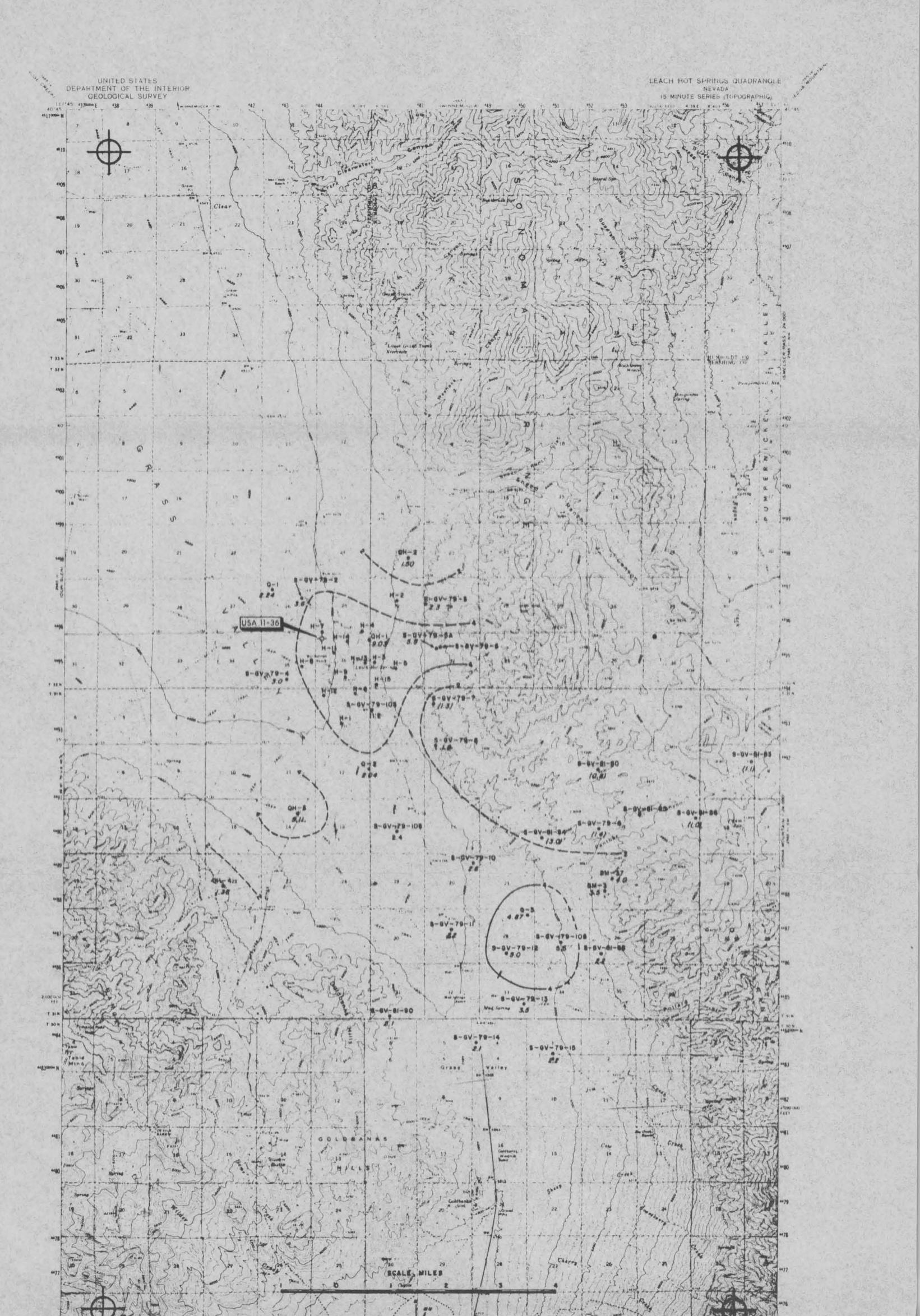
LEVATI	ONS: GNE			81		CA	DF RD8
i	PIPE SIZ	E HOL	E SEA	T F.C			CEMENTING DATA: Sacks, Kind, etc.
Conduct				-		····	
Surface:		-		_			
Intermo	t:						· · · · · · · · · · · · · · · · · · ·
Oll Strin	ğ:						
DATE	DEPTH	FOOT-		ES OFF	·	UD	REMARKS
	TODAY	AGE	DEG.	DEPTH	WT	VIS	(Activity) (Formation) (D.S.T.) (Coring) (etc.)
	, 						
7-1	8565	. 0					Running continuous temp. survey successfully, TIH with DC'S, HW, and 10 stds.
						<u> </u>	5" DP, POOH laying down 10 stds. of DP, 12 jts. HW, 12 jts. DC 's 12 ¼"
}				·			tools, stabilizers, reamers, etc., TIH with 5" DP to 7,100', set 50 sacks cement
].							plug consisting of 40% SSA-1, .75% CFR2, 3% HR7, at 7100' 5:40 p.m., POOH setting back 2700' DP, laying down the remainder, picked up EZSV tool
				· ·			TIH with same, set at 2,572', 10:40 p.m., pressure up back side 500 PSI, break
1							down formation at 900 PSI, squeezed 130 sacks cmt. consisting of 40% SSA-1,
			,		· · ·		.75% CFR2, got off of EZSV, pulled 1 std., spotted 20 sxs. cement consisting of 40% SSA-1, .75% CFR-2 on top of EZSV, cleared pipe with 30 bbl. water at
							midnight.
	<u></u>				ļ		
7-2	8565	0					POOH laying down 81 jts. of DP, TIH with 60 jts. POOH, laying down same,
							at 60' in, picked up kelley, pumped 9 bbls. water ahead, set 30 sacks cement plug consisting of 40% SSA-1, .75% CFR-2, displaced with 2 bbls. of water to
		6 - 1 - E					clear lines, washed BOE clean for safety measure, dismantled and set out BOPE
						┝╍╌╸┥	stack in 3 components, load drillpipe, cut off casing head 6 1/2 ' below surface, weld on cap with handle, released rig at 12 NOON 7-2-80, P&A at 8,565 ' depth,
							final report.
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APPENDIX B

FIGURES 2 - 10





Explanation

- S-GV-79-15 Sunedco-Grass Valley project holes.
- Q-3, QH-4 Heat-flow and heat-flow-hydrologic test holes.
 - H-1 Shallow hydrologic test wells.
- BM-37 Hole used by Sass <u>et al.</u> (1971) in heat flow determinations.
- 2.6 Heat flow (in 10⁻⁶ cal/cm²-sec, or HFU) from 100-150m depth interval. Parentheses indicate value from slightly shallower depth. Sunedco's holes represented by average of values computed for maximum and minimum porosity conditions. Published values shown as reported.
- 2.4 Heat-flow (in HFU) from 300-450m depth interval. Average of volues computed for minimum and maximum porosity conditions.

Contours on heat flow values at 2 and 4 HFU. Based chiefly on values from IOO-I5Om interval, but also reflecting values from deeper interval. Contours dashed where approximate.

PHASE III

AMINOIL USA, INC.

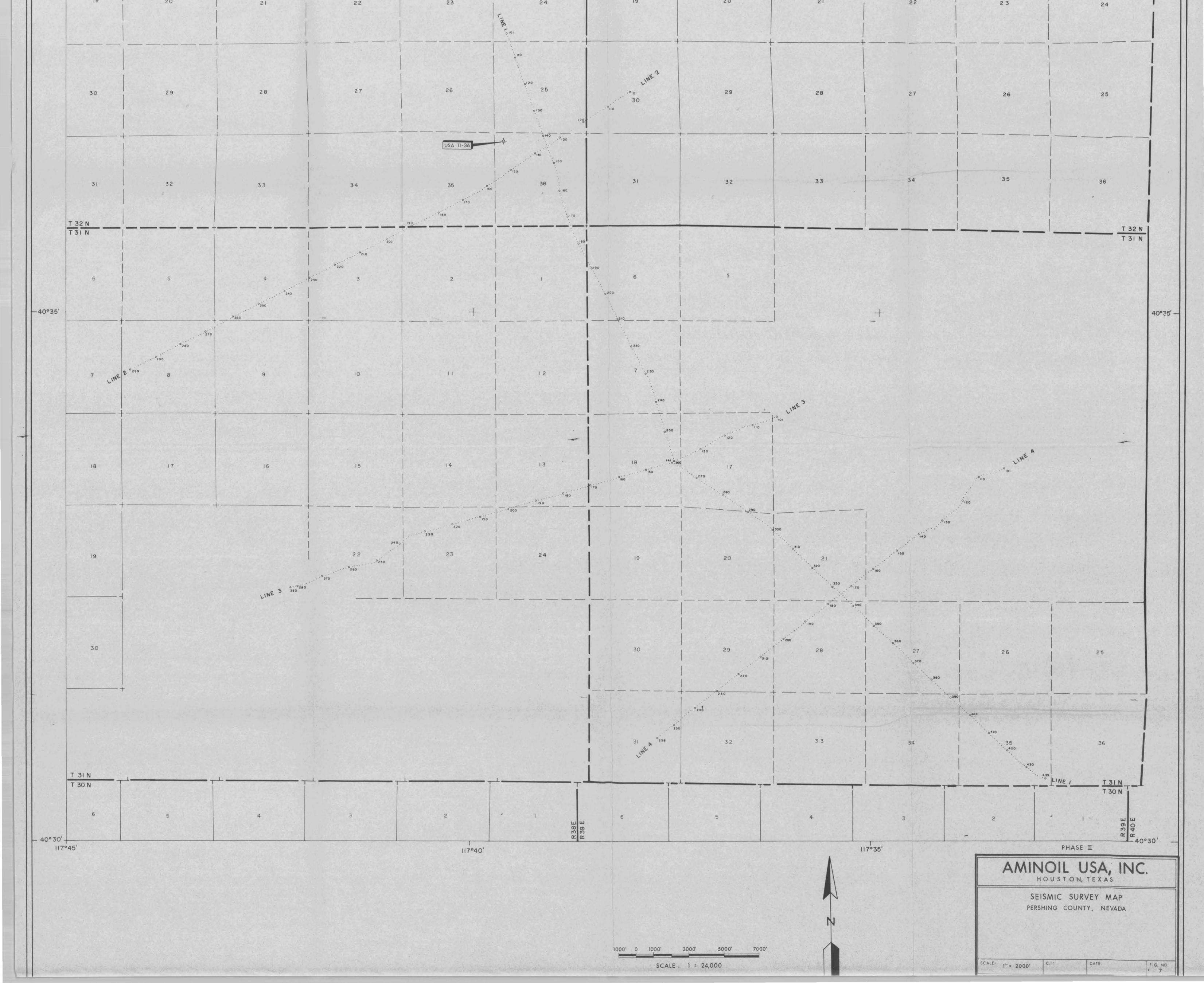
GRASS VALLEY AREA

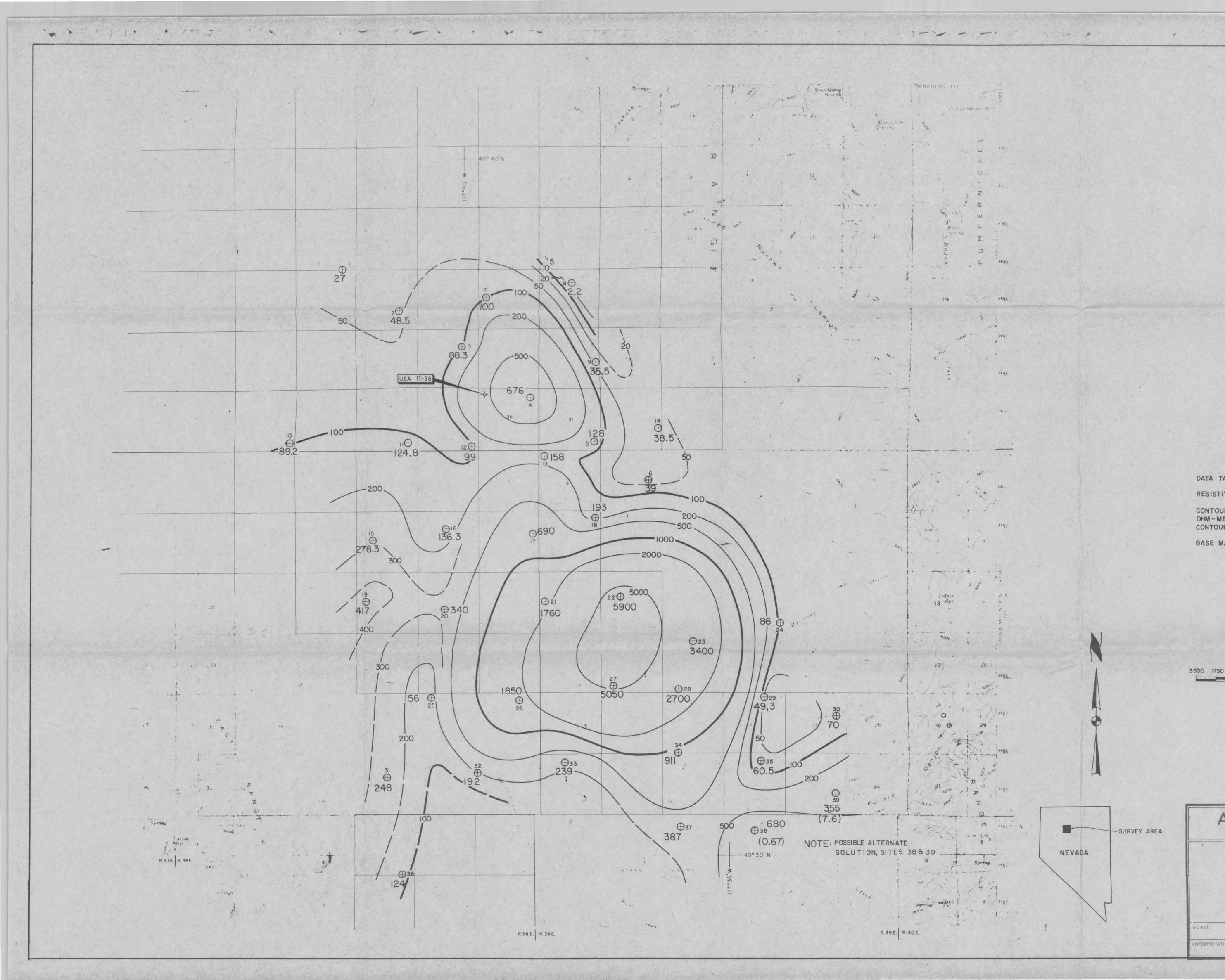
TEMPERATURE GRADIENT WELL LOCATIONS & HEAT FLOW CONTOURS

C.1.:	DATE	FIG. NO 10
and the second	DRAFTING:	FILE NO:
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19 20		19 20		





DATA TAKEN FROM RTE COMPONENT RESISTIVITY VALUES IN OHM-METERS

A MARY MARKEN AND A STORE

CONTOUR INTERVAL = 1,2,5,×10^N OHM-METERS WITH SUPPLEMENTARY CONTOURS

BASE MAP: USGS TOPO.

	1				
	θ	SITE L	OCATION		
	00	SITE N	UMBER	a for the	
3500 1750	0	3500	7000	10,500	14,000 feet
				•	
		PHA	SE II		

--SURVEY AREA NEVADA 1 10

SCALE:

INTERPRETATION

AMINOIL USA, INC. HOUSTON, TEXAS GRASS VALLEY AREA PERSHING COUNTY, NEVADA RESISTIVITY DISTRIBUTION

AT - 12,000 FEET

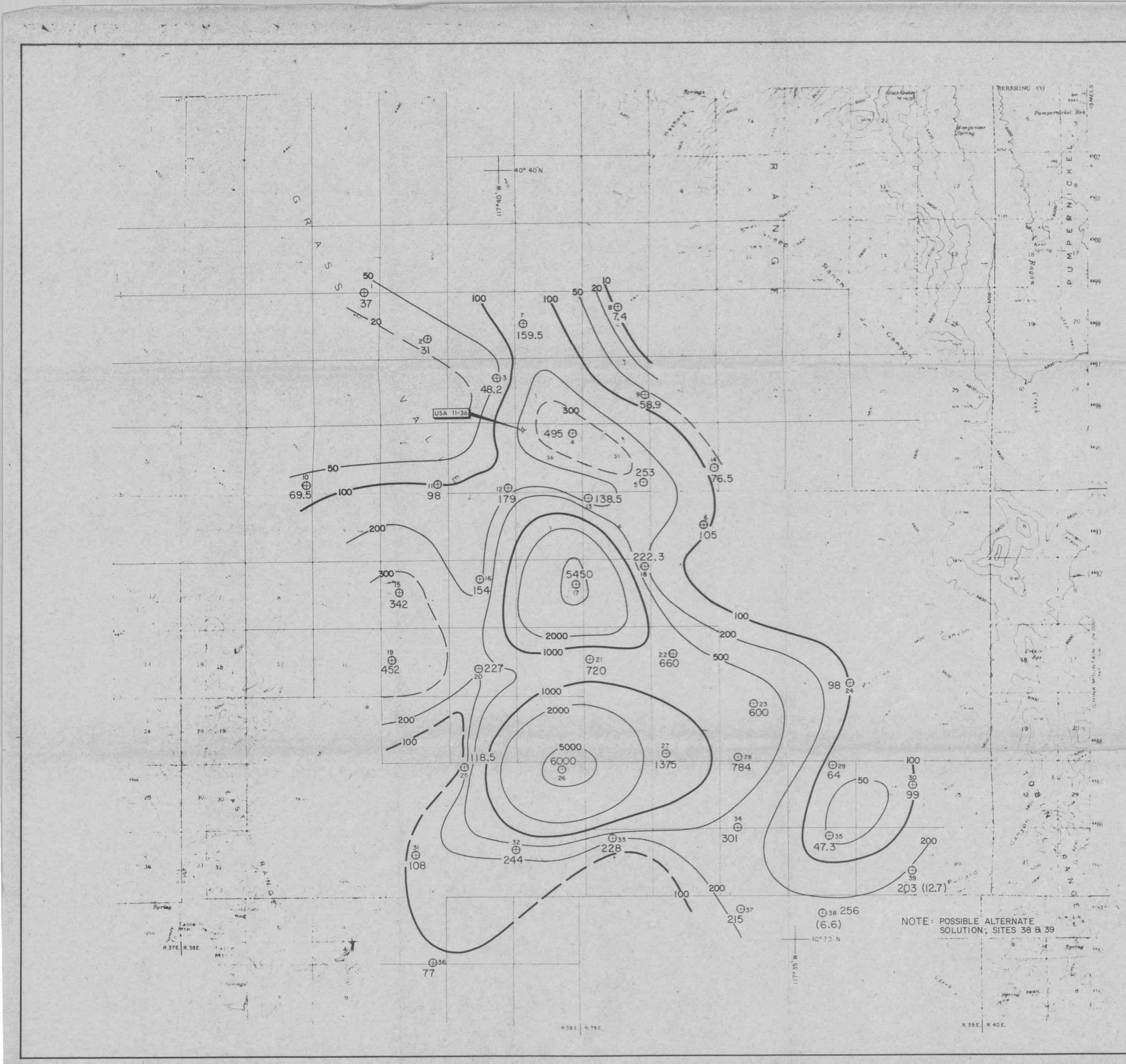
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FIG. NO

CEILE NO



DATA TAKEN FROM RTE COMPONENT RESISTIVITY VALUES IN OHM-METERS

CONTOUR INTERVAL = 1,2,5,×10^N OHM-METERS WITH SUPPLEMENTARY CONTOURS

BASE MAP: USGS TOPO.

1

-SURVEY AREA

-

NEVADA

\oplus	SITE LOCATION
00	SITE NUMBER

00	1750	0	3500	7000	10,500	14,000
			-			

AMINOIL USA, INC. HOUSTON, TEXAS GRASS VALLEY AREA

PHASE II

PERSHING COUNTY, NEVADA RESISTIVITY DISTRIBUTION AT - 4000 FEET

DATE

SCALE

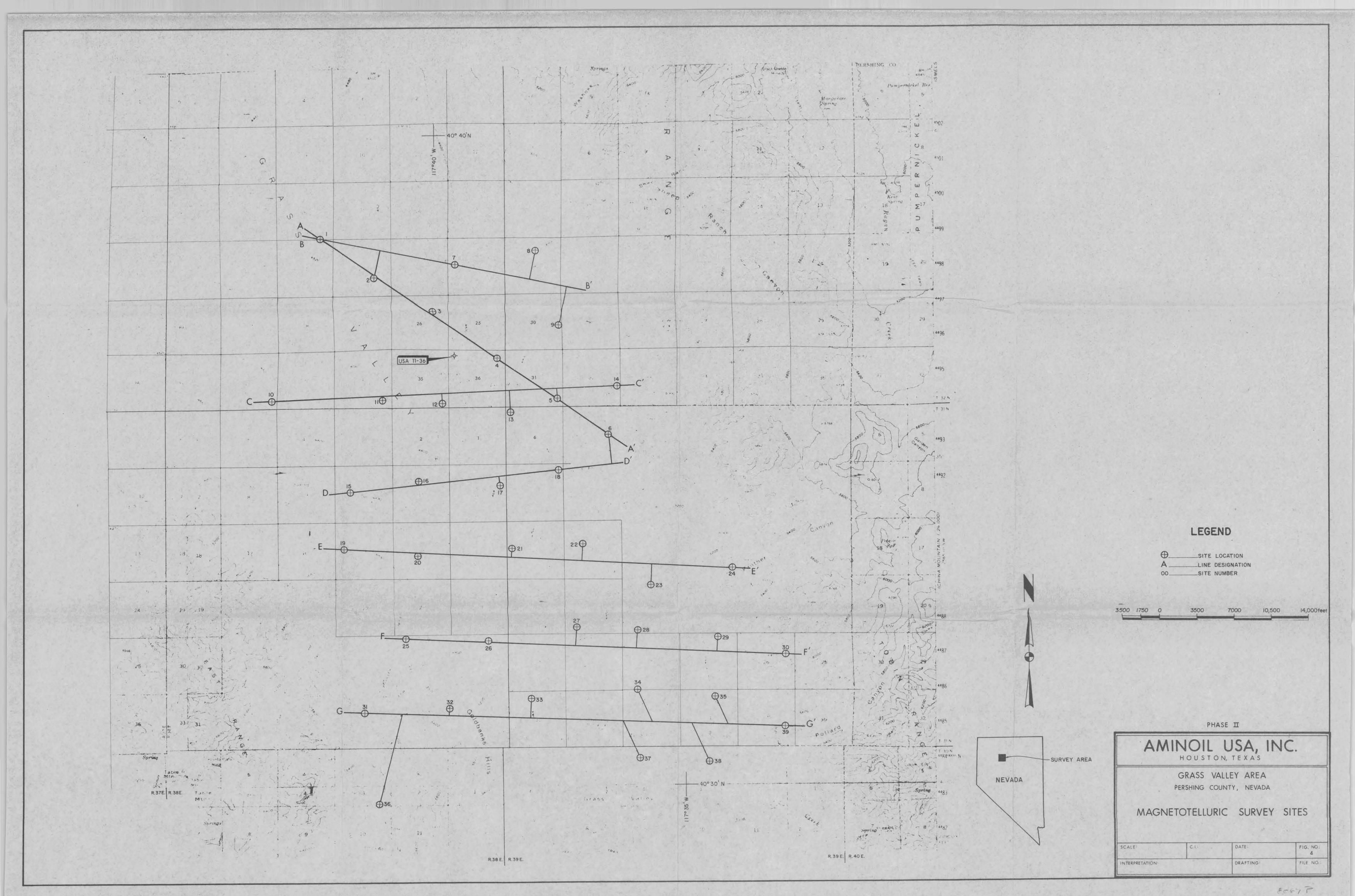
INTERPRETATION

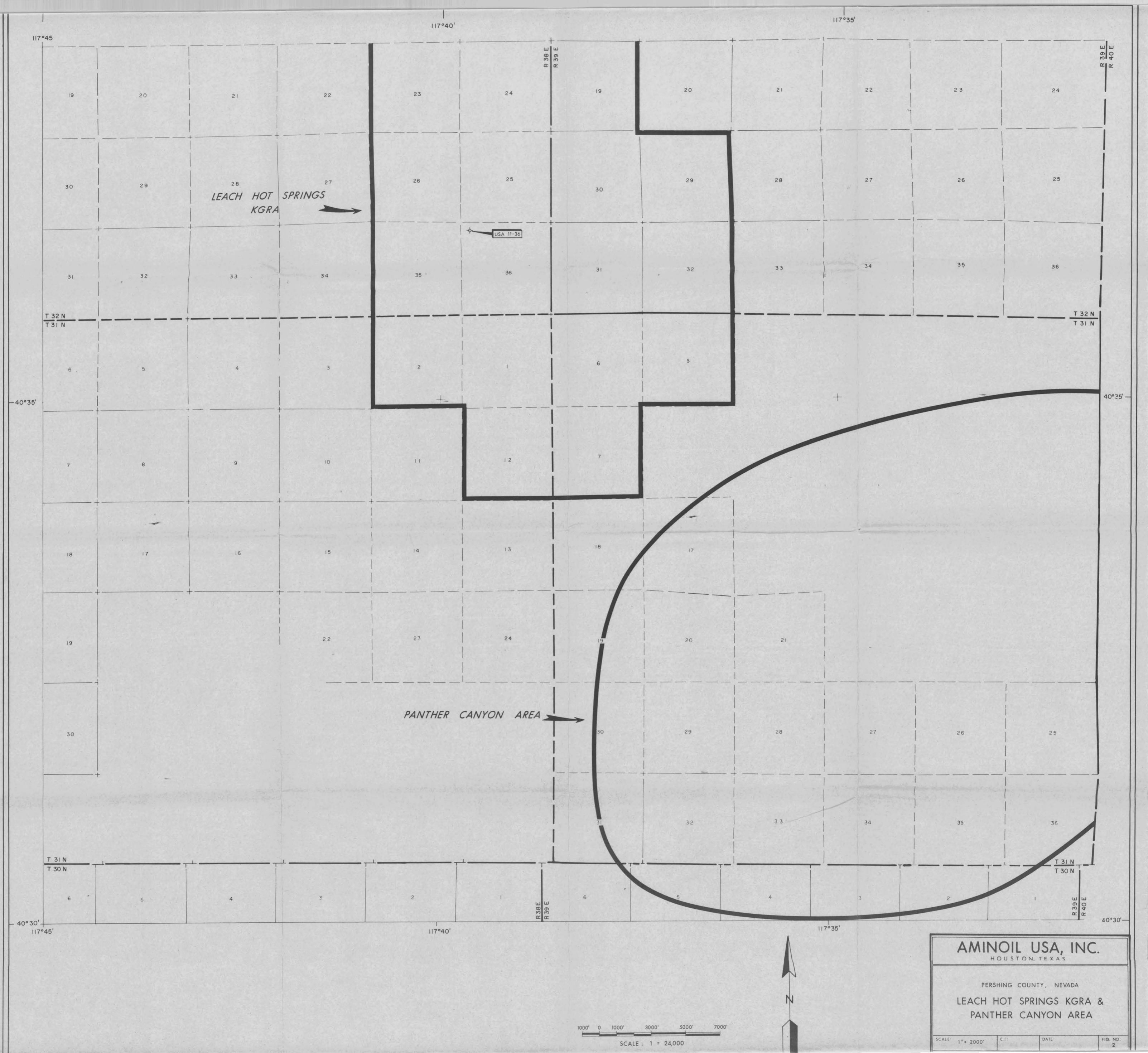
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FIG. NO.



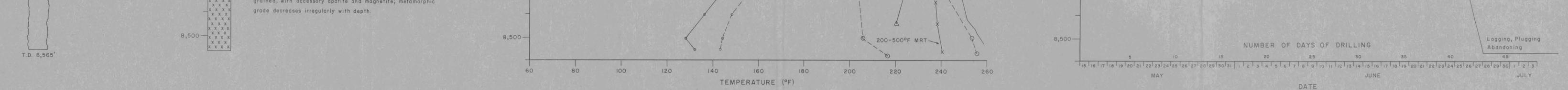


TEMPERATURE DATA

PENETRATION RECORD

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CASING	G PROGRAM	, LITHOLOG	IC LOG
	TEMPERATU	RE SURVEYS &	
	DRILLING T	IME CURVE	
SCALE	C ()	DATE	FIG. NO
INTERPRETATION		DRAFTING	FILE NO

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